

# **TLV1704-SEP Single-Event Latch-Up (SEL) Radiation Report**

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## **ABSTRACT**

The purpose of this study was to characterize the effects of heavy-ion irradiation on the single-event latch-up (SEL) performance of the TLV1704-SEP 2.2-V to 36-V, microPower comparator. Heavy-ions with an LET<sub>EFF</sub> of 43 MeV-cm<sup>2</sup>/mg were used to irradiate the devices with a fluence of  $1 \times 10^7$  ions/cm<sup>2</sup>. The results demonstrate that the TLV1704-SEP is SEL-free up to LET<sub>EFF</sub> = 43 MeV-cm<sup>2</sup>/mg at 125°C.

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## 1 Overview

The TLV1704-SEP (Quad) device offers a wide supply range, rail-to-rail inputs, low quiescent current, and low propagation delay. All these features come in industry-standard, extremely-small packages, making these devices the best general-purpose comparators available. The open collector output offers the advantage of allowing the output to be pulled to any voltage rail up to +36 V above the negative power supply regardless of the TLV1704-SEP supply voltage. The device is a microPower comparator. Low input offset voltage, low input bias currents, low supply current, and open-collector configuration makes the TLV1704-SEP device flexible enough to handle almost any application, from simple voltage detection to driving a single relay.

[www.ti.com/product/TLV1704-SEP/technicaldocuments](http://www.ti.com/product/TLV1704-SEP/technicaldocuments)

**Table 1. Overview Information<sup>(1)</sup>**

DESCRIPTION	DEVICE INFORMATION
TI Part Number	TLV1704-SEP
MLS Number	TLV1704AMPWTPSEP
Device Function	Radiation Hardened microPower Quad Comparator in Space Enhanced Plastic
Technology	BICOM3XHV
Exposure Facility	Radiation Effects Facility, Cyclotron Institute, Texas A&M University
Heavy Ion Fluence per Run	$1 \times 10^6 - 1 \times 10^7$ ions/cm <sup>2</sup>
Irradiation Temperature	125°C (for SEL testing)

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## 2 SEE Mechanisms

The primary single-event effect (SEE) events of interest in the TLV1704-SEP are single-event latch-up (SEL). From a risk/impact point-of-view, the occurrence of an SEL is potentially the most destructive SEE event and the biggest concern for space applications. The BICOM3XHV was used for the TLV1704-SEP. CMOS circuitry introduces a potential for SEL and SEB susceptibility. SEL can occur if excess current injection caused by the passage of an energetic ion is high enough to trigger the formation of a parasitic cross-coupled PNP and NPN bipolar structure (formed between the p-sub and n-well and n+ and p+ contacts). The parasitic bipolar structure initiated by a single-event creates a high-conductance path (inducing a steady-state current that is typically orders-of-magnitude higher than the normal operating current) between power and ground that persists (is “latched”) until power is removed or until the device is destroyed by the high-current state. The process modifications applied for SEL-mitigation were sufficient as the TLV1704-SEP exhibited no SEL with heavy-ions up to an  $LET_{EFF}$  of 43 MeV-cm<sup>2</sup>/mg at a fluence of 10<sup>7</sup> ions/cm<sup>2</sup> and a chip temperature of 125°C.

This study was performed to evaluate the SEL effects with a bias voltage of 36 V on V<sub>S</sub> Supply Voltage. Heavy ions with  $LET_{EFF} = 43$  MeV-cm<sup>2</sup>/mg were used to irradiate the devices. Flux of 10<sup>5</sup> ions/s-cm<sup>2</sup> and fluence of 10<sup>7</sup> ions/cm<sup>2</sup> were used during the exposure at 125°C temperature.

