

# TMCS1126 Precision 500kHz Hall-Effect Current Sensor With $\pm 1100\text{V}$ Reinforced Isolation Working Voltage, Overcurrent Detection and Ambient Field Rejection

## 1 Features

- High continuous current capability:  $82\text{ A}_{\text{RMS}}$
- Robust reinforced isolation
  - Withstand isolation voltage:  $5000\text{ V}_{\text{RMS}}$
  - Reinforced working voltage:  $1100\text{ V}_{\text{DC}}$
- High accuracy
  - Sensitivity error:  $\pm 0.1\%$
  - Sensitivity drift:  $\pm 20\text{ ppm}/^\circ\text{C}$
  - Offset error:  $\pm 0.2\text{ mV}$
  - Offset drift:  $\pm 2\text{ }\mu\text{V}/^\circ\text{C}$
  - Non-linearity:  $\pm 0.1\%$
- Low lifetime drift:  $\pm 0.5\%$  (maximum)
- High immunity to external magnetic fields
- Precision zero-current reference output
- Signal bandwidth:  $500\text{ kHz}$
- Low propagation delay:  $95\text{ ns}$
- Fast overcurrent detection response:  $100\text{ ns}$
- Operating supply range:  $3\text{ V}$  to  $5.5\text{ V}$
- Bidirectional and unidirectional current sensing
- Multiple sensitivity options:
  - TMCS1126x6x:  $15\text{ mV/A}$
  - TMCS1126x1x:  $25\text{ mV/A}$
  - TMCS1126x7x:  $30\text{ mV/A}$
  - TMCS1126x9x:  $33\text{ mV/A}$
  - TMCS1126x8x:  $40\text{ mV/A}$
  - TMCS1126x2x:  $50\text{ mV/A}$
  - TMCS1126x3x:  $75\text{ mV/A}$
  - TMCS1126x4x:  $100\text{ mV/A}$
  - TMCS1126x5x:  $150\text{ mV/A}$
- Safety related certifications (planned)
  - UL 1577 Component Recognition Program
  - IEC/CB 62368-1

## 2 Applications

- [Solar Energy](#)
- [EV charging](#)
- [Power supplies](#)
- [Industrial AC/DC](#)

## 3 Description

The TMCS1126 is a galvanically isolated Hall-effect current sensor with industry leading isolation and accuracy. An output voltage proportional to the input current is provided with excellent linearity and low drift at all sensitivity options. Precision signal conditioning circuitry with built-in drift compensation is capable of less than 1.45% maximum total error over temperature and lifetime with no system level calibration, or less than 1% maximum total error including both lifetime and temperature drift with a one-time calibration at room temperature.

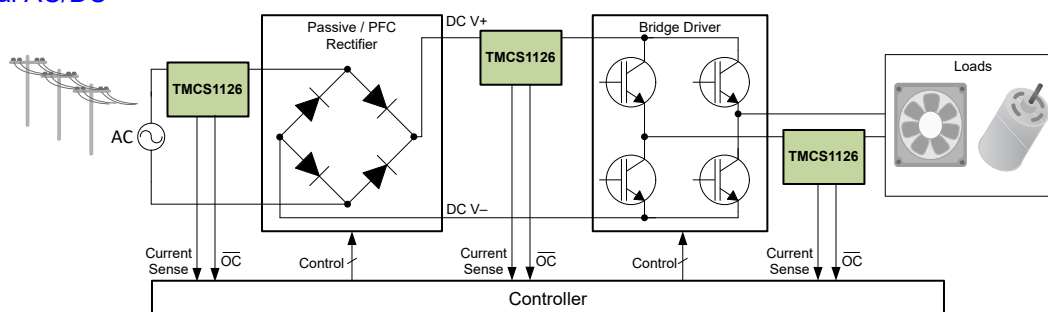
AC or DC input current flows through an internal conductor generating a magnetic field measured by integrated on-chip Hall-effect sensors. Core-less construction eliminates the need for magnetic concentrators. Differential Hall sensors reject interference from stray external magnetic fields. Low conductor resistance increases measurable current ranges up to  $\pm 103\text{ A}$  while minimizing power loss and easing thermal dissipation requirements. Insulation capable of withstanding  $5000\text{ V}_{\text{RMS}}$ , coupled with minimum  $8.1\text{ mm}$  creepage and clearance provide up to  $1100\text{ V}_{\text{DC}}$  reliable lifetime reinforced working voltage. Integrated shielding enables excellent common-mode rejection and transient immunity.

Fixed sensitivity allows the device to operate from a single  $3\text{ V}$  to  $5.5\text{ V}$  power supply, eliminating ratiometry errors and improving supply noise rejection. TI provides the TMCS1126xxB as a lower-cost option.

### Package Information<sup>(1)</sup>

PART NUMBER	PACKAGE	PACKAGE SIZE <sup>(2)</sup>
TMCS1126	DVG (SOIC, 10)	$10.3\text{ mm} \times 10.3\text{ mm}$

- (1) For all available packages, see [Section 12](#).  
 (2) The package size (length  $\times$  width) is a nominal value and includes pins, where applicable.



**Typical Application**



An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. ADVANCE INFORMATION for preproduction products; subject to change without notice.

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## 4 Device Comparison

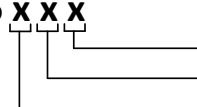
**Table 4-1. Device Comparison**

PRODUCT	SENSITIVITY	ZERO CURRENT OUTPUT VOLTAGE	I <sub>IN</sub> LINEAR MEASUREMENT RANGE <sup>(1)</sup>	
			V <sub>S</sub> = 5 V	V <sub>S</sub> = 3.3 V
TMCS1126A1x	25 mV/A	2.5 V	±96 A <sup>(2)</sup>	–96 A to 28 A <sup>(2)</sup>
TMCS1126A7x	30 mV/A		±80 A <sup>(2)</sup>	–80 A to 23.3 A <sup>(2)</sup>
TMCS1126A8x	40 mV/A		±60 A <sup>(2)</sup>	–60 A to 17.5 A <sup>(2)</sup>
TMCS1126A2x	50 mV/A		±48 A <sup>(2)</sup>	–48 A to 14 A <sup>(2)</sup>
TMCS1126A3x	75 mV/A		±32 A	–32 A to 9.3 A
TMCS1126A4x	100 mV/A		±24 A	–24 A to 7 A
TMCS1126A5x	150 mV/A		±16 A	–16 A to 4.7 A
TMCS1126B6x	15 mV/A	1.65 V	–103.3 A to 216.7 A <sup>(2)</sup>	±103.3 A <sup>(2)</sup>
TMCS1126B1x	25 mV/A		–62 A to 130 A <sup>(2)</sup>	±62 A <sup>(2)</sup>
TMCS1126B9x	33 mV/A		–46.9 A to 98.5 A <sup>(2)</sup>	±46.9 A <sup>(2)</sup>
TMCS1126B2x	50 mV/A		–31 A to 65 A <sup>(2)</sup>	±31 A
TMCS1126B3x	75 mV/A		–20.7 A to 43.3 A <sup>(2)</sup>	±20.7 A
TMCS1126B4x	100 mV/A		–15.5 A to 32.5 A	±15.5 A
TMCS1126B5x	150 mV/A		–10.3 A to 21.7 A	±10.3 A
TMCS1126C1x	25 mV/A	0.33 V	–9.2 A to 183 A <sup>(2)</sup>	–9.2 A to 115 A <sup>(2)</sup>
TMCS1126C2x	50 mV/A		–4.6 A to 91.4 A <sup>(2)</sup>	–4.6 A to 57.4 A <sup>(2)</sup>
TMCS1126C3x	75 mV/A		–3.1 A to 60.9 A <sup>(2)</sup>	–3.1 A to 38.3 A <sup>(2)</sup>
TMCS1126C4x	100 mV/A		–2.3 A to 45.7 A <sup>(2)</sup>	–2.3 A to 28.7 A
TMCS1126C5x	150 mV/A		–1.5 A to 30.5 A	–1.5 A to 19.1 A

- (1) Linear range limited by the maximum output swing to power supply (3V to 5.5V) and ground, not by thermal limitations.  
(2) Current levels must remain below both allowable continuous DC/RMS and transient peak current safe operating areas to not exceed device thermal limits. See the [Safe Operating Area](#) section.

### Part Number Naming Designators :

**TMCS1126 x x x**



A - Hi Grade ; B - Lo Grade  
Sensitivity  
Zero Current Output Voltage

## 5 Pin Configuration and Functions

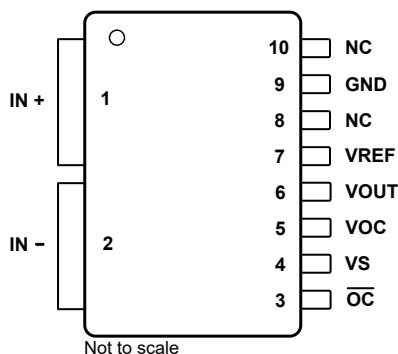


Figure 5-1. DVG Package 10-Pin SOIC Top View

Table 5-1. Pin Functions

PIN		TYPE	DESCRIPTION
NO.	NAME		
1	IN+	Analog Input	Input current positive pin
2	IN–	Analog Input	Input current negative pin
3	$\overline{OC}$	Digital Output	Overcurrent output, open-drain active low. Connect pin to GND if not used.
4	VS	Analog	Power supply
5	VOC	Analog Input	Overcurrent threshold. Sets overcurrent threshold. Connect pin to VS if not used.
6	VOUT	Analog Output	Output voltage
7	VREF	Analog Output	Zero current output voltage reference
8	NC	-	Reserved. Pin can be connected to GND, VS, or left floating.
9	GND	Analog	Ground
10	NC	-	Reserved. Pin can be connected to GND, VS, or left floating.

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>S</sub>	Supply voltage	GND – 0.3	6	V
	Analog input	VOC	GND – 0.3 (V <sub>S</sub> ) + 0.3	V
	Analog output	VOUT, VREF		
	Digital output	$\overline{OC}$		
	No Connect	NC		
T <sub>J</sub>	Junction temperature	–65	165	°C
T <sub>stg</sub>	Storage temperature	–65	165	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

### 6.2 ESD Ratings

			VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±1000	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.  
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V <sub>S</sub>	Operating supply voltage	3	5	5.5	V
T <sub>A</sub> <sup>(1)</sup>	Operating free-air temperature	–40		125	°C

- (1) Input current safe operating area is constrained by junction temperature. Recommended condition based on use with the [TMCS1126xEVM](#). Input current rating is derated for elevated ambient temperatures.

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TMCS1126 <sup>(2)</sup>	UNIT
		DVG (SOIC-W-10)	
		10 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	27.9	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	26.8	
R <sub>θJB</sub>	Junction-to-board thermal resistance	10.1	
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	4.4	
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	8.3	

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.  
(2) Applies when device is mounted on [TMCS1126xEVM](#). For more details, see the [Safe Operating Area](#) section.

