

TPS6281x 2.75V to 6V, Adjustable-Frequency Step-Down Converter

1 Features

- **Functional Safety-Capable**
 - Documentation available to aid functional safety system design
- Input voltage range: 2.75V to 6V
- Family of 1A, 2A, 3A, and 4A
- Quiescent current 15µA typical
- Output voltage from 0.6V to 5.5V
- Output voltage accuracy $\pm 1\%$ (PWM operation)
- Adjustable soft start
- Forced PWM or PWM and PFM operation
- Adjustable switching frequency of 1.8MHz to 4MHz
- Precise ENABLE input allows
 - User-defined undervoltage lockout
 - Exact sequencing
- 100% duty cycle mode
- Active output discharge
- Spread spectrum clocking - optional
- Power-good output with window comparator

2 Applications

- Factory automation and control
- Test and measurement
- Patient monitoring and diagnostics
- Wireless infrastructure
- Data center interconnect, optical modules

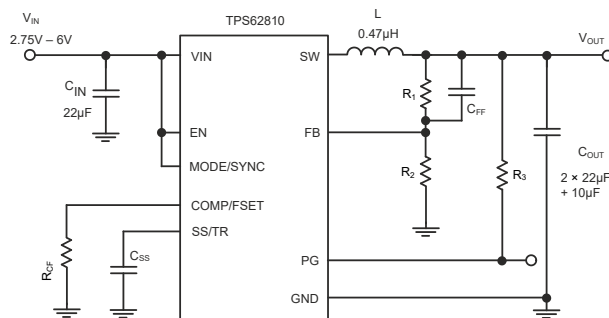
3 Description

The TPS6281x is family of pin-to-pin 1A, 2A, 3A, and 4A synchronous step-down DC/DC converters. All devices offer high efficiency and ease of use. The TPS6281x family is based on a peak current mode control topology. The TPS6281x is designed for industrial as well as telecommunication applications. Low resistive switches allow up to 4A continuous output current at high ambient temperature. The switching frequency is externally adjustable from 1.8MHz to 4MHz and can also be synchronized to an external clock in the same frequency range. In PWM/PFM mode, the TPS6281x automatically enter power save mode at light loads to maintain high efficiency across the whole load range. The TPS6281x provide 1% output voltage accuracy in PWM mode which helps design a power supply with high output voltage accuracy. The SS/TR pin allows setting the start-up time or forming tracking of the output voltage to an external source. This feature allows external sequencing of different supply rails and limiting the inrush current during start-up. The TPS6281x is available in a 3mm × 2mm VQFN package.

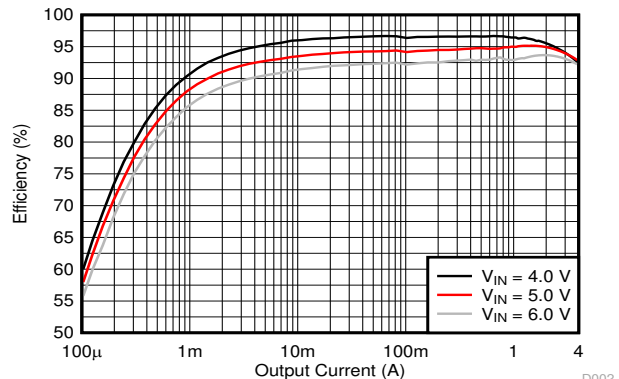
Device Information

PART NUMBER ⁽³⁾	PACKAGE ⁽¹⁾	PACKAGE SIZE ⁽²⁾
TPS62810	RWY (VQFN-HR, 9)	3mm × 2mm
TPS62811		
TPS62812		
TPS62813		

- (1) For more information, see [Section 12](#).
- (2) The package size (length × width) is a nominal value and includes pins, where applicable.
- (3) See the [Device Comparison Table](#).