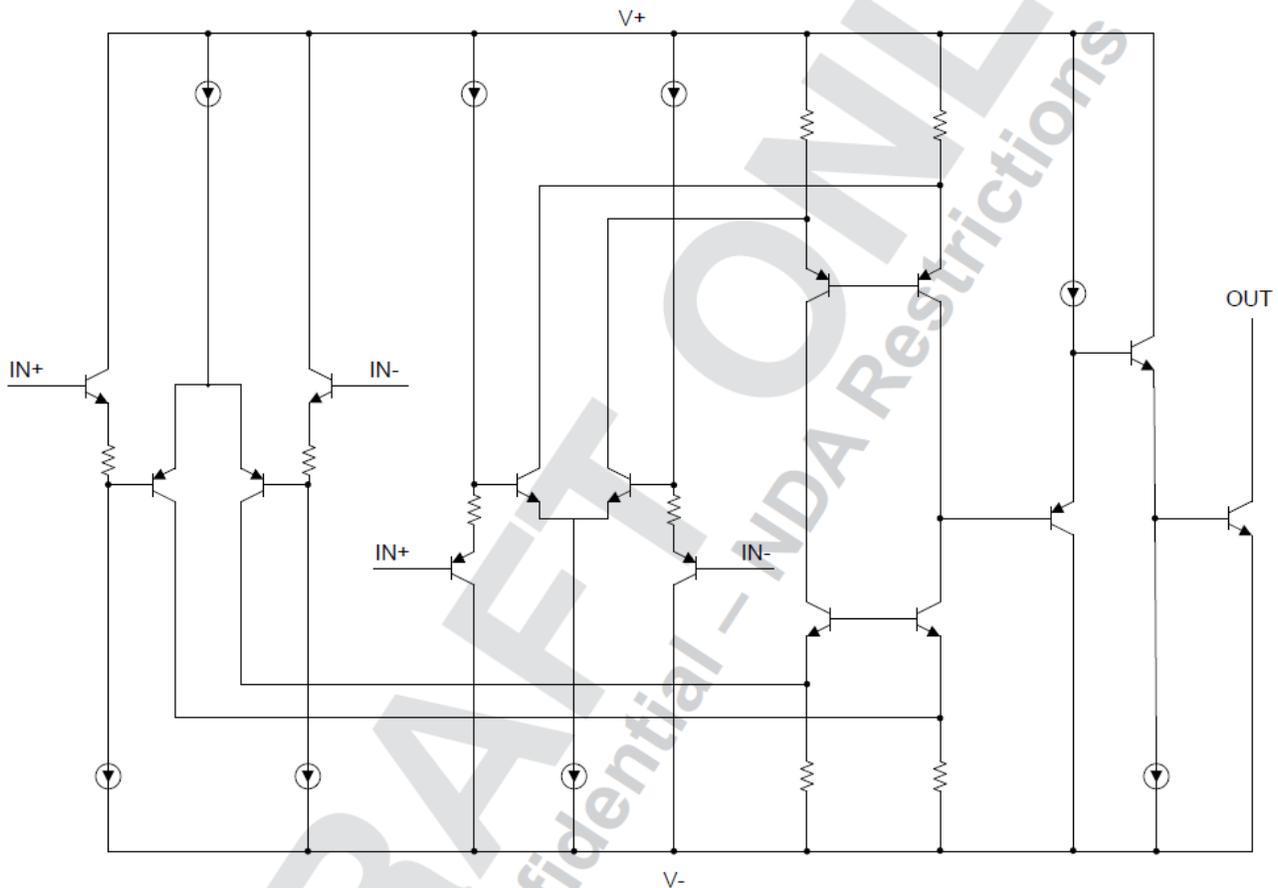
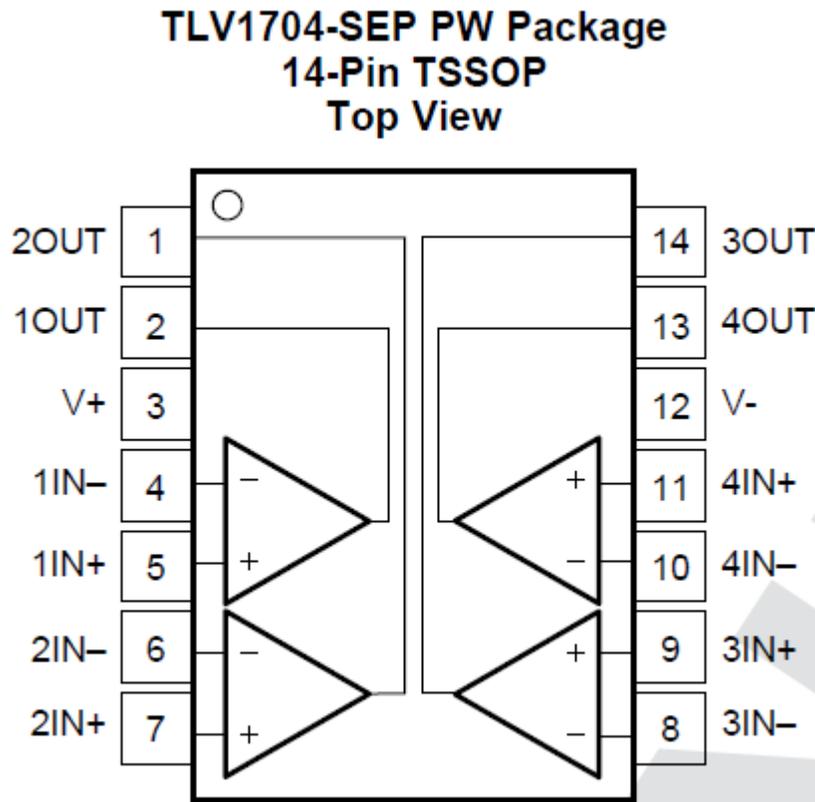