## 6.5 Insulation Specifications

PARAMETER		TEST CONDITIONS	VALUE	UNIT
<b>GENERAL</b>				
CLR	External clearance <sup>(1)</sup>	Shortest terminal-to-terminal distance through air	8.1	mm
CPG	External creepage <sup>(1)</sup>	Shortest terminal-to-terminal distance across the package surface	8.1	mm
CTI	Comparative tracking index	DIN EN 60112; IEC 60112	600	V
	Material group	According to IEC 60664-1	I	
	Overvoltage category per IEC 60664-1	Rated mains voltage $\leq 150 V_{RMS}$	I-IV	
		Rated mains voltage $\leq 300 V_{RMS}$	I-IV	
		Rated mains voltage $\leq 600 V_{RMS}$	I-IV	
$V_{IORM}$	Maximum repetitive peak isolation voltage	AC voltage (bipolar), Basic Isolation	2070	$V_{PK}$
		AC voltage (bipolar), Reinforced Isolation	1100	
$V_{IOWM}$	Maximum basic isolation working voltage	AC voltage (sine wave)	1464	$V_{RMS}$
		DC voltage	2070	$V_{DC}$
	Maximum reinforced isolation working voltage	AC voltage (sine wave)	778	$V_{RMS}$
		DC voltage	1100	$V_{DC}$
$V_{IOTM}$	Maximum transient isolation voltage	$V_{TEST} = \sqrt{2} \times V_{ISO}$ , $t = 60$ s (qualification); $V_{TEST} = 1.2 \times V_{IOTM}$ , $t = 1$ s (100% production)	7071	$V_{PK}$
$V_{IOSM}$	Maximum surge isolation voltage <sup>(2)</sup>	Test method per IEC 62368-1, 1.2/50 $\mu$ s waveform, $V_{TEST} = 1.3 \times V_{IOSM}$ (qualification)	10000	$V_{PK}$
$q_{pd}$	Apparent charge <sup>(3)</sup>	Method a: After I/O safety test subgroup 2/3, $V_{ini} = V_{IOTM}$ , $t_{ini} = 60$ s; $V_{pd(m)} = 1.2 \times V_{IORM}$ , $t_m = 10$ s	$\leq 5$	pC
		Method a: After environmental tests subgroup 1, $V_{ini} = V_{IOTM}$ , $t_{ini} = 60$ s; $V_{pd(m)} = 1.2 \times V_{IORM}$ , $t_m = 10$ s	$\leq 5$	
		Method b3: At routine test (100% production) and preconditioning (type test) $V_{ini} = 1.2 \times V_{IOTM}$ , $t_{ini} = 1$ s; $V_{pd(m)} = 1.2 \times V_{IOTM}$ , $t_m = 1$ s	$\leq 5$	
$C_{IO}$	Barrier capacitance, input to output <sup>(4)</sup>	$V_{IO} = 0.4 \sin(2\pi f t)$ , $f = 1$ MHz	0.6	pF
$R_{IO}$	Isolation resistance, input to output <sup>(4)</sup>	$V_{IO} = 500$ V, $T_A = 25^\circ\text{C}$	$>10^{12}$	$\Omega$
		$V_{IO} = 500$ V, $100^\circ\text{C} \leq T_A \leq 125^\circ\text{C}$	$>10^{11}$	$\Omega$
		$V_{IO} = 500$ V at $T_S = 150^\circ\text{C}$	$>10^9$	$\Omega$
	Pollution degree		2	
<b>UL 1577</b>				
$V_{ISO}$	Withstand isolation voltage	$V_{TEST} = V_{ISO}$ , $t = 60$ s (qualification); $V_{TEST} = 1.2 \times V_{ISO}$ , $t = 1$ s (100% production)	5000	$V_{RMS}$

- (1) Apply creepage and clearance requirements according to the specific equipment isolation standards of an application. Take care to maintain the creepage and clearance distance of the board design to make sure that the mounting pads of the isolator on the printed-circuit board do not reduce this distance. Creepage and clearance on a printed-circuit board become equal in certain cases. Techniques such as inserting grooves, ribs, or both on a printed circuit board are used to help increase these specifications.
- (2) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.
- (3) Apparent charge is electrical discharge caused by a partial discharge (pd).
- (4) All pins on each side of the barrier tied together creating a two-terminal device

## 6.6 Electrical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = 5\text{V}$  on TMCS1126Axx,  $V_S = 3.3\text{V}$  on TMCS1126Bxx and TMCS1126Cxx (unless otherwise noted)

PARAMETERS		TEST CONDITIONS	MIN	TYP	MAX	UNIT
INPUT						
R <sub>IN</sub>	Input Conductor Resistance	IN+ to IN–	0.7			mΩ
R <sub>IN</sub>	Input conductor resistance temperature drift	T <sub>A</sub> = −40°C to +125°C	2.1			μΩ/°C
I <sub>IN,MAX</sub>	Maximum Continuous Input Current <sup>(1)</sup>	T <sub>A</sub> = 25°C	82			A <sub>RMS</sub>
		T <sub>A</sub> = 125°C	44			
OUTPUT						
S	Sensitivity	TMCS1126x6x	15			mV/A
		TMCS1126x1x	25			
		TMCS1126x7x	30			
		TMCS1126x9x	33			
		TMCS1126x8x	40			
		TMCS1126x2x	50			
		TMCS1126x3x	75			
		TMCS1126x4x	100			
		TMCS1126x5x	150			
	Sensitivity Error	TMCS1126xxA, 0.05 V ≤ V <sub>OUT</sub> ≤ V <sub>S</sub> − 0.2 V	±0.1%		±0.45%	
		TMCS1126xxB, 0.05 V ≤ V <sub>OUT</sub> ≤ V <sub>S</sub> − 0.2 V	±0.3%		±1%	
	Sensitivity Thermal Drift	TMCS1126xxA, 0.05 V ≤ V <sub>OUT</sub> ≤ V <sub>S</sub> − 0.2 V, T <sub>A</sub> = −40°C to +125°C	±20		±50	ppm/°C
		TMCS1126xxB, 0.05 V ≤ V <sub>OUT</sub> ≤ V <sub>S</sub> − 0.2 V, T <sub>A</sub> = −40°C to +125°C	±40		±100	
	Sensitivity Lifetime Drift	0.05 V ≤ V <sub>OUT</sub> ≤ V <sub>S</sub> − 0.2 V	±0.2%		±0.5%	
	Nonlinearity Error	TMCS1126xxA, V <sub>OUT</sub> = 0.1 V to V <sub>S</sub> − 0.1 V	±0.1%			
		TMCS1126xxB, V <sub>OUT</sub> = 0.1 V to V <sub>S</sub> − 0.1 V	±0.2%			
V <sub>OUT,0A</sub>	Zero Current Output Voltage	TMCS1126Axx, I <sub>IN</sub> = 0A	2.5			V
		TMCS1126Bxx, I <sub>IN</sub> = 0A	1.65			
		TMCS1126Cxx, I <sub>IN</sub> = 0A	0.33			
V <sub>OE</sub>	Output Voltage Offset Error: Grade A	TMCS1126x6A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.2		±1	mV
		TMCS1126x1A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.2		±1	
		TMCS1126x7A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.3		±1.5	
		TMCS1126x9A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.3		±1.5	
		TMCS1126x8A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.3		±1.5	
		TMCS1126x2A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.3		±1.5	
		TMCS1126x3A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.4		±2	
		TMCS1126x4A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.5		±2.5	
		TMCS1126x5A, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.6		±3	
	Output Voltage Offset Error: Grade B	TMCS1126x6B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.7		±2	
		TMCS1126x1B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.7		±2	
		TMCS1126x7B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.8		±2.5	
		TMCS1126x9B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.8		±2.5	
		TMCS1126x8B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.8		±2.5	
		TMCS1126x2B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±0.8		±2.5	
		TMCS1126x3B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±1		±3	
		TMCS1126x4B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±1.5		±4.5	
		TMCS1126x5B, V <sub>OUT,0A</sub> − V <sub>REF</sub> , I <sub>IN</sub> = 0A	±2		±6	

at  $T_A = 25^\circ\text{C}$ ,  $V_S = 5\text{V}$  on TMCS1126Axx,  $V_S = 3.3\text{V}$  on TMCS1126Bxx and TMCS1126Cxx (unless otherwise noted)

PARAMETERS		TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Output Voltage Offset Drift: Grade A	TMCS1126x6A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 2$	$\pm 10$	$\mu V/^{\circ}C$
		TMCS1126x1A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 2$	$\pm 10$	
		TMCS1126x7A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 5$	$\pm 15$	
		TMCS1126x9A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 5$	$\pm 15$	
		TMCS1126x8A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 5$	$\pm 15$	
		TMCS1126x2A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 5$	$\pm 15$	
		TMCS1126x3A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 10$	$\pm 35$	
		TMCS1126x4A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 10$	$\pm 35$	
		TMCS1126x5A, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 12$	$\pm 40$	
	Output Voltage Offset Drift: Grade B	TMCS1126x6B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 10$	$\pm 30$	
		TMCS1126x1B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 10$	$\pm 30$	
		TMCS1126x7B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 15$	$\pm 40$	
		TMCS1126x9B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 15$	$\pm 40$	
		TMCS1126x8B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 15$	$\pm 40$	
		TMCS1126x2B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 15$	$\pm 40$	
		TMCS1126x3B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 20$	$\pm 55$	
		TMCS1126x4B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 30$	$\pm 70$	
		TMCS1126x5B, $V_{OUT,0A} - V_{REF}$ , $I_{IN} = 0A$ , $T_A = -40^{\circ}C$ to $125^{\circ}C$		$\pm 40$	$\pm 80$	
PSRR	Power Supply Rejection Ratio: Grade A	TMCS1126xxA, Input Referred, $V_S = 3V$ to $5.5V$ , $T_A = -40^{\circ}C$ to $+125^{\circ}C$		$\pm 10$	$\pm 45$	mA/V
	Power Supply Rejection Ratio: Grade B	TMCS1126xxB, Input Referred, $V_S = 3V$ to $5.5V$ , $T_A = -40^{\circ}C$ to $+125^{\circ}C$		$\pm 40$	$\pm 80$	
CMTI	Common Mode Transient Immunity	$V_{CM} = 1000V$ , $\Delta V_{OUT} < 200mV$ , $1\mu s$	75	150		kV/ $\mu s$
CMRR	Common Mode Rejection Ratio	Input Referred, DC to 60Hz		5		$\mu A/V$
CMFR	Common Mode Field Rejection	Uniform External Magnetic Field, Input Referred, DC to 1kHz			10	mA/mT
	Input Noise Density	Input Referred, Full Bandwidth		150		$\mu A/\sqrt{Hz}$
$C_{L,MAX}$	Maximum capacitive load	VOUT to GND		4.7		nF
	Short circuit output current	VOUT short to GND, short to $V_S$		50		mA
Swing $_{VS}$	Swing to $V_S$ power supply rail	$R_L = 10k\Omega$ to GND, $T_A = -40^{\circ}C$ to $+125^{\circ}C$	$V_S - 0.02$	$V_S - 0.05$		V
Swing $_{GND}$	Swing to GND		$V_{GND} + 5$	$V_{GND} + 10$		mV
BANDWIDTH & RESPONSE						
BW	Analog Bandwidth	- 3dB Gain		500		kHz
SR	Slew Rate <sup>(2)</sup>	Output rate of change between reaching 10% and 90% of final value as shown in Figure 8-2 with a 100ns input step.		4		V/ $\mu s$
$t_r$	Response Time <sup>(2)</sup>	Time between input and output reaching 90% of final values, as shown in Figure 8-2 with a 100ns input step and a 1V output transition.		500		ns



at  $T_A = 25^\circ\text{C}$ ,  $V_S = 5\text{V}$  on TMCS1126Axx,  $V_S = 3.3\text{V}$  on TMCS1126Bxx and TMCS1126Cxx (unless otherwise noted)