Simplified Schematic



Efficiency vs Output Current; $V_{OUT} = 3.3V$; PWM/ PFM; $f_s = 2.25MHz$



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4 Device Comparison Table

DEVICE NUMBER	OUTPUT CURRENT	Vout DISCHARGE	FOLDBACK CURRENT LIMIT	SPREAD SPECTRUM CLOCKING (SSC)	OUTPUT VOLTAGE
TPS62811RWYR	1A	ON	OFF	OFF	Adjustable
TPS62812RWYR	2A	ON	OFF	OFF	Adjustable
TPS62813RWYR	3A	ON	OFF	OFF	Adjustable
TPS62810RWYR	4A	ON	OFF	OFF	Adjustable

5 Pin Configuration and Functions

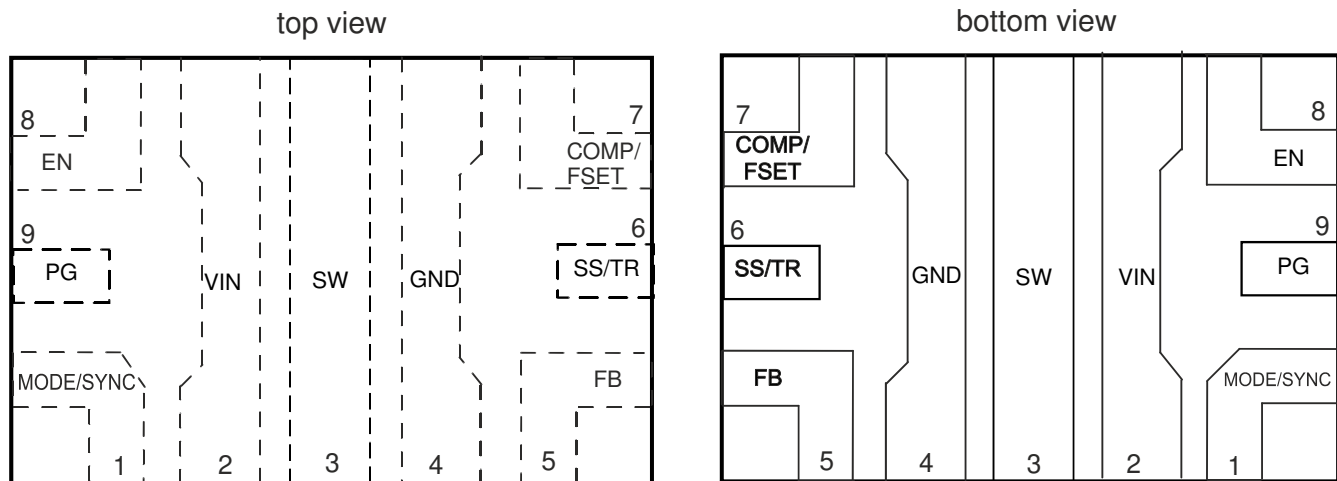


Figure 5-1. RWY Package 9 Pin (VQFN-HR)

Table 5-1. Pin Functions

PIN		TYPE ⁽¹⁾	DESCRIPTION
NAME	NO.		
EN	8	I	This pin is the enable pin of the device. Connect to logic low to disable the device. Pull high to enable the device. Do not leave this pin unconnected.
FB	5	I	Voltage feedback input, connect the resistive output voltage divider to this pin. For the fixed voltage versions, connect the FB pin directly to the output voltage.
GND	4		Ground pin
MODE/SYNC	1	I	The device runs in PFM/PWM mode when this pin is pulled low. If the pin is pulled high, the device runs in forced PWM mode. Do not leave this pin unconnected. The mode pin can also be used to synchronize the device to an external frequency. See the Specifications for the detailed specification of the digital signal applied to this pin for external synchronization.
COMP/FSET	7	I	Device compensation and frequency set input. A resistor from this pin to GND defines the compensation of the control loop as well as the switching frequency if not externally synchronized. If the pin is tied to GND or VIN, the switching frequency is set to 2.25MHz. Do not leave this pin unconnected.
PG	9	O	Open drain power good output. Low impedance when not "power good", high impedance when "power good". This pin can be left open or be tied to GND when not used.
SS/TR	6	I	Soft-Start / Tracking pin. A capacitor connected from this pin to GND defines the rise time for the internal reference voltage. The pin can also be used as an input for tracking and sequencing - see the Soft Start / Tracking (SS/TR) section.
SW	3	—	This pin is the switch pin of the converter and is connected to the internal Power MOSFETs.
VIN	2	—	Power supply input. Connect the input capacitor as close as possible between pin VIN and GND.