Figure 1. Functional Block Diagram of the TLV1704-SEP

### 3 Test Device and Test Board Information

The TLV1704-SEP is packaged in a 14-pin, TSSOP shown with pinout in [Figure 2](#). The TLV1704-SEP bias board is used for the SEE characterization is shown in [Figure 3](#) and bias diagram in [Figure 4](#).



NOTE: TLV1704-SEP pinout diagram. The package was decap'ed to reveal the die face for all heavy ion testing.

**Figure 2. TLV1704-SEP Pinout Diagram**

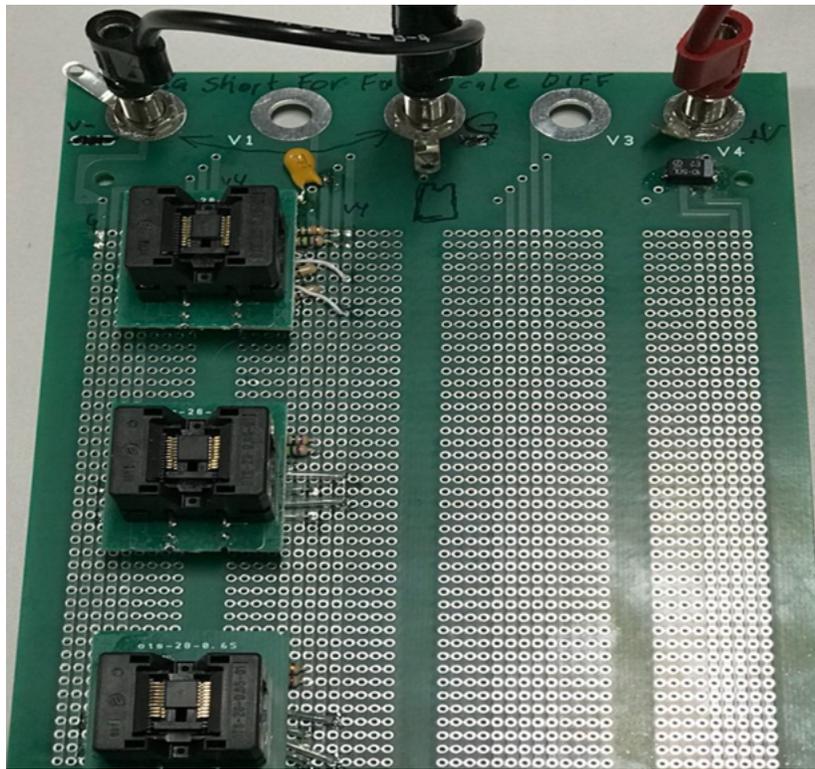


Figure 3. TLV1704-SEP Bias Board used for SEL Testing

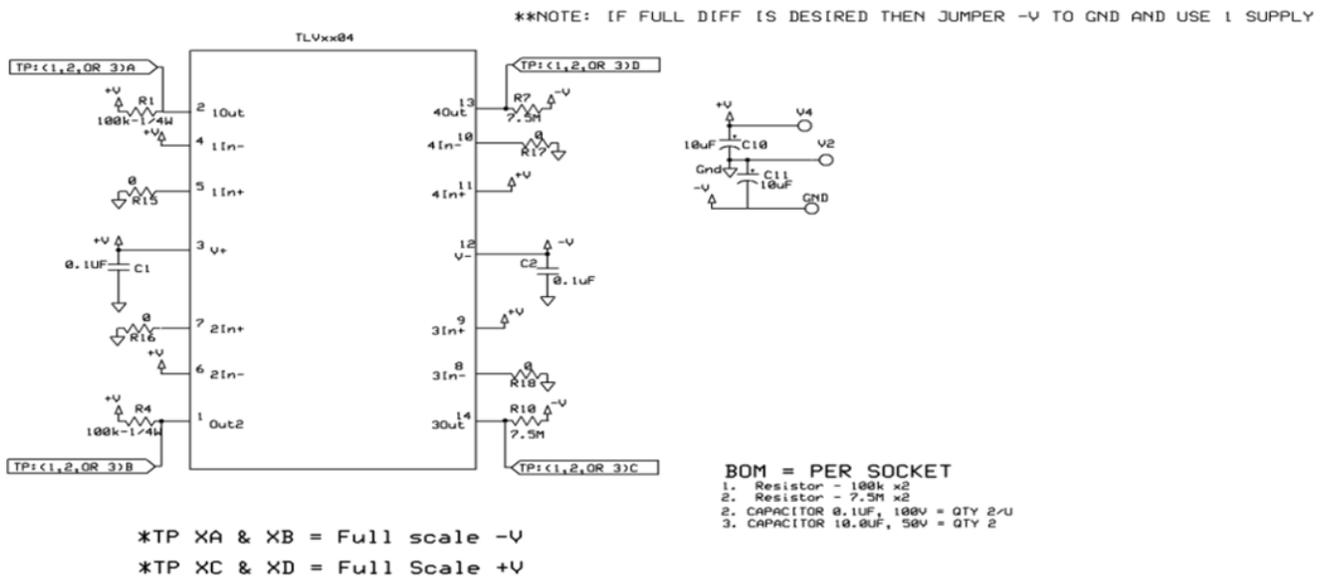


Figure 4. TLV1704-SEP Bias Diagram

## 4 Irradiation Facility and Setup

The heavy ion species used for the SEE studies on this product were provided and delivered by the TAMU Cyclotron Radiation Effects Facility [3] using a superconducting cyclotron and advanced electron cyclotron resonance (ECR) ion source. Ion beams are delivered with high uniformity over a 1-in diameter circular cross sectional area for the in-air station. Uniformity is achieved by means of magnetic defocusing. The intensity of the beam is regulated over a broad range spanning several orders of magnitude. For the bulk of these studies, ion fluxes between  $10^4$  and  $10^5$  ions/s-cm<sup>2</sup> were used to provide heavy ion fluences between  $10^6$  and  $10^7$  ions/cm<sup>2</sup>. For these experiments Silver (Ag) ions were used. Ion beam uniformity for all tests was in the range of 91% to 98%.