PARAMETERS		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_r$	Propagation Delay <sup>(2)</sup>	Time between input and output reaching 10% of final values as shown in Figure 8-2 with a 100ns input step and a 1V output transition.		95		ns
	Current Overload Recovery Time			300		ns
<b>INTEGRATED REFERENCE</b>						
$V_{REF}$	Reference Output Voltage	TMCS1126Axx		2.5		V
		TMCS1126Bxx		1.65		
		TMCS1126Cxx		0.33		
	Reference Output Voltage Error: Grade A	TMCS1126AxA, $V_S = 5\text{V}$		$\pm 0.02\%$	$\pm 0.15\%$	
		TMCS1126BxA, $V_S = 3.3\text{V}$		$\pm 0.02\%$	$\pm 0.15\%$	
		TMCS1126CxA, $V_S = 3.3\text{V}$		$\pm 0.05\%$	$\pm 0.2\%$	
	Reference Output Voltage Error: Grade B	TMCS1126AxB, $V_S = 5\text{V}$		$\pm 0.1\%$	$\pm 0.4\%$	
		TMCS1126BxB, $V_S = 3.3\text{V}$		$\pm 0.12\%$	$\pm 0.5\%$	
		TMCS1126CxB, $V_S = 3.3\text{V}$		$\pm 0.2\%$	$\pm 1\%$	
	Reference Output Voltage Drift: Grade A	TMCS1126xxA $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		8	20	ppm/ $^\circ\text{C}$
	Reference Output Voltage Drift: Grade B	TMCS1126xxB $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		15	50	
	Reference Output Voltage PSRR	$V_S = 3\text{V}$ to $5.5\text{V}$		80	200	$\mu\text{V/V}$
	Maximum Reference Output Capacitive Load			20		nF
	Reference Output Voltage Load Regulation	$V_{REF}$ load = $-5\text{mA}$ , $0\text{mA}$ , $+5\text{mA}$		0.2		mV/mA
<b>OVER CURRENT DETECTION</b>						
$V_{OC}$	Over Current Detection Threshold Voltage	$V_{OC} = S \times I_{OC} / 2.5$	0.3		$V_S$	V
$R_{OC}$	Over Current Input Impedance		230			k $\Omega$
	Over Current Hysteresis	TMCS1126x6x		8.3		A
		TMCS1126x1x		4.5		
		TMCS1126x7x		4.2		
		TMCS1126x9x		3.8		
		TMCS1126x8x		3.1		
		TMCS1126x2x		3.5		
		TMCS1126x3x		2.2		
		TMCS1126x4x		1.4		
		TMCS1126x5x		2.7		
	$I_{OC}$ error	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 7\%$	$\pm 15\%$	
	Over Current Detection Response Time	$I_{IN}$ step = $120\%$ of $I_{OC}$		100	250	ns
$OC_{OL}$	Over Current Pull-down Voltage	$I_{OL} = 3\text{mA}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	GND	0.07	0.2	V
ALERT	Output Frequency			8		kHz
	Output Duty Cycle, Active Low	Thermal Alert		80		
		Sensor Alert		50		
		Thermal & Sensor Alert		20		
	ALERT Pull-down Voltage	$I_{OL} = 3\text{mA}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	GND	0.07	0.2	V
<b>POWER SUPPLY</b>						
$V_S$	Supply voltage	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	3.0		5.5	V
$I_Q$	Quiescent current	$T_A = 25^\circ\text{C}$		11	14	mA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			14.5	
	Power on time	Time from $V_S > 3\text{V}$ to valid output		27.5		ms

- (1) Thermally limited by junction temperature. Applies when device mounted on [TMCS1126xEVM](#). For more details, see the [Safe Operating Area](#) section.
- (2) Refer to the [Transient Response](#) section for details on transient response of the device.

## 7 Parameter Measurement Information

### 7.1 Accuracy Parameters

The ideal first-order transfer function of the TMCS1126 is given by Equation 1, where the output voltage is a linear function of input current. The accuracy of the device is quantified both by the error terms in the transfer function parameters, as well as by nonidealities that introduce additional error terms not in the simplified linear model. See [Total Error Calculation Examples](#) for example calculations of total error, including all device error terms.

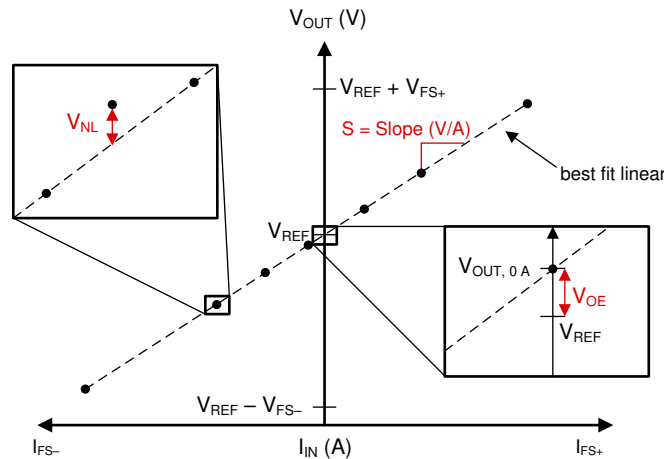
$$V_{OUT} = (I_{IN} \times S) + V_{REF} \quad (1)$$

where

- $V_{OUT}$  is the analog output voltage.
- $I_{IN}$  is the isolated input current.
- $S$  is the sensitivity of the device.
- $V_{REF}$  is the zero current reference output voltage for the device variant.

#### 7.1.1 Sensitivity Error

Sensitivity is the proportional change in the sensor output voltage due to a change in the input conductor current. This sensitivity is the slope of the first-order transfer function of the sensor (see [Figure 7-1](#)). The sensitivity of the TMCS1126 is tested and calibrated at the factory for high accuracy.



**Figure 7-1. Sensitivity, Offset, and Nonlinearity Error**

Sensitivity error  $e_S$  is the deviation from ideal sensitivity and is defined in Equation 2 as the variation of the best-fit measured sensitivity from the ideal sensitivity.

$$e_S = \frac{(S_{fit} - S_{ideal})}{S_{ideal}} \quad (2)$$

where

- $e_S$  is the sensitivity error.
- $S_{fit}$  is the best fit sensitivity.
- $S_{ideal}$  is the ideal sensitivity.

Sensitivity thermal drift  $S_{drift, therm}$  is the change in sensitivity with temperature and is reported in ppm/°C. To calculate sensitivity error at any given temperature  $T$  use Equation 3 to multiply the sensitivity thermal drift by the change in temperature from 25°C and add it to sensitivity error at 25°C.

$$e_{S, \Delta T} = e_{S, 25^\circ C} + (S_{drift, therm} \times \Delta T) \quad (3)$$

where

- $S_{\text{drift,therm}}$  is the sensitivity drift over temperature in ppm/°C.
- $\Delta T$  is the change in device temperature from 25°C.

Sensitivity lifetime drift  $S_{\text{drift,life}}$  is the change in sensitivity due to operational and environmental stresses over the entire lifetime of the device, and is reported as a worst-case percentage change in sensitivity over lifetime at 25°C.

### 7.1.2 Offset Error and Offset Error Drift

Offset error is the deviation from the ideal output with zero input current and most often limits measurement accuracy at low input current levels. Offset error can be referred to the output as offset voltage error or referred to the input as offset current error. When divided by device sensitivity,  $S$ , output voltage offset error  $V_{\text{OE}}$  is input referred as input current offset error  $I_{\text{OS}}$  (see Equation 4). Offset error referred to the input (RTI) allows for more direct comparisons or offset error with input current. Regardless of whether offset error is referred to the input as current offset error  $I_{\text{OS}}$ , or to the output as voltage offset error  $V_{\text{OE}}$ , offset error is a single error source and should only be included once in either input referred, or output referred error calculations.

$$I_{\text{OS}} = \frac{V_{\text{OE}}}{S} \quad (4)$$

As shown in Figure 7-1, the output voltage offset error  $V_{\text{OE}}$  of the TMCS1126 is the difference between the zero current output voltage  $V_{\text{OUT,0A}}$  and the zero current output reference voltage  $V_{\text{REF}}$  (see Equation 5).

$$V_{\text{OE}} = V_{\text{OUT,0A}} - V_{\text{REF}} \quad (5)$$

The output offset error  $V_{\text{OE}}$  includes magnetic offset error in the Hall sensor, offset voltage error in the signal chain, and offset error in the internal zero current output reference voltage  $V_{\text{REF}}$ . The internal zero current output reference voltage is brought out to pin VREF so that errors in the internal reference voltage as well as errors introduced at the system level can be removed.

Offset drift is the change in the offset as a function of temperature  $T$ . Output offset drift is reported in  $\mu\text{V}/^\circ\text{C}$ . To calculate offset error at any given temperature, multiply the offset drift by the change in temperature and add it to offset error at 25°C (see Equation 6).

$$V_{\text{OE},\Delta T} = V_{\text{OE},25^\circ\text{C}} + (V_{\text{OE,drift}} \times \Delta T) \quad (6)$$

where

- $V_{\text{OE,drift}}$  is the output voltage offset drift with temperature in  $\mu\text{V}/^\circ\text{C}$ .
- $\Delta T$  is the change in device temperature from 25°C.

### 7.1.3 Nonlinearity Error

Nonlinearity is the deviation of the output voltage from a linear relationship to the input current. Nonlinearity voltage, as shown in Figure 7-1, is the maximum voltage deviation from the best-fit line based on measured parameters (see Equation 7).

$$V_{\text{NL}} = V_{\text{OUT,meas}} - [(I_{\text{meas}} \times S_{\text{fit}}) + V_{\text{OUT,0A}}] \quad (7)$$

where

- $V_{\text{OUT,meas}}$  is the voltage output at maximum deviation from best fit.
- $I_{\text{meas}}$  is the input current at maximum deviation from best fit.
- $S_{\text{fit}}$  is the best-fit sensitivity of the device.
- $V_{\text{OUT,0A}}$  is the device zero current output voltage.

Nonlinearity error for the TMCS1126 is specified as a percentage of the full-scale output range,  $V_{\text{FS}}$  (see Equation 8).

$$e_{NL} = \frac{V_{NL}}{V_{FS}} \quad (8)$$

#### 7.1.4 Power Supply Rejection Ratio

Power supply rejection ratio (PSRR) is the change in device offset due to variations in supply voltage. Use [Equation 9](#) to calculate input referred offset errors caused by supply variations on TMCS1126Axx variants. Use [Equation 10](#) to calculate input referred offset errors caused by supply variations on TMCS1126Bxx and TMCS1126Cxx variants.

$$e_{PSRR} = \frac{PSRR \times (V_S - 5)}{I_{IN}} \quad (9)$$

$$e_{PSRR} = \frac{PSRR \times (V_S - 3.3)}{I_{IN}} \quad (10)$$

where

- PSRR is the input referred power supply rejection ratio in mA/V.
- $V_S$  is the operational supply voltage.

#### 7.1.5 Common-Mode Rejection Ratio

Common-mode rejection ratio (CMRR) quantifies the effective input current error due to a varying voltage on the isolated input of the device. Due to magnetic coupling and galvanic isolation of the current signal, the TMCS1126 has very high rejection of input common-mode voltage. Use [Equation 11](#) to calculate the percent error contribution from the input common-mode variation.

$$e_{CMRR} = \frac{CMRR \times V_{CM}}{I_{IN}} \quad (11)$$

where

- CMRR is the input-referred common-mode rejection in  $\mu A/V$ .
- $V_{CM}$  is the operational AC or DC voltage on the input of the device.

#### 7.1.6 External Magnetic Field Errors

The TMCS1126 suppresses interference from external magnetic fields generated by adjacent high-current carrying conductors, nearby motors, magnets, or any other sources of stray magnetic fields. Common-mode field rejection (CMFR) quantifies the effective input-referred error caused by stray magnetic fields. Use [Equation 12](#) to calculate percentage error contributions from stray external magnetic fields,  $B_{EXT}$ .

$$e_{Bext} = \frac{B_{EXT} \times CMFR}{I_{IN}} \quad (12)$$

where

- $B_{EXT}$  is the intensity of the external magnetic field in mT.
- CMRF is the common-mode field rejection in mA/mT.