(1) I = input, O = output

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Pin voltage range ⁽¹⁾	VIN	−0.3	6.5	V
	SW	−0.3	VIN+0.3	V
	SW (transient for less than 10ns) ⁽²⁾	−3	10	V
	FB	−0.3	4	V
	PG, SS/TR, COMP/FSET	−0.3	VIN+0.3	V
Pin voltage range ⁽¹⁾	EN, MODE/SYNC	−0.3	6.5	V
Storage temperature, Tstg		−65	150	°C

(1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

(2) While switching

6.2 ESD Ratings

			VALUE	UNIT
V(ESD)	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 ⁽²⁾	±750	

(1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process

(2) JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

		MIN	NOM	MAX	UNIT
VIN	Supply voltage range	2.75		6	V
VOU	Output voltage range	0.6		5.5	V
L	Effective inductance for a switching frequency of 1.8 MHz to 3.5 MHz	0.32	0.47	0.9	μH
L	Effective inductance for a switching frequency of 3.5 MHz to 4 MHz	0.25	0.33	0.9	μH
COU	Effective output capacitance for 1A and 2A version ⁽¹⁾	15	22	470	μF
COU	Effective output capacitance for 3A and 4A version ⁽¹⁾	27	47	470	μF
CIN	Effective input capacitance ⁽¹⁾	5	10		μF
RCF	Resistor value from COMP/FSET to GND when not tied to GND or VIN	4.5		100	kΩ
TJ	Operating junction temperature	−40		+150	°C

(1) The values given for the capacitors in the table are effective capacitance, which includes the DC bias effect. Due to the DC bias effect of ceramic capacitors, the effective capacitance is lower than the nominal value when a voltage is applied. Please check the manufacturer's DC bias curves for the effective capacitance vs DC voltage applied. Further restrictions may apply. Please see the feature description for COMP/FSET about the output capacitance vs compensation setting and output voltage.

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS6281x	UNIT
		RWY	
		9 PINS	
RθJA	Junction-to-ambient thermal resistance	71.1	°C/W
RθJC(top)	Junction-to-case (top) thermal resistance	37.2	°C/W
RθJB	Junction-to-board thermal resistance	16.4	°C/W
ψJT	Junction-to-top characterization parameter	0.9	°C/W
ψJB	Junction-to-board characterization parameter	16.1	°C/W

6.4 Thermal Information (continued)

THERMAL METRIC ⁽¹⁾		TPS6281x	UNIT
		RWY	
		9 PINS	
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	n/a	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

