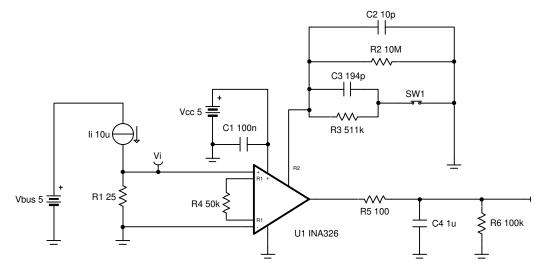


#### **Design Goals**

Input		Output		Supply		
l <sub>iMin</sub>	I <sub>iMax</sub>	V <sub>oMin</sub>	V <sub>oMax</sub>	V <sub>cc</sub>	V <sub>ee</sub>	V <sub>ref</sub>
10 µA	10 mA	100 mV	4.9 V	5.0 V	0 V	0 V

#### **Design Description**

This single-supply, low-side, current-sensing solution accurately detects load current between 10  $\mu$ A and 10 mA. A unique yet simple gain switching network was implemented to accurately measure the three-decade load current range.



#### **Design Notes**

- 1. Use a maximum shunt resistance to minimize relative error at minimum load current.
- 2. Select 0.1% tolerance resistors for R<sub>1</sub>, R<sub>2</sub>, R<sub>3</sub>, and R<sub>4</sub> in order to achieve approximately 0.1% FSR gain error.
- 3. Use a switch with low on-resistance (R<sub>on</sub>) to minimize interaction with feedback resistances, preserving gain accuracy.
- 4. Minimize capacitance on INA326 gain setting pins.
- 5. Scale the linear output swing based on the gain error specification.

1



# **Design Steps**

1. Define full-scale shunt resistance.

$$R_1 = \frac{V_{iMax}}{I_{iMax}} = \frac{250 \text{mV}}{10 \text{mA}} = 25\Omega$$

2. Select gain resistors to set output range.

$$G_{IiMax} = \frac{V_{oMax}}{V_{iMax}} = \frac{V_{oMax}}{R_1 \times I_{iMax}} = \frac{4.9V}{25\Omega \times 10mA} = 19.6\frac{V}{V}$$

$$G_{IiMin} = \frac{V_{oMin}}{V_{iMin}} = \frac{V_{oMin}}{R_1 \times I_{iMin}} = \frac{100mV}{25\Omega \times 10\mu A} = 400\frac{V}{V}$$

$$R_2 = \frac{R_4 \times G_{IiMin}}{2} = \frac{50k\Omega \times 400\frac{V}{V}}{2} = 10M\Omega$$

$$R_2 \parallel R_3 = \frac{R_4 \times G_{IiMax}}{2} = \frac{50k\Omega \times 19.6\frac{V}{V}}{2} = 490k\Omega$$

$$R_3 = \frac{490k\Omega \times R_2}{R_2 - 490k\Omega} = 515.25k\Omega \approx 511k\Omega \text{ (Standard Value)}$$

3. Select a capacitor for the output filter.

$$f_p = \frac{1}{2 \times \pi \times R_5 \times C_4} = \frac{1}{2 \times \pi \times 100\Omega \times 1 \ \mu F} = 1.59 \text{kHz}$$

4. Select a capacitor for gain and filtering network.

$$C_{2} = \frac{1}{2 \times \pi \times R_{2} \times f_{p}} = \frac{1}{2 \times \pi \times 10M\Omega \times 1.59 \text{kHz}} = 10 \text{pF}$$

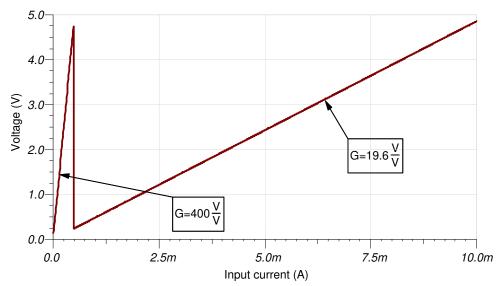
$$C_{3} = \frac{1}{2 \times \pi \times (R_{2} \mid \mid R_{3}) \times f_{p}} - C_{2} = \frac{1}{2 \times \pi \times (10M\Omega \mid \mid 511 \text{k}\Omega) \times 1.59 \text{kHz}} - 10 \text{pF}$$

 $C_3 = 196 pF \approx 194 pF$  (Standard Value)

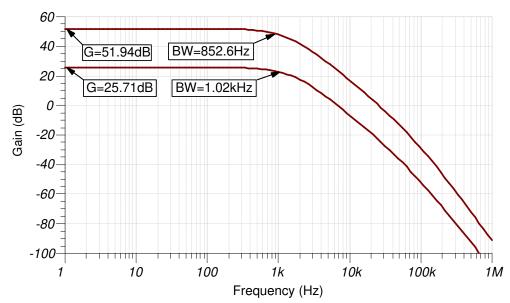


## **Design Simulations**

## **DC Simulation Results**



## **AC Simulation Results**





Page

### **Design References**

See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.

See circuit SPICE simulation file SBOC498.

See TIPD104, Current Sensing Solution, 10 µA-10 mA, Low-Side, Single Supply.

### **Design Featured Op Amp**

INA326				
V <sub>ss</sub>	1.8 V to 5.5 V			
V <sub>inCM</sub>	Rail-to-rail			
V <sub>out</sub>	Rail-to-rail			
V <sub>os</sub>	0.1 mV			
Ι <sub>q</sub>	3.4 mA 2 nA			
۱ <sub>b</sub>				
UGBW	1 kHz			
SR	Filter limited			
#Channels	1			
INA326				

## **Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

#### Changes from January 28, 2018 to February 1, 2019

Downscale the title and changed title role to 'Amplifiers'. Added link to circuit cookbook landing page......1

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