## 7.2 Transient Response Parameters

Critical TMCS1126 transient step response parameters are shown in Figure 7-2. Propagation delay,  $t_{pd}$ , is the time period between the input current waveform reaching 10% of its final value and the output voltage,  $V_{OUT}$ , reaching 10% of its final value. Response time,  $t_r$ , is the time period between the input current reaching 90% of its final value and the output voltage reaching 90% of its final value, for an input current step sufficient to cause a 1V change in the output voltage. Slew rate, SR, is defined as the rate of change between the output voltage reaching 10% and 90% of its final value during the sufficiently fast input current step.

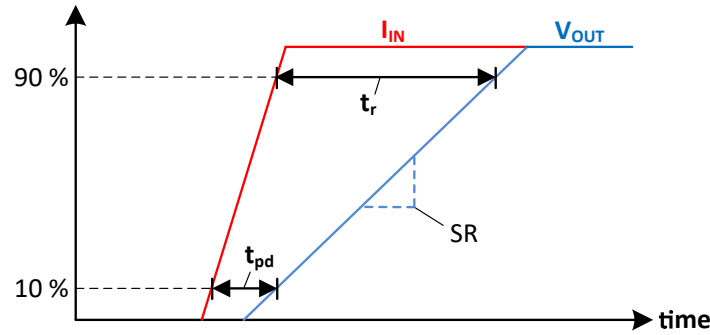


Figure 7-2. Transient Step Response

### 7.2.1 CMTI, Common-Mode Transient Immunity

CMTI is the capability of the device to tolerate a rising or falling voltage step on the input without coupling significant disturbance on the output signal. The device is specified for the maximum common-mode transition rate under which the output signal will not experience a disturbance greater than 200-mV lasting longer than 1  $\mu$ s. Higher edge rates than the specified CMTI can be supported with sufficient filtering or blanking time after common-mode transitions.

## 7.3 Safe Operating Area

The isolated input current safe operating area (SOA) of the TMCS1126 is constrained by self-heating due to power dissipation in the input conductor. Depending upon the use case, the SOA is constrained by multiple conditions, including exceeding maximum junction temperature, Joule heating in the leadframe, or leadframe fusing under extremely high currents. These mechanisms depend on input current pulse duration, amplitude, and device thermal states.

Current SOA strongly depends on the thermal environment and design of the system-level printed circuit board(PCB). Multiple thermal variables control the transfer of heat from the device to the surrounding environment, including air flow, ambient temperature, and PCB construction and design. All ratings are for a single TMCS1126 device mounted on the [TMCS1126xEVM](#), or equivalent PCB design with no air flow under specified ambient temperature conditions. Device use profiles must satisfy continuous current conduction SOA capabilities for the thermal environment planned for system operation.

### 7.3.1 Continuous DC or Sinusoidal AC Current

The longest thermal time constants of device packaging and PCBs are in the order of seconds; therefore, any continuous DC or sinusoidal AC periodic waveform with a frequency higher than 1 Hz can be evaluated based on the RMS continuous-current levels. The continuous-current capability has a strong dependence upon the operating ambient temperature range expected in operation. [Figure 7-3](#) shows the maximum continuous current-handling capability of the device when mounted on the [TMCS1126xEVM](#). Current capability falls off at higher ambient temperatures because of the reduced thermal transfer from junction-to-ambient and increased power dissipation in the leadframe. By improving the thermal design of an application, the SOA can be extended to higher currents at elevated temperatures. Using larger and heavier copper power planes, providing air flow over the board, or adding heat sinking structures to the area of the device can all improve thermal performance.

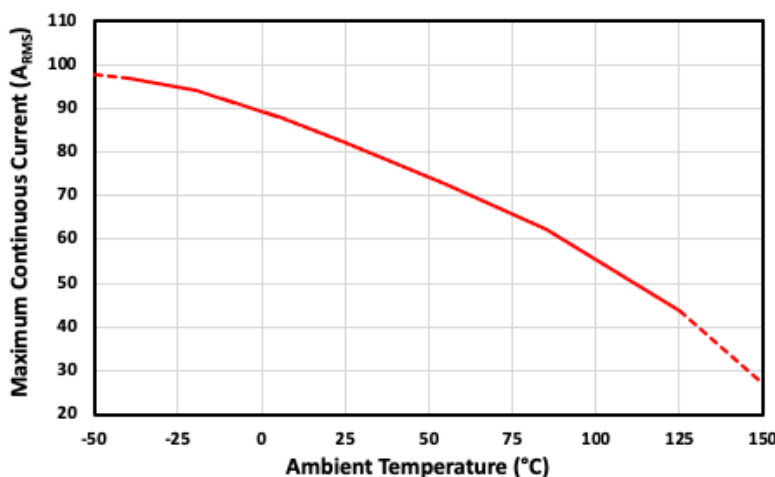


Figure 7-3. Maximum Continuous RMS Current vs Ambient Temperature



of device lifetime working voltages follow the VDE 0884-11 standard for reinforced insulation, requiring time-dependent dielectric breakdown (TDDb) data-projection failure rates of less than 1 part per million (ppm), and a minimum insulation lifetime of 30 years. The VDE standard also requires additional safety margins of 20% for working voltage, and 30% for insulation lifetime, translating into a minimum required lifetime of 39 years at 900 V<sub>RMS</sub> for the TMCS1126.

### 8.3.3 Ambient Field Rejection

The TMCS1126 is designed to provide high levels of current measurement accuracy in harsh environments. Immunity to interference from stray magnetic fields allows for use in close proximity to high current carrying traces, motor windings, inductors, or any other erroneous source of stray magnetic fields. The TMCS1126 incorporates differential Hall sensors that are strategically located and configured to reject interference from stray external magnetic fields. Ambient Field Rejection (AFR) limited only by Hall element matching and package leadframe coupling reduces errors from stray magnetic fields.

### 8.3.4 High-Precision Signal Chain

The TMCS1126 uses a precision, low-drift signal chain with proprietary sensor linearization techniques to provide a highly accurate and stable current measurement across the full temperature range and lifetime of the device. The device is fully tested and calibrated at the factory to account for any variations in either silicon processing, assembly or packaging of the device. The full signal chain provides a fixed sensitivity voltage output that is proportional to the current flowing through the leadframe of the isolated input.

#### 8.3.4.1 Temperature Stability

The TMCS1126 includes a proprietary temperature compensation technique which results in significantly improved parametric drift across the full temperature range. This compensation technique accounts for changes in ambient temperature, self-heating, and package stress. A zero-drift signal chain architecture along with Hall sensor temperature compensation methods enable stable sensitivity while minimizing offset errors across temperature. System-level performance is drastically improved across required operating conditions.

#### 8.3.4.2 Lifetime and Environmental Stability

In addition to large thermal drift, typical magnetic current sensors suffer an additional 2% to 3% drift in sensitivity due to aging over the lifetime of the device. The same proprietary compensation techniques used in the TMCS1126 to reduce temperature drift are also used to greatly reduce lifetime drift due to aging from stress and environmental conditions especially at high operating temperatures. As shown in the [Electrical Characteristics](#), the TMCS1126 has industry leading lifetime sensitivity drift realized after Highly Accelerated Stress Tests (HAST) at 130°C and 85% relative humidity (RH) during standard three lot AEC-Q100 qualifications. Low sensitivity and offset drift within the bounds specified in the [Electrical Characteristics](#) are also observed after 1000 hour, 125°C high temperature operating life stress tests are performed as prescribed by AEC-Q100 qualifications. These tests mimic typical device lifetime operation, and show device performance variation due to aging is vastly improved compared with typical magnetic current sensors.

### 8.3.5 Internal Reference Voltage

The TMCS1126 has a precision internal reference that determines the zero current output voltage, V<sub>OUT,0A</sub>. Overall current sensing dynamic range can be optimized by choosing either of the three different zero current output voltage options listed in the [Device Comparison](#) table. These extremely low-drift precision zero current reference options listed in [Equation 13](#), [Equation 14](#), and [Equation 15](#) provide for precise bidirectional or unidirectional current measurements using various supply voltages ranging between 3.0 V to 5.5 V.

- TMCS1126Axx → V<sub>OUT,0A</sub> = V<sub>REF</sub> = 2.5 V (13)

- TMCS1126Bxx → V<sub>OUT,0A</sub> = V<sub>REF</sub> = 1.65 V (14)

- TMCS1126Cxx → V<sub>OUT,0A</sub> = V<sub>REF</sub> = 0.33 V (15)



### 8.3.6 Current-Sensing Measurable Ranges

The zero current reference voltage,  $V_{REF}$ , along with device sensitivity,  $S$ , and supply voltage,  $V_S$ , determine the linear input current measurement range of the device as listed in the [Device Comparison](#) table. The maximum linear output voltage,  $V_{OUT,max}$ , is limited by the exceptional near-to-supply output voltage swing,  $Swing_{VS}$ , of the TMCS1126 as defined in the [Electrical Characteristics](#) table and shown in [Equation 16](#).

$$V_{OUT,max} = V_S - Swing_{VS} \quad (16)$$

The minimum linear output voltage,  $V_{OUT,min}$ , is limited by the exceptional near-to-ground linear output swing,  $Swing_{GND}$ , as is also defined in the [Electrical Characteristics](#) table and shown in [Equation 17](#).

$$V_{OUT,min} = Swing_{GND} \quad (17)$$

Overall maximum dynamic range can be optimized with proper device selection by referring minimum and maximum linear output voltage swing to minimum and maximum linear input current range by dividing output voltage by sensitivity,  $S$  (see [Equation 18](#) and [Equation 19](#)).

$$I_{IN,max+} = \frac{(V_{OUT,max} - V_{OUT,0A})}{S} \quad (18)$$

$$I_{IN,max-} = \frac{(V_{OUT,0A} - V_{OUT,min})}{S} \quad (19)$$

where

- $I_{IN,max+}$  is the maximum linear measurable positive input current.
- $I_{IN,max-}$  is the maximum linear measurable negative input current.
- $S$  is the sensitivity of the device variant.
- $V_{OUT,0A}$  is the appropriate zero current output voltage.

As an example for determining linear input current measurement range, consider the TMCS1126A2A, TMCS1126B2A and TMCS1126C2A, all with 50 mV/A sensitivity as shown in the [Device Comparison](#) table. When used with a 5V supply, the TMCS1126A2A has a balanced  $\pm 48A$  bidirectional linear current measurement range about the 2.5V zero current output reference voltage,  $V_{REF}$ , as shown in [Figure 8-1](#). When used with a 3.3V supply, the TMCS1126B2A has a balanced  $\pm 31A$  bidirectional linear current measurement range about the 1.65V zero current output reference voltage. If used with a 5V supply, the linear current measurement range of the TMCS1126B2A can be extended from  $-31 A$  to  $+65 A$  as shown in [Figure 8-1](#). The TMCS1126C2A with a 0.33V zero current reference voltage is intended for measuring unidirectional currents. When used with a 3.3V supply the TMCS1126C2A has a unidirectional linear current measurement range from  $-5 A$  to  $+57 A$  which can be extended from  $-5 A$  to  $+91.4 A$  when used with a 5V supply.