6.5 Electrical Characteristics

over operating junction temperature ($T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.75\text{V}$ to 6V . Typical values at $V_{IN} = 5\text{V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
I _Q	Operating Quiescent Current	EN = high, I _{OUT} = 0mA, Device not switching, T _J = 125°C			21	μA
I _Q	Operating Quiescent Current	EN = high, I _{OUT} = 0mA, Device not switching		15	30	μA
I _{SD}	Shutdown Current	EN = 0V, at T _J = 125°C			18	μA
I _{SD}	Shutdown Current	EN = 0V, Nominal value at T _J = 25°C, Max value at T _J = 150°C		1.5	26	μA
V _{UVLO}	Undervoltage Lockout Threshold	Rising Input Voltage	2.5	2.6	2.75	V
		Falling Input Voltage	2.25	2.5	2.6	V
T _{SD}	Thermal Shutdown Temperature	Rising Junction Temperature		170		°C
	Thermal Shutdown Hysteresis			15		
CONTROL (EN, SS/TR, PG, MODE/SYNC)						
V _{IH}	High Level Input Voltage for MODE/SYNC Pin		1.1			V
V _{IL}	Low Level Input Voltage for MODE/SYNC Pin				0.3	V
f _{SYNC}	Frequency Range on MODE/ SYNC Pin for Synchronization	requires a resistor from COMP/FSET to GND, see application section	1.8		4	MHz
	Duty Cycle of Synchronization Signal at MODE/SYNC Pin		20%	50%	80%	
	Time to Lock to External Frequency			50		μs
V _{IH}	Input Threshold Voltage for EN pin; Rising Edge		1.06	1.1	1.15	V
V _{IL}	Input Threshold Voltage for EN pin; Falling Edge		0.96	1.0	1.05	V
I _{LKG}	Input Leakage Current for EN, MODE/SYNC	V _{IH} = V _{IN} or V _{IL} = GND			150	nA
	Resistance from COMP/FSET to GND for Logic Low	internal frequency setting with f = 2.25MHz	0		2.5	kΩ
	voltage on COMP/FSET for logic high	internal frequency setting with f = 2.25MHz		V _{IN}		V
V _{TH_PG}	UVP Power Good Threshold Voltage; dc Level	Rising (%V _{FB})	92%	95%	98%	
	UVP Power Good Threshold Voltage; dc Level	Falling (%V _{FB})	87%	90%	93%	
	OVP Power Good Threshold; dc Level	Rising (%V _{FB})	107%	110%	113%	
	OVP Power Good Threshold; dc Level	Falling (%V _{FB})	104%	107%	111%	
	Power Good De-glitch Time	for a high level to low level transition on power good		40		μs
V _{OL_PG}	Power Good Output Low Voltage	I _{PG} = 2mA		0.07	0.3	V

6.5 Electrical Characteristics (continued)

over operating junction temperature ($T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.75\text{V}$ to 6V . Typical values at $V_{IN} = 5\text{V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