## 5 Results

### 5.1 SEL Results

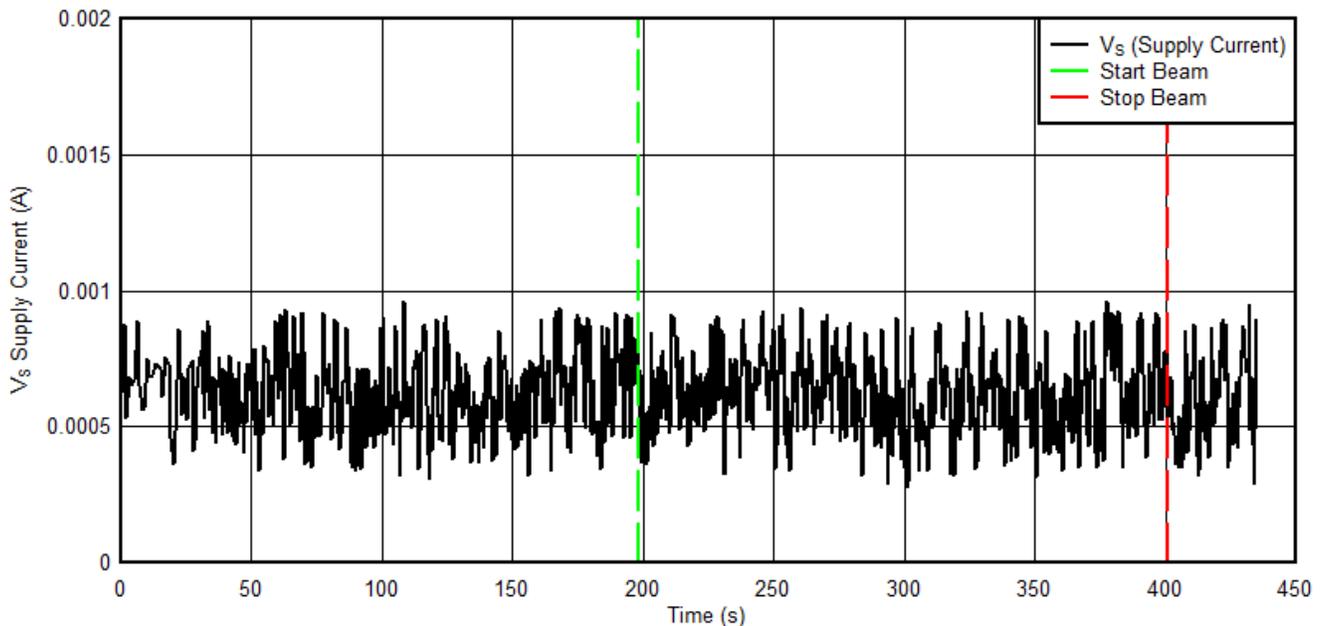
During SEL characterization, the device was heated using forced hot air, maintaining the IC temperature at 125°C. The temperature was monitored by means of a K-type thermocouple attached as close as possible to the IC. The species used for the SEL testing was a silver ( $^{47}\text{Ag}$ ) ion with an angle-of-incidence of  $0^\circ$  for an  $\text{LET}_{\text{EFF}} = 43 \text{ MeV}\cdot\text{cm}^2/\text{mg}$ . The kinetic energy in the vacuum for this ion is 1.634 GeV (15-MeV/amu line). A flux of approximately  $10^5 \text{ ions}/\text{cm}^2\cdot\text{s}$  and a fluence of approximately  $10^7 \text{ ions}$  were used for two runs. The  $V_s$  supply voltage is supplied externally on board at recommended maximum voltage setting of 36 V. Run duration to achieve this fluence was approximately 2 minutes. No SEL events were observed during all four runs shown in Table 2. Figure 5 shows a plot of the current vs time.

**Table 2. TLV1704-SEP SEL Conditions Using  $^{47}\text{Ag}$  at an Angle-of-Incidence of  $45^\circ$**

RUN #	DISTANCE (mm)	TEMPERATURE ( $^\circ\text{C}$ )	ION	ANGLE	FLUX ( $\text{ions}\cdot\text{cm}^2/\text{mg}$ )	FLUENCE (# ions)	$\text{LET}_{\text{EFF}}$ ( $\text{MeV}\cdot\text{cm}^2/\text{mg}$ )
30	40	125	Ag	$0^\circ$	1.00E+05	2.00E+07	43