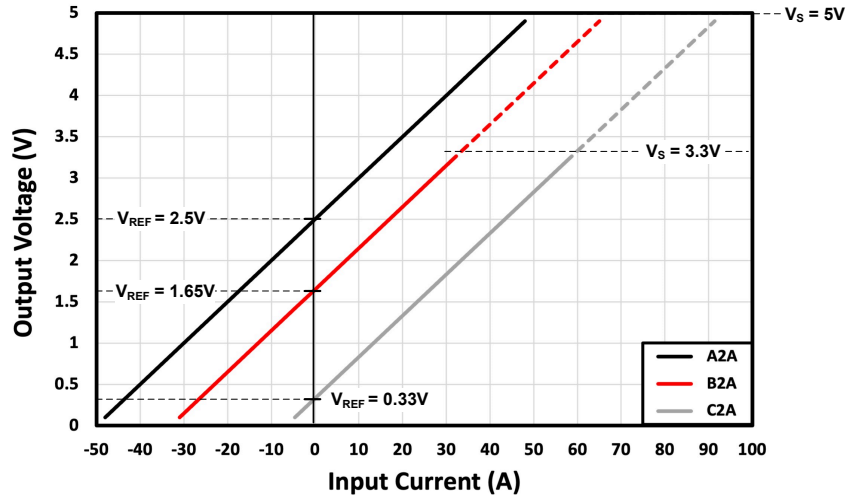


Figure 8-1. Output Voltage Relationship to Input Current for TMCS1126x2A

### 8.3.7 Overcurrent Detection

In addition to a fast precision analog signal response, the TMCS1126 also offers a fast digital overcurrent response. The Overcurrent Detection (OCD) circuit provides a comparator output that can be used to trigger a warning or system shutdown to prevent damage that may occur in the event of excessive current flow caused by shorts circuits, motor stalls, or other system conditions. This fast digital response can be configured on both bidirectional and unidirectional devices to trip either inside or outside the analog measurement range. When set up to trigger outside the analog measurement range, this fast digital overcurrent output  $\overline{OC}$  along with the precision analog output VOUT allows the user to optimize of control-loop dynamic range.

The desired overcurrent threshold  $I_{OC}$  is set by applying an external voltage  $V_{OC}$  to the VOC pin according to Equation 20.

$$V_{OC} = \frac{S \times I_{OC}}{2.5} \quad (20)$$

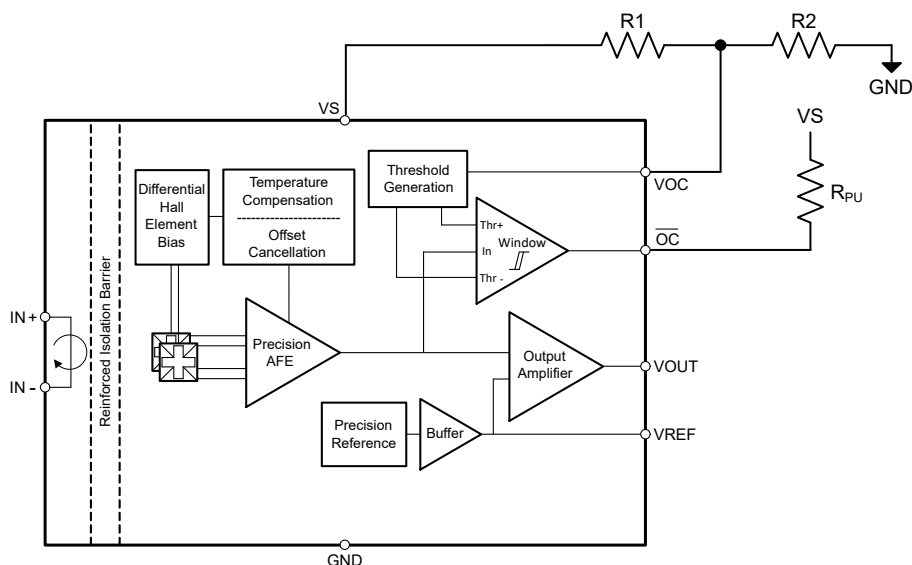
where

- S is the device sensitivity in mV/A.
- $I_{OC}$  is the desired overcurrent threshold.
- $V_{OC}$  is the voltage applied that sets the overcurrent threshold.

A digital-to-analog converter (DAC) can be used to set the desired overcurrent threshold  $I_{OC}$ , or a simple external resistor divider circuit can be used as shown in Figure 8-2. For example, to set the desired overcurrent threshold to  $I_{OC} = \pm 50$  A on the bidirectional TMCS1126A3A or TMCS1126B3A devices, or to  $I_{OC} = 50$  A on the unidirectional TMCS1126C3A device, resistors R1 and R2 should be sized to apply a voltage  $V_{OC} = 1.5$  V to the VOC pin according to Equation 20.

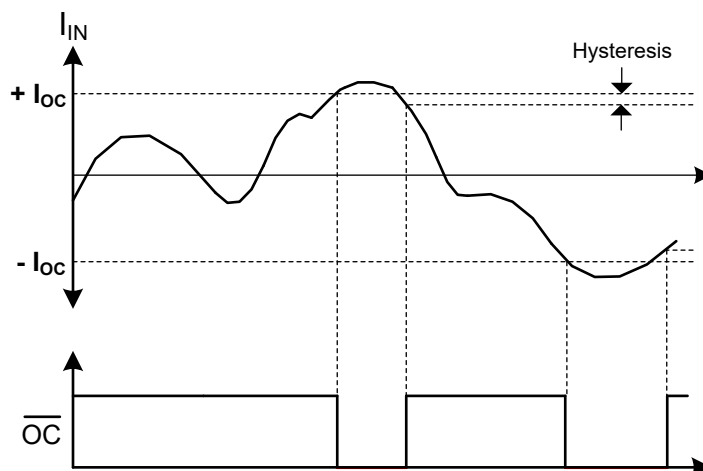
with

- TMCS1126A3A, TMCS1126B3A and TMCS1126C3A device sensitivity, **S = 75 mV/A**.
- Desired overcurrent threshold,  **$I_{OC} = 50$  A**.
- Applied overcurrent threshold voltage  **$V_{OC} = 1.5$  V**.



**Figure 8-2. User Configurable Overcurrent Threshold**

Figure 8-3 shows the overcurrent digital output  $\overline{OC}$  response as active-low. When the input current exceeds  $\pm I_{OC}$  on a bidirectional device, the fast  $\overline{OC}$  pin is pulled low. The input current must return to within  $\pm I_{OC}$  by more than a hysteresis current  $I_{Hys}$  before the  $\overline{OC}$  pin resets back to the normal high-state.



**Figure 8-3. Overcurrent Detection Diagram**

## 8.4 Device Functional Modes

### 8.4.1 Power-Down Behavior

As a result of the inherent galvanic isolation of the device, very little consideration must be paid to powering down the device, as long as the limits in the [Absolute Maximum Ratings](#) table are not exceeded on any pins. The isolated current input and the low-voltage signal chain can be decoupled in operational behavior, as either can be energized with the other shut down, as long as the isolation barrier capabilities are not exceeded. The low-voltage power supply can be powered down while the isolated input is still connected to an active high-voltage signal or system.

## 9 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 9.1 Application Information

The key feature sets of the TMCS1126 provide significant advantages in any application where an isolated current measurement is required.

- Galvanic isolation provides a high isolated working voltage and excellent immunity to input voltage transients.
- Hall based measurement simplifies system level solution without the need for a power supply on the high-voltage (HV) side.
- An input current path through the low impedance conductor minimizes power dissipation.
- Excellent accuracy and low temperature drift eliminate the need for multipoint calibrations without sacrificing system performance.
- A wide operating supply range enables a single device to function across a wide range of voltage levels.

These advantages increase system-level performance while minimizing complexity for any application where precision current measurements must be made on isolated currents. Specific examples and design requirements are detailed in the following section.

#### 9.1.1 Total Error Calculation Examples

Users can calculate the total error for any arbitrary device condition and current level. Consider error sources like input-referred offset current ( $I_{OS}$ ), Common Mode Rejection Ratio (CMRR), Power Supply Rejection Ratio (PSRR), sensitivity error, nonlinearity, as well as errors caused by any external magnetic fields ( $B_{EXT}$ ). Compare each of these error sources in percentage terms, as some are significant drivers of error and some have inconsequential impact to current measurement error. Offset (Equation 21), CMRR (Equation 22), PSRR (Equation 23), and external magnetic field error (Equation 24) are all referred to the input, and so are divided by the actual input current  $I_{IN}$  to calculate percentage errors. For sensitivity error and nonlinearity error calculations, the percentage limits explicitly specified in the *Electrical Characteristics* table can be used.

$$e_{I_{OS}} = \frac{I_{OS}}{I_{IN}} = \frac{V_{OE}}{S \times I_{IN}} \quad (21)$$

$$e_{CMRR} = \frac{CMRR \times V_{CM}}{I_{IN}} \quad (22)$$

$$e_{PSRR,A} = \frac{PSRR \times (V_S - 5V)}{I_{IN}}; e_{PSRR,B} = e_{PSRR,C} = \frac{PSRR \times (V_S - 3.3V)}{I_{IN}} \quad (23)$$

$$e_{B_{EXT}} = \frac{B_{EXT} \times CMFR}{I_{IN}} \quad (24)$$

where

- $V_{OE}$  is the output-referred offset voltage error.
- $V_{CM}$  is the input common-mode voltage.
- $e_{PSRR,A}$  is the power supply rejection error for TMCS1126Axx devices.
- $e_{PSRR,B}$  is the power supply rejection error for TMCS1126Bxx devices.
- $e_{PSRR,C}$  is the power supply rejection error for TMCS1126Cxx devices.
- $V_S$  is the supply voltage.
- CMFR is the common-mode magnetic field rejection.

When calculating error contributions across temperature, only offset error and sensitivity error contributions vary significantly. To determine the offset error across temperature, use [Equation 25](#) to calculate total input-referred offset error current,  $I_{OS}$ , at any ambient temperature,  $T_A$ .

$$e_{I_{OS}, \Delta T} = \frac{V_{OE, 25^\circ C} + (V_{OE, drift} \times \Delta T)}{S \times I_{IN}} \quad (25)$$

where

- $V_{OE, 25^\circ C}$  is the output-referred offset error at 25°C.
- $V_{OE, drift}$  is the output-referred offset drift with temperature in  $\mu V/^\circ C$ .
- $\Delta T$  is the change in temperature from 25°C.
- $S$  is the sensitivity of the device variant.

Sensitivity error at 25°C is specified as  $e_{S, 25^\circ C}$  in the [Electrical Characteristics](#) table along with sensitivity variation over temperature as sensitivity thermal drift  $S_{drift, therm}$  in ppm/°C. To determine the sensitivity error across temperature, use [Equation 26](#) to calculate sensitivity error at any ambient temperature,  $T_A$ , over the given application operating ambient temperature range between –40°C and 125°C.

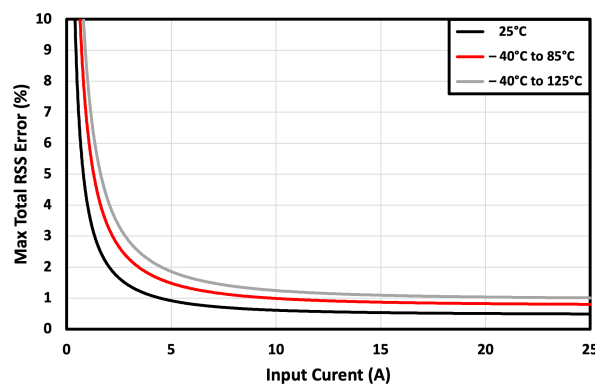
$$e_{S, \Delta T} = e_{S, 25^\circ C} + (S_{drift, therm} \times \Delta T) \quad (26)$$

To accurately calculate the total expected error of the device, the contributions from each of the individual components above must be understood in reference to operating conditions. To account for the individual error sources that are statistically uncorrelated, use a root sum square (RSS) error calculation to calculate total error. For the TMCS1126, only the input-referred offset current ( $I_{OS}$ ), CMRR, and PSRR are statistically correlated. These error terms are lumped in an RSS calculation to reflect this nature, as shown in [Equation 27](#) for room temperature and in [Equation 28](#) across a given temperature range. The same methodology can be applied for calculating typical total error by using the appropriate error term specification.

$$e_{RSS} = \sqrt{(|e_{I_{OS}}| + |e_{PSRR}| + |e_{CMRR}|)^2 + e_{B_{ext}}^2 + e_S^2 + e_{NL}^2} \quad (27)$$

$$e_{RSS, \Delta T} = \sqrt{(|e_{I_{OS}, \Delta T}| + |e_{PSRR}| + |e_{CMRR}|)^2 + e_{B_{ext}}^2 + e_{S, \Delta T}^2 + e_{NL}^2} \quad (28)$$

The total error calculation has a strong dependence on the actual input current, therefore always calculate total error across the dynamic range that is required. These curves asymptotically approach the sensitivity and nonlinearity error at high current levels, and approach infinity at low current levels due to offset error terms with input current in the denominator. Key figures of merit for any current-measurement system include the total error percentage at full-scale current, as well as the dynamic range of input current over which the error remains below some key level. [Figure 9-1](#) shows the RSS maximum total error as a function of input current for a TMCS1126A2A at room temperature and across the full temperature range with a 5.25V supply.