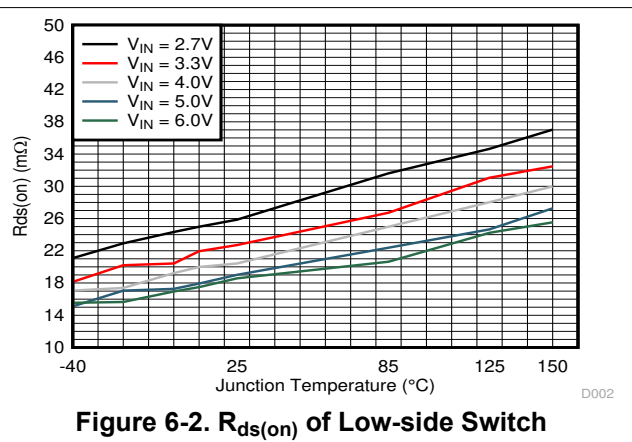
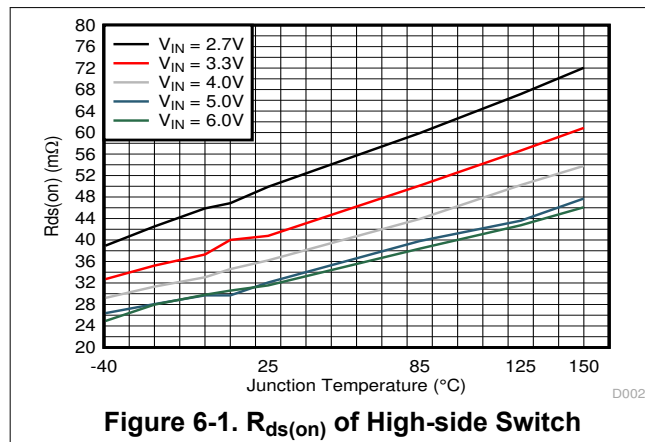
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
I_{LKG_PG}	Input Leakage Current (PG)	$V_{PG} = 5\text{V}$			100	nA
$I_{SS/TR}$	SS/TR Pin Source Current		2.1	2.5	2.8	μA
	Tracking Gain	$V_{FB} / V_{SS/TR}$ for nominal $V_{FB} = 0.6\text{V}$		1		
	Tracking Offset	feedback voltage with $V_{SS/TR} = 0\text{V}$ for nominal $V_{FB} = 0.6\text{V}$		17		mV
POWER SWITCH						
$R_{DS(ON)}$	High-Side MOSFET ON-Resistance	$V_{IN} \geq 5\text{V}$		37	60	$\text{m}\Omega$
$R_{DS(ON)}$	Low-Side MOSFET ON-Resistance	$V_{IN} \geq 5\text{V}$		15	35	$\text{m}\Omega$
	High-Side MOSFET leakage current	$V_{IN} = 6\text{V}; V(\text{SW}) = 0\text{V}$			30	μA
	Low-Side MOSFET leakage current	$V(\text{SW}) = 6\text{V}$			55	μA
	SW leakage	$V(\text{SW}) = 0.6\text{V}$; current into SW pin	-0.025		30	μA
I_{LIMH}	High-Side MOSFET Current Limit	DC value, for TPS62810; $V_{IN} = 3\text{V}$ to 6V	4.8	5.6	6.55	A
I_{LIMH}	High-Side MOSFET Current Limit	DC value, for TPS62813; $V_{IN} = 3\text{V}$ to 6V	3.9	4.5	5.25	A
I_{LIMH}	High-Side MOSFET Current Limit	DC value, for TPS62812; $V_{IN} = 3\text{V}$ to 6V	2.8	3.4	4.2	A
I_{LIMH}	High-Side MOSFET Current Limit	DC value, for TPS62811; $V_{IN} = 3\text{V}$ to 6V	2.0	2.6	3.25	A
I_{LIMNEG}	Negative Valley Current Limit	DC value		-1.8		A
f_S	PWM Switching Frequency Range		1.8	2.25	4	MHz
f_S	PWM Switching Frequency	with COMP/FSET tied to V_{IN} or GND	2.025	2.25	2.475	MHz
	PWM Switching Frequency Tolerance	using a resistor from COMP/FSET to GND, $f_S = 1.8\text{MHz}$ to 4MHz	-19%		18%	
$t_{on,min}$	Minimum on-time of HS FET	$T_J = -40^{\circ}\text{C}$ to 125°C , $V_{IN} = 3.3\text{V}$		50	75	ns
$t_{on,min}$	Minimum on-time of LS FET	$V_{IN} = 3.3\text{V}$		30		ns
OUTPUT						
V_{FB}	Feedback Voltage	adjustable output voltage versions		0.6		V
I_{LKG_FB}	FB Input Leakage Current for Adjustable Voltage Versions	$V_{FB} = 0.6\text{V}$		1	70	nA
I_{LKG_FB}	FB Input Current for Fixed Voltage Versions	V_{FB} voltage at target output voltage		1		μA
V_{FB}	Feedback Voltage Accuracy for Adjustable Voltage Versions	$V_{IN} \geq V_{OUT} + 1\text{V}$	PWM mode	-1%	1%	
V_{FB}	Feedback Voltage Accuracy for Fixed Voltage Versions	$V_{IN} \geq V_{OUT} + 1\text{V}$	PWM mode, $T_J = -40^{\circ}\text{C}$ to 125°C	-1%	1%	
V_{FB}	Feedback Voltage Accuracy for Fixed Voltage Versions	$V_{IN} \geq V_{OUT} + 1\text{V}$	PWM mode	-1%	1.3%	
V_{FB}	Feedback Voltage Accuracy	$V_{IN} \geq V_{OUT} + 1\text{V}$; $V_{OUT} \geq 1.5\text{V}$	PFM mode; $C_{o,eff} \geq 22\mu\text{F}$, $L = 0.47\mu\text{H}$	-1%	2%	
V_{FB}	Feedback Voltage Accuracy	$1\text{V} \leq V_{OUT} < 1.5\text{V}$	PFM mode; $C_{o,eff} \geq 47\mu\text{F}$, $L = 0.47\mu\text{H}$	-1%	2.5%	
V_{FB}	Feedback Voltage Accuracy with Voltage Tracking	$V_{IN} \geq V_{OUT} + 1\text{V}$; $V_{SS/TR} = 0.3\text{V}$	PWM mode	-1%	7%	
	Load Regulation	PWM mode operation		0.05		%/A
	Line Regulation	PWM mode operation, $I_{OUT} = 1\text{A}$, $V_{IN} \geq V_{OUT} + 1\text{V}$		0.02		%/V
	Output Discharge Resistance				50	Ω