No SEL events were observed, indicating that the TLV1704-SEP is SEL-immune at  $\text{LET}_{\text{EFF}} = 43 \text{ MeV}\cdot\text{cm}^2/\text{mg}$  and  $T = 125^\circ\text{C}$ . Using the MFTF method described in Appendix A and combining (or summing) the fluences of the two runs @  $125^\circ\text{C}$  ( $2 \times 10^7$ ), the upper-bound cross-section (using a 95% confidence level) is calculated as:

$$\sigma_{\text{SEL}} \leq 1.84 \times 10^{-7} \text{ cm}^2 \text{ for } \text{LET}_{\text{EFF}} = 43 \text{ MeV}\cdot\text{cm}^2/\text{mg} \text{ and } T = 125^\circ\text{C}.$$



**Figure 5. Current vs Time (I vs t) Data for  $V_s$  Current During SEL Run # 1**

## 6 Summary

Radiation effects Radiation Hardened microPower Quad Comparator in Space Enhanced Plastic TLV1704-SEP was studied. This device passed total dose rate of up to 30 krad(Si) and is latch-up immune up to  $LET_{EFF} = 43 \text{ MeV-cm}^2/\text{mg}$  and  $T = 125^\circ\text{C}$ .

## Confidence Interval Calculations

For conventional products where hundreds of failures are seen during a single exposure, one can determine the average failure rate of parts being tested in a heavy-ion beam as a function of fluence with high degree of certainty and reasonably tight standard deviation, and thus have a good deal of confidence that the calculated cross-section is accurate.

With radiation hardened parts however, determining the cross-section becomes more difficult since often few, or even, no failures are observed during an entire exposure. Determining the cross-section using an average failure rate with standard deviation is no longer a viable option, and the common practice of assuming a single error occurred at the conclusion of a null-result can end up in a greatly underestimated cross-section.

In cases where observed failures are rare or non-existent, the use of confidence intervals and the chi-squared distribution is indicated. The Chi-Squared distribution is particularly well-suited for the determination of a reliability level when the failures occur at a constant rate. In the case of SEE testing, where the ion events are random in time and position within the irradiation area, one expects a failure rate that is independent of time (presuming that parametric shifts induced by the total ionizing dose do not affect the failure rate), and thus the use of chi-squared statistical techniques is valid (since events are rare an exponential or Poisson distribution is usually used).

In a typical SEE experiment, the device-under-test (DUT) is exposed to a known, fixed fluence (ions/cm<sup>2</sup>) while the DUT is monitored for failures. This is analogous to fixed-time reliability testing and, more specifically, time-terminated testing, where the reliability test is terminated after a fixed amount of time whether or not a failure has occurred (in the case of SEE tests fluence is substituted for time and hence it is a fixed fluence test [5]). Calculating a confidence interval specifically provides a range of values which is likely to contain the parameter of interest (the actual number of failures/fluence). Confidence intervals are constructed at a specific confidence level. For example, a 95% confidence level implies that if a given number of units were sampled numerous times and a confidence interval estimated for each test, the resulting set of confidence intervals would bracket the true population parameter in about 95% of the cases.

In order to estimate the cross-section from a null-result (no fails observed for a given fluence) with a confidence interval, we start with the standard reliability determination of lower-bound (minimum) mean-time-to-failure for fixed-time testing (an exponential distribution is assumed):

$$MTTF = \frac{2nT}{\chi^2_{2(d+1); 100(1-\frac{\alpha}{2})}} \tag{1}$$

Where *MTTF* is the minimum (lower-bound) mean-time-to-failure, *n* is the number of units tested (presuming each unit is tested under identical conditions) and *T*, is the test time, and  $\chi^2$  is the chi-square distribution evaluated at  $100(1 - \alpha / 2)$  confidence level and where *d* is the degrees-of-freedom (the number of failures observed). With slight modification for our purposes we invert the inequality and substitute *F* (fluence) in the place of *T*:

$$MFTF = \frac{2nF}{\chi^2_{2(d+1); 100(1-\frac{\alpha}{2})}} \tag{2}$$

Where now *MFTF* is mean-fluence-to-failure and *F* is the test fluence, and as before,  $\chi^2$  is the chi-square distribution evaluated at  $100(1 - \alpha / 2)$  confidence and where *d* is the degrees-of-freedom (the number of failures observed). The inverse relation between *MTTF* and failure rate is mirrored with the *MFTF*. Thus the upper-bound cross-section is obtained by inverting the *MFTF*:

$$\sigma = \frac{\chi^2_{2(d+1); 100(1-\frac{\alpha}{2})}}{2nF} \tag{3}$$

Assume that all tests are terminated at a total fluence of  $10^6$  ions/cm<sup>2</sup>. Also assume there are a number of devices with very different performances that are tested under identical conditions. Assume a 95% confidence level ( $\sigma = 0.05$ ). Note that as  $d$  increases from 0 events to 100 events the actual confidence interval becomes smaller, indicating that the range of values of the true value of the population parameter (in this case the cross-section) is approaching the mean value + 1 standard deviation. This makes sense when one considers that as more events are observed the statistics are improved such that uncertainty in the actual device performance is reduced.

**Table 3. Experimental Example Calculation of MFTF and  $\sigma$  Using a 95% Confidence Interval<sup>(1)</sup>**

Degrees-of-Freedom (d)	2(d + 1)	$\chi^2$ @ 95%	Calculated Cross Section (cm <sup>2</sup> )		
			Upper-Bound @ 95% Confidence	Mean	Average + Standard Deviation
0	2	7.38	3.69E-06	0.00E+00	0.00E+00
1	4	11.14	5.57E-06	1.00E-06	2.00E-06
2	6	14.45	7.22E-06	2.00E-06	3.41E-06
3	8	17.53	8.77E-06	3.00E-06	4.73E-06
4	10	20.48	1.02E-05	4.00E-06	6.00E-06
5	12	23.34	1.17E-05	5.00E-06	7.24E-06
10	22	36.78	1.84E-05	1.00E-05	1.32E-05
50	102	131.84	6.59E-05	5.00E-05	5.71E-05
100	202	243.25	1.22E-04	1.00E-04	1.10E-04

<sup>(1)</sup> Using a 95% confidence interval for several different observed results ( $d = 0, 1, 2, \dots, 100$  observed events during fixed-fluence tests) assuming  $10^6$  ions/cm<sup>2</sup> for each test. Note that as the number of observed events increases the confidence interval approaches the mean.

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## References

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- (1) M. Shoga and D. Binder, "Theory of Single Event Latchup in Complementary Metal-Oxide Semiconductor Integrated Circuits", *IEEE Trans. Nucl. Sci.*, Vol. 33(6), Dec. 1986, pp. 1714-1717.
- (2) G. Bruguier and J. M. Palau, "Single particle-induced latchup", *IEEE Trans. Nucl. Sci.*, Vol. 43(2), Mar. 1996, pp. 522-532.
- (3) TAMU Radiation Effects Facility website. <http://cyclotron.tamu.edu/ref/>
- (4) "The Stopping and Range of Ions in Matter" (SRIM) software simulation tools website. [www.srim.org/index.htm#SRIMMENU](http://www.srim.org/index.htm#SRIMMENU)
- (5) D. Kececioglu, "Reliability and Life Testing Handbook", Vol. 1, PTR Prentice Hall, New Jersey, 1993, pp. 186-193.
- (6) ISDE CRÉME-MC website. <https://creme.isde.vanderbilt.edu/CREME-MC>
- (7) A. J. Tylka, J. H. Adams, P. R. Boberg, et al., "CREME96: A Revision of the Cosmic Ray Effects on Micro-Electronics Code", *IEEE Trans. on Nucl. Sci.*, Vol. 44(6), Dec. 1997, pp. 2150-2160.
- (8) A. J. Tylka, W. F. Dietrich, and P. R. Boberg, "Probability distributions of high-energy solar-heavy-ion fluxes from IMP-8: 1973-1996", *IEEE Trans. on Nucl. Sci.*, Vol. 44(6), Dec. 1997, pp. 2140-2149.

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