**Figure 9-1. RSS Error vs Input Current**

### 9.1.1.1 Room-Temperature Error Calculations

For room-temperature total error calculations, specifications across temperature and drift are ignored. As an example, consider a TMCS1126B2A with a supply voltage ( $V_S$ ) of 3.1 V and a worst-case common-mode excursion of 600 V to calculate operating-point-specific parameters. Consider a measurement error due to an external 400- $\mu$ T magnetic field generated by a 20A<sub>DC</sub> current flowing through an adjacent trace or conductor that is 10 mm away. The full-scale current range of the device in specified conditions is slightly greater than  $\pm 31$  A, as shown in the [Device Comparison](#) table. In this case, the calculating error at both 25 A and 12.5 A highlights error dependencies on the input-current level. [Table 9-1](#) shows the individual error components and RSS maximum total error calculations at room temperature under the conditions specified. Relative to other errors, the additional errors from CMRR, external ambient magnetic fields  $B_{EXT}$  and nonlinearity are negligible, and can typically be excluded from total error calculations.

**Table 9-1. Total Error Calculation: Room Temperature Example**

ERROR COMPONENT	SYMBOL	EQUATION	ERROR AT $I_{IN} = 25$ A	ERROR AT $I_{IN} = 12.5$ A
Input offset error	$e_{Ios}$	$e_{Ios} = \frac{I_{OS}}{I_{IN}} = \frac{V_{OE}}{S \times I_{IN}}$	0.10%	0.19%
PSRR error	$e_{PSRR}$	$e_{PSRR} = \frac{PSRR \times (V_S - 3.3)}{I_{IN}}$	0.04%	0.08%
CMRR error	$e_{CMRR}$	$e_{CMRR} = \frac{CMRR \times V_{CM}}{I_{IN}}$	0.01%	0.02%
External Field error	$e_{Bext}$	$e_{Bext} = \frac{B_{EXT} \times CMFR}{I_{IN}}$	0.02%	0.03%
Sensitivity error	$e_S$	Specified in <a href="#">Electrical Characteristics</a>	0.45%	0.45%
Nonlinearity error	$e_{NL}$	Specified in <a href="#">Electrical Characteristics</a>	0.10%	0.10%
RSS total error	$e_{RSS}$	$e_{RSS} = \sqrt{( e_{Ios}  +  e_{PSRR}  +  e_{CMRR} )^2 + e_{Bext}^2 + e_S^2 + e_{NL}^2}$	0.48%	0.55%

### 9.1.1.2 Full-Temperature Range Error Calculations

To calculate total error across any specific temperature range, use [Equation 27](#) and [Equation 28](#) for RSS maximum total errors, similar to the example for room temperatures. Conditions from the example in [Room-Temperature Error Calculations](#) have been replaced with their respective equations and error components for a  $-40^\circ\text{C}$  to  $85^\circ\text{C}$  temperature range below in [Table 9-2](#).

**Table 9-2. Total Error Calculation:  $-40^\circ\text{C}$  to  $85^\circ\text{C}$  Example**

ERROR COMPONENT	SYMBOL	EQUATION	ERROR AT $I_{IN} = 25$ A	ERROR AT $I_{IN} = 12.5$ A
Input offset error	$e_{Ios, \Delta T}$	$e_{Ios, \Delta T} = \frac{V_{OE, 25^\circ\text{C}} + (V_{OE, drift} \times \Delta T)}{S \times I_{IN}}$	0.19%	0.38%
PSRR error	$e_{PSRR}$	$e_{PSRR} = \frac{PSRR \times (V_S - 3.3)}{I_{IN}}$	0.04%	0.08%
CMRR error	$e_{CMRR}$	$e_{CMRR} = \frac{CMRR \times V_{CM}}{I_{IN}}$	0.01%	0.02%
External Field error	$e_{Bext}$	$e_{Bext} = \frac{B_{EXT} \times CMFR}{I_{IN}}$	0.02%	0.03%
Sensitivity error	$e_{S, \Delta T}$	$e_{S, \Delta T} = e_{S, 25^\circ\text{C}} + (S_{drift, therm} \times \Delta T)$	0.75%	0.75%
Nonlinearity error	$e_{NL}$	Specified in <a href="#">Electrical Characteristics</a>	0.10%	0.10%
RSS total error	$e_{RSS, \Delta T}$	$e_{RSS, \Delta T} = \sqrt{( e_{Ios, \Delta T}  +  e_{PSRR}  +  e_{CMRR} )^2 + e_{Bext}^2 + e_{S, \Delta T}^2 + e_{NL}^2}$	0.80%	0.90%

## 9.2 Typical Application

In many applications, power must be converted from AC sources for use in DC circuitry. Some type of controlled power factor correction (PFC) stage is usually needed to improve power transfer efficiency. Faster and faster power switches are being used in modern PFC stages to reduce overall size and to improve power transfer efficiency. Often, the PFC stage of AC to DC converters is connected directly to AC power grids. A primary challenge to sensing in PFC stages is that the current sensor is subjected to large voltage spikes coming from the high-voltage (HV) power grid along with large transients coming from high speed power switches during charge transfer. Inherent isolation in the TMCS1126 construction helps overcome these challenges by providing high levels of isolation between the HV current sensing nodes and low-voltage control circuitry, with high common-mode transient immunity (CMTI). Figure 9-2 shows the use of the TMCS1126 measuring phase currents in a common AC to DC converter stage.

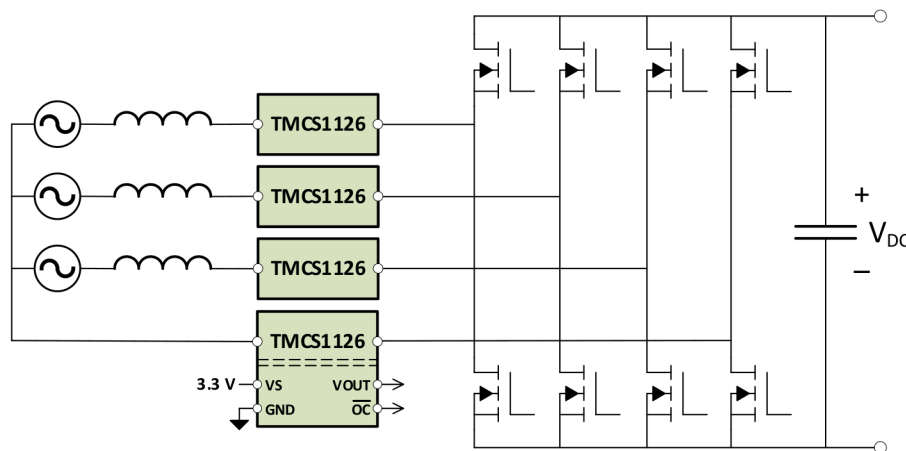


Figure 9-2. AC to DC Converter Current Sensing

### 9.2.1 Design Requirements

For a 3-phase current sensing application, make sure to provide linear sensing across the expected current range, and make sure that the device remains within working thermal constraints. A single TMCS1126 can be used to measure current in each phase if necessary. For this example, consider a nominal supply of 5 V but a minimum of 4.9 V to include for some supply variation. Maximum output swings are defined according to TMCS1126 specifications, and a full-scale current measurement of  $\pm 20$  A is required.

Table 9-3. Example Application Design Requirements

DESIGN PARAMETER	EXAMPLE VALUE
$V_{S,nom}$	5 V
$V_{S,min}$	4.9 V
$I_{IN,FS}$	$\pm 20$ A

### 9.2.2 Detailed Design Procedure

The primary design parameter for using the TMCS1126 is the optimum sensitivity variant based on the required measured current levels and the selected supply voltage. Positive and negative currents are measured in this in-line phase current application example, therefore select a bidirectional variant. The TMCS1126 has a precision internal reference voltage that determines the zero current output voltage,  $V_{OUT,0A}$ . The internal reference voltage on TMCS1126Axx variants, with zero current output voltage  $V_{OUT,0A} = 2.5$  V is intended for bidirectional current measurements when used with 5-V power supplies. The internal reference voltage on TMCS1126Bxx variants, with zero current output voltage  $V_{OUT,0A} = 1.65$  V is intended for bidirectional current measurements when used with 3.3-V power supplies. Further consideration of noise and integration with an ADC can be explored, but is beyond the scope of this application design example. The TMCS1126 output voltage  $V_{OUT}$  is proportional to the input current  $I_{IN}$  as defined by Equation 29 with output offset set by  $V_{OUT,0A}$ .



$$V_{OUT} = (I_{IN} \times S) + V_{OUT,0A} \quad (29)$$

Design of the sensing solution focuses on maximizing the sensitivity of the device while maintaining linear measurement over the expected current input range. The TMCS1126 has a slightly smaller linear output range to the supply than to ground, therefore the measurable current range is always constrained by the positive swing to supply,  $Swing_{VS}$ . To account for the operating margin, consider the minimum possible supply voltage  $V_{S,min}$ . With the previous parameters, the maximum linear output voltage  $V_{OUT,max}$  is defined by Equation 30.

$$V_{OUT,max} = V_{S,min} - Swing_{VS} \quad (30)$$

Design parameters for this example application are shown in Table 9-4 along with the calculated output range.

**Table 9-4. Example Application Design Parameters**

DESIGN PARAMETER	EXAMPLE VALUE
$Swing_{VS}$	0.1 V
$V_{OUT,max}$	4.8 V
$V_{OUT,0A}$	2.5 V
$V_{OUT,max} - V_{OUT,0A}$	2.3 V

These design parameters result in a maximum positive linear output voltage swing of  $\pm 2.3$  V about  $V_{OUT,0A} = 2.5$  V. To determine which sensitivity variant of the TMCS1126 most fully uses this linear range, use Equation 31 to calculate the maximum current range for a bidirectional current  $\pm I_{IN,max}$ .

$$I_{IN,max} = \frac{(V_{OUT,max} - V_{OUT,0A})}{S} \quad (31)$$

where

- $S$  is the sensitivity of the relevant AxA variant.

Table 9-5 shows the calculation for each gain variant of the TMCS1126 with the appropriate sensitivities.

**Table 9-5. Maximum Full-Scale Current Ranges With 2.3-V Positive Output Swing**

VARIANT	SENSITIVITY	$I_{IN,max}$
TMCS1126A1x	25 mV/A	$\pm 92$ A
TMCS1126A2x	50 mV/A	$\pm 46$ A
TMCS1126A3x	75 mV/A	$\pm 30.6$ A
TMCS1126A4x	100 mV/A	$\pm 23$ A
TMCS1126A5x	150 mV/A	$\pm 15.3$ A

In general, the highest sensitivity variant is selected to provide the lowest maximum input current range that is larger than the desired full-scale current range. For the design parameters in this example, either the higher precision TMCS1126A4A or the less accurate TMCS1126A4B (both with sensitivity of 0.1 V/A) is the proper selection because the maximum  $\pm 23$  A linear measurable range is larger than the desired  $\pm 20$  A full-scale current range.

### 9.3 Power Supply Recommendations

The TMCS1126 only requires a power supply ( $V_S$ ) on the low-voltage isolated side, which powers the analog circuitry independent of the isolated current input.  $V_S$  determines the full-scale output range of the analog output  $V_{OUT}$ , and can be supplied with any voltage between 3 V and 5.5 V. To filter noise in the power-supply path, place a low-ESR decoupling capacitor of 0.1  $\mu$ F between  $V_S$  and GND pins as close as possible to the supply and ground pins of the device. To compensate for noisy or high-impedance power supplies, add more decoupling capacitance.



The TMCS1126 power supply  $V_S$  can be sequenced independently of current flowing through the input. However, there is a typical 25ms delay between  $V_S$  reaching the recommended operating voltage and the analog output being valid. Within this delay  $V_{OUT}$  transfers from a high impedance state to the active drive state, during which time the output voltage could transition between GND and  $V_S$ . If this behavior must be avoided, a stable supply voltage to  $V_S$  should be provided for longer than 25 ms prior to applying input current.

## 9.4 Layout

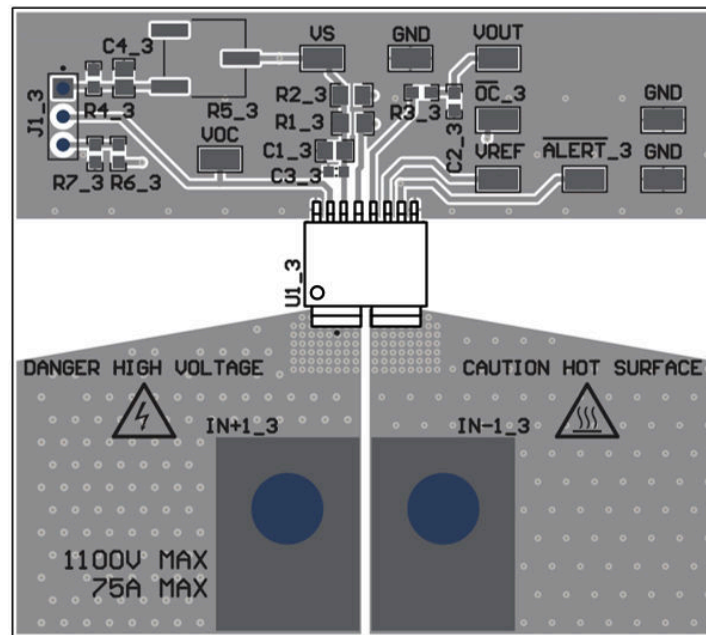
### 9.4.1 Layout Guidelines

The TMCS1126 is specified for a continuous current handling capability on the [TMCS1126xEVM](#) which uses 4-oz copper pour planes. This current capability is fundamentally limited by the maximum device junction temperature and the thermal environment, primarily the PCB layout and design. To maximize current-handling capability and thermal stability of the device, take care with PCB layout and construction to optimize the thermal capability. Efforts to improve the thermal performance beyond the design and construction of the [TMCS1126xEVM](#) can result in increased continuous-current capability due to higher heat transfer to the ambient environment. Keys to improving thermal performance of the PCB include:

- Use large copper planes for both input current path and isolated power planes and signals.
- Use heavier copper PCB construction.
- Place thermal via *farms* around the isolated current input.
- Provide airflow across the surface of the PCB.

### 9.4.2 Layout Example

An example layout, shown in [Figure 9-3](#), is from the [TMCS1126xEVM User's Guide](#). Device performance is targeted for thermal and magnetic characteristics of this layout, which provides optimal current flow from the terminal connectors to the device input pins while large copper planes enhance thermal performance.



**Figure 9-3. Recommended Board Layout**

## 10 Device and Documentation Support

### 10.1 Device Support

#### 10.1.1 Development Support

For development tool support see the following:

- [TMCS1126xEVM](#)

### 10.2 Documentation Support

#### 10.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, [TMCS1126xEVM User's Guide](#)
- Texas Instruments, [Isolation Glossary](#)

### 10.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](#). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 10.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 10.5 Trademarks

TI E2E™ is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

### 10.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 10.7 Glossary

[TI Glossary](#)

This glossary lists and explains terms, acronyms, and definitions.

## 11 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

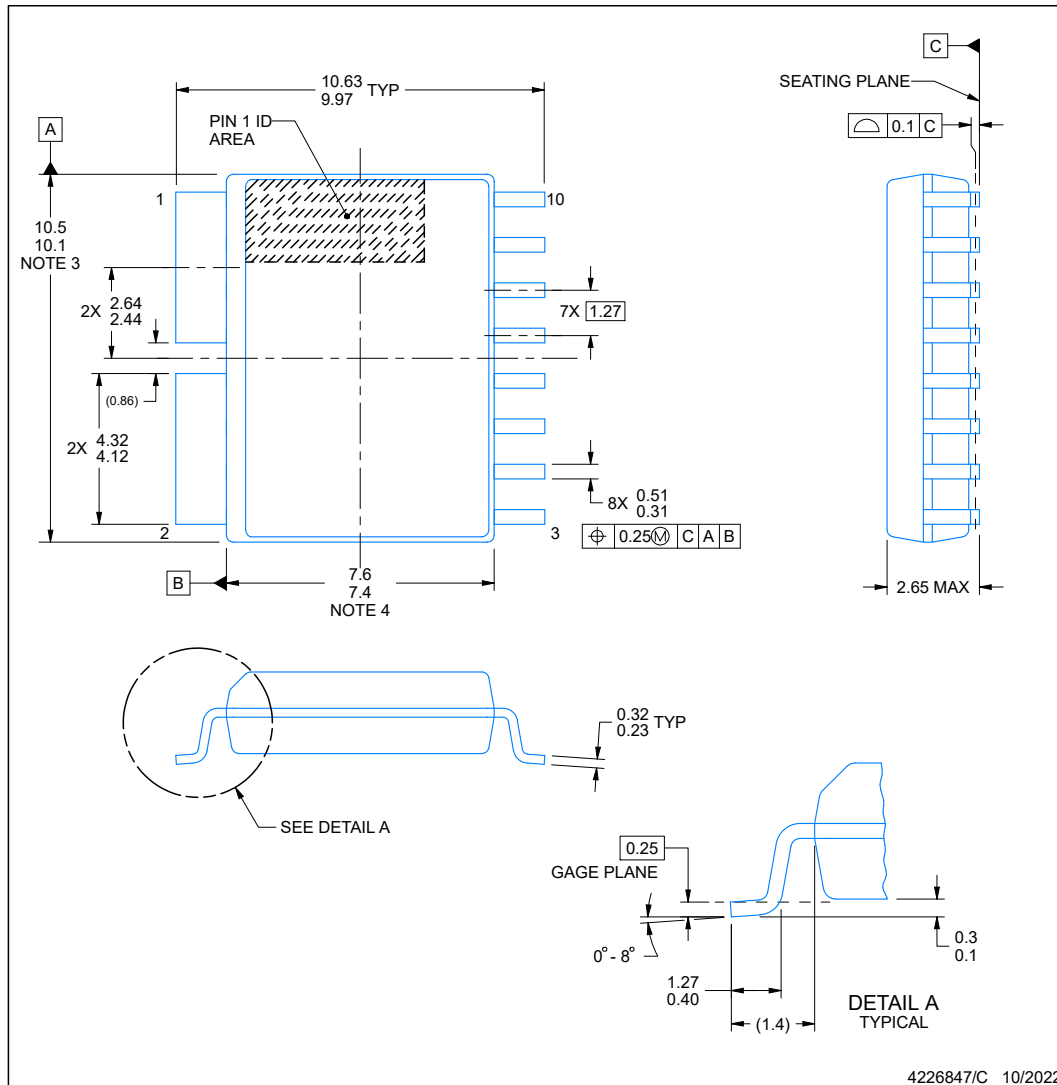
DATE	REVISION	NOTES
November 2023	*	Initial Release

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGE OUTLINE****DVG0010A****SOIC - 2.65 mm max height**

SMALL OUTLINE PACKAGE

**NOTES:**

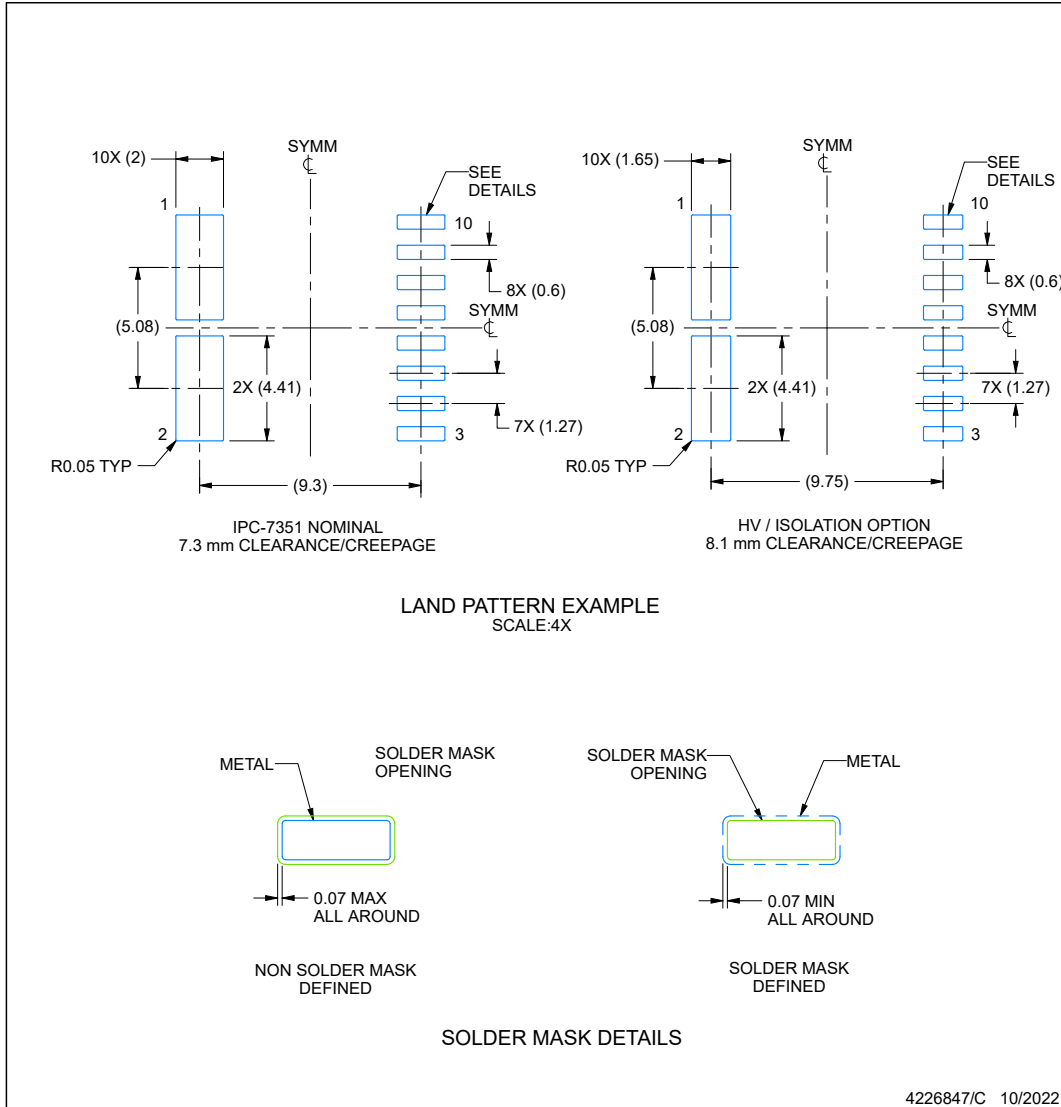
1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm, per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm, per side.
5. Reference JEDEC registration MS-013.

## EXAMPLE BOARD LAYOUT

**DVG0010A**

**SOIC - 2.65 mm max height**

SMALL OUTLINE PACKAGE



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

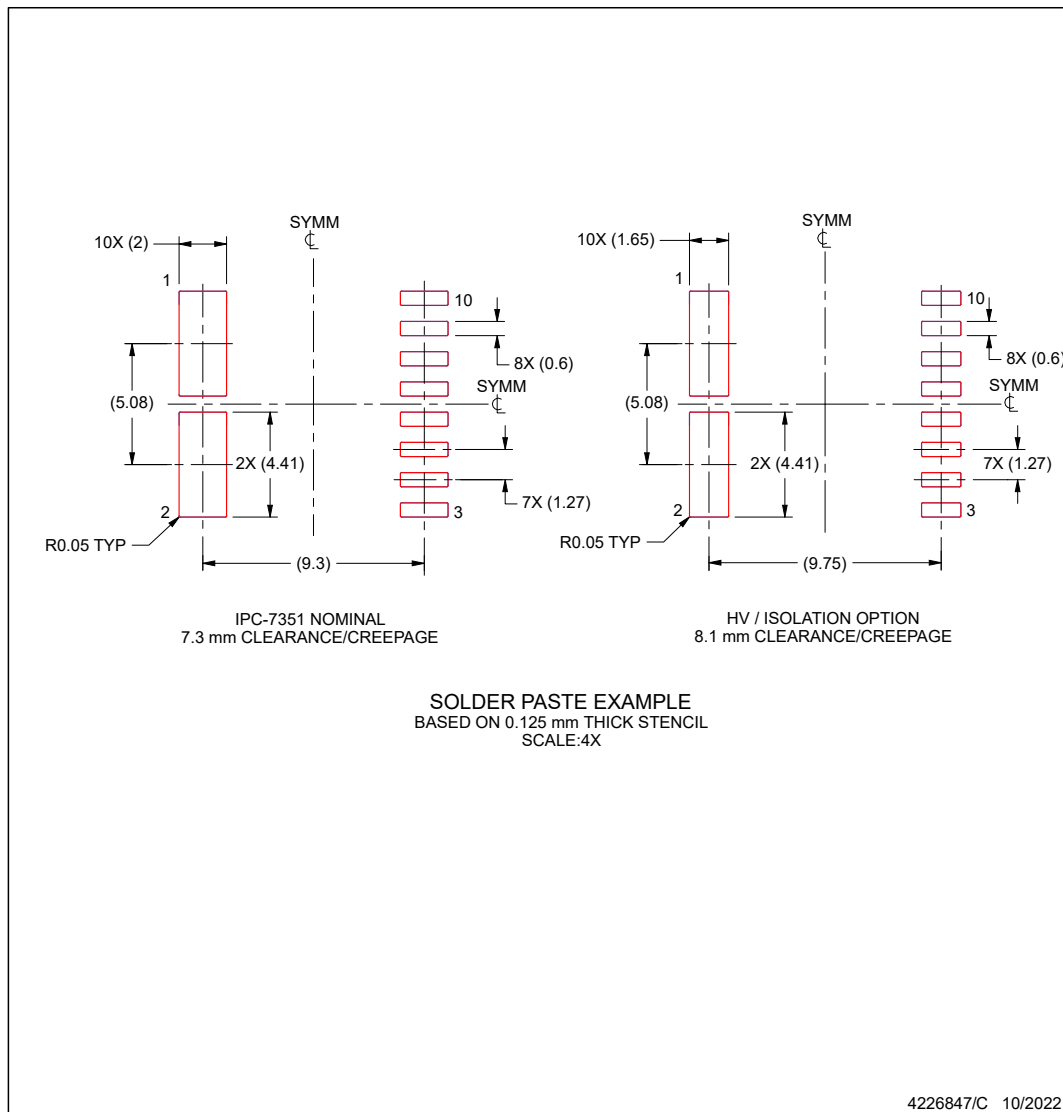
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

## EXAMPLE STENCIL DESIGN

**DVG0010A**

**SOIC - 2.65 mm max height**

SMALL OUTLINE PACKAGE



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

## 12.1 Package Option Addendum

### Packaging Information

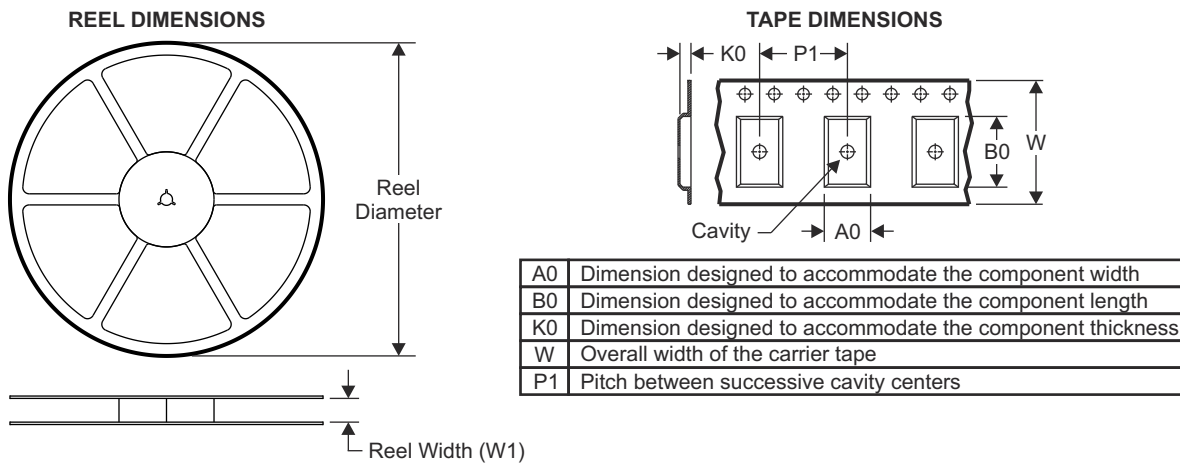
Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish <sup>(6)</sup>	MSL Peak Temp <sup>(3)</sup>	Op Temp (°C)	Device Marking <sup>(4) (5)</sup>
PMCS1126A1B QDVGR	ACTIVE	SOIC	DVG	10	2000	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	PMCS1126A1
PMCS1126A2B QDVGR	ACTIVE	SOIC	DVG	10	2000	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	PMCS1126A2
PMCS1126B1B QDVGR	ACTIVE	SOIC	DVG	10	2000	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	PMCS1126B1
PMCS1126B2B QDVGR	ACTIVE	SOIC	DVG	10	2000	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	PMCS1126B2

- (1) The marketing status values are defined as follows:  
**ACTIVE:** Product device recommended for new designs.  
**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.  
**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.  
**PRE\_PROD** Unannounced device, not in production, not available for mass market, nor on the web, samples not available.  
**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.  
**OBSOLETE:** TI has discontinued the production of the device.
- (2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check [www.ti.com/productcontent](http://www.ti.com/productcontent) for the latest availability information and additional product content details.  
**TBD:** The Pb-Free/Green conversion plan has not been defined.  
**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.  
**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.  
**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material).
- (3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

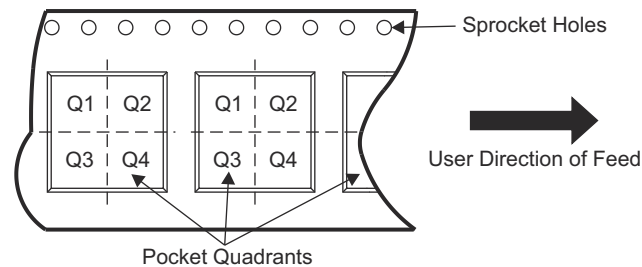
**Important Information and Disclaimer:** The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

## 12.2 Tape and Reel Information



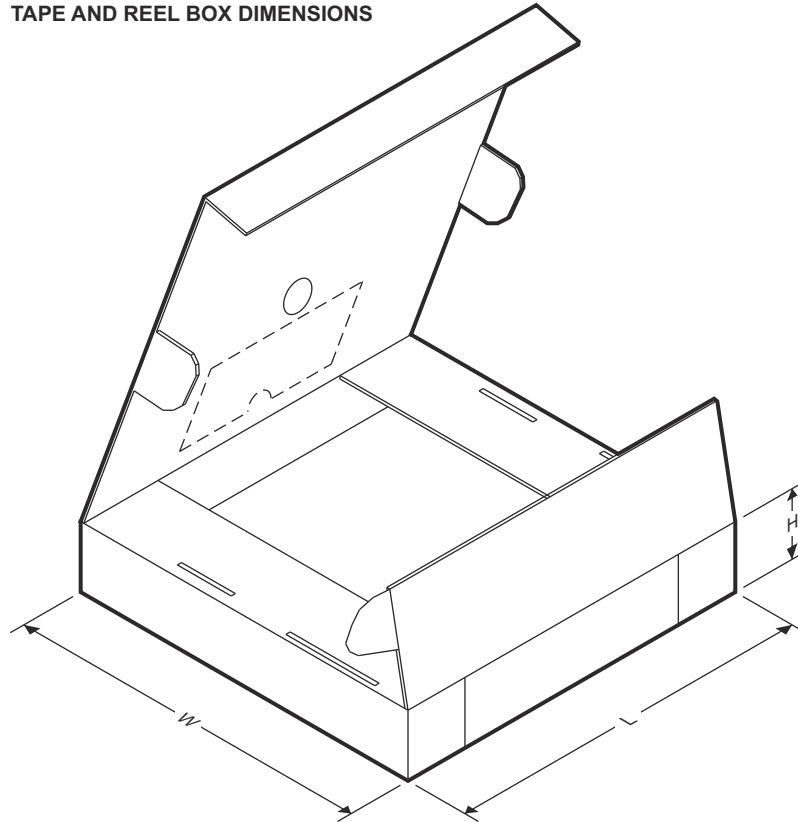
### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
PMCS1126A1BQDVGR	SOIC	DVG	10	2000	330	16.4	10.75	10.7	2.7	12	16	Q1
PMCS1126A2BQDVGR	SOIC	DVG	10	2000	330	16.4	10.75	10.7	2.7	12	16	Q1
PMCS1126B1BQDVGR	SOIC	DVG	10	2000	330	16.4	10.75	10.7	2.7	12	16	Q1
PMCS1126B2BQDVGR	SOIC	DVG	10	2000	330	16.4	10.75	10.7	2.7	12	16	Q1



# TAPE AND REEL BOX DIMENSIONS



Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
PMCS1126A1BQDVGR	SOIC	DVG	10	2000	350	350	43
PMCS1126A2BQDVGR	SOIC	DVG	10	2000	350	350	43
PMCS1126B1BQDVGR	SOIC	DVG	10	2000	350	350	43
PMCS1126B2BQDVGR	SOIC	DVG	10	2000	350	350	43

ADVANCE INFORMATION

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
PMCS1126A1BQDVGR	ACTIVE	SOIC	DVG	10	2000	TBD	Call TI	Call TI	-40 to 125		<a href="#">Samples</a>
PMCS1126A2BQDVGR	ACTIVE	SOIC	DVG	10	2000	TBD	Call TI	Call TI	-40 to 125		<a href="#">Samples</a>
PMCS1126B1BQDVGR	ACTIVE	SOIC	DVG	10	2000	TBD	Call TI	Call TI	-40 to 125		<a href="#">Samples</a>
PMCS1126B2BQDVGR	ACTIVE	SOIC	DVG	10	2000	TBD	Call TI	Call TI	-40 to 125		<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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