6.5 Electrical Characteristics (continued)

over operating junction temperature ($T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.75\text{V}$ to 6V . Typical values at $V_{IN} = 5\text{V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{delay}	Start-up Delay Time	$I_{\text{OUT}} = 0\text{mA}$, Time from EN=high to start switching; V_{IN} applied already	135	250	470	μs
t_{ramp}	Ramp time; SS/TR Pin Open	$I_{\text{OUT}} = 0\text{mA}$, Time from first switching pulse until 95% of nominal output voltage; device not in current limit	100	150	200	μs

6.6 Typical Characteristics



7 Parameter Measurement Information

7.1 Schematic

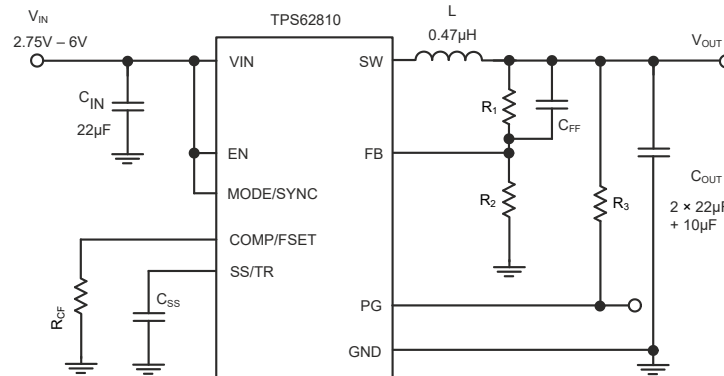


Figure 7-1. Measurement Setup for TPS62810 and TPS62813

Table 7-1. List of Components

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS62810 or TPS62813	Texas Instruments
L	0.47µH inductor; XEL4030-471MEB	Coilcraft
C _{IN}	22µF / 10V; GCM31CR71A226KE02L	Murata
C _{OUT}	2 × 22µF / 10V; GCM31CR71A226KE02L + 1 × 10µF / 6.3V; GCM188D70J106ME36	Murata
C _{SS}	4.7nF (equal to 1ms start-up ramp)	Any
R _{CF}	8.06kΩ	Any
C _{FF}	10pF	Any
R ₁	Depending on V _{OUT}	Any
R ₂	Depending on V _{OUT}	Any
R ₃	100kΩ	Any

(1) See the [Third-party Products Disclaimer](#).

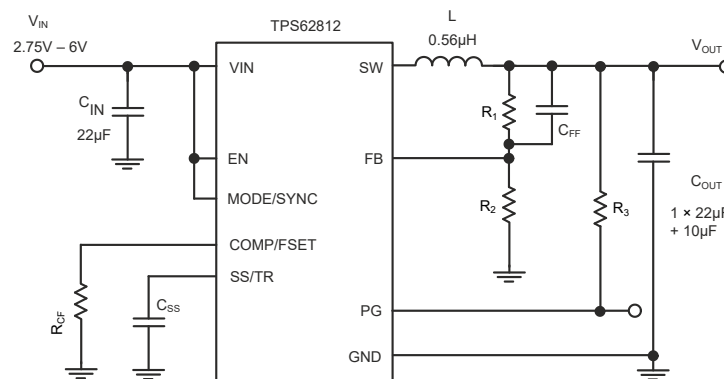


Figure 7-2. Measurement Setup for TPS62812 and and TPS62811

Table 7-2. List of Components

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS62812 or TPS62811	Texas Instruments
L	0.56μH inductor; XEL4020-561MEB	Coilcraft
C _{IN}	22μF / 10V; GCM31CR71A226KE02L	Murata
C _{OUT}	1 × 22μF / 10V; GCM31CR71A226KE02L + 1 × 10μF / 6.3V; GCM188D70J106ME36	Murata
C _{SS}	4.7nF (equal to 1ms start-up ramp)	Any
R _{CF}	8.06kΩ	Any
C _{FF}	10pF	Any
R ₁	Depending on VOUT	Any
R ₂	Depending on VOUT	Any
R ₃	100kΩ	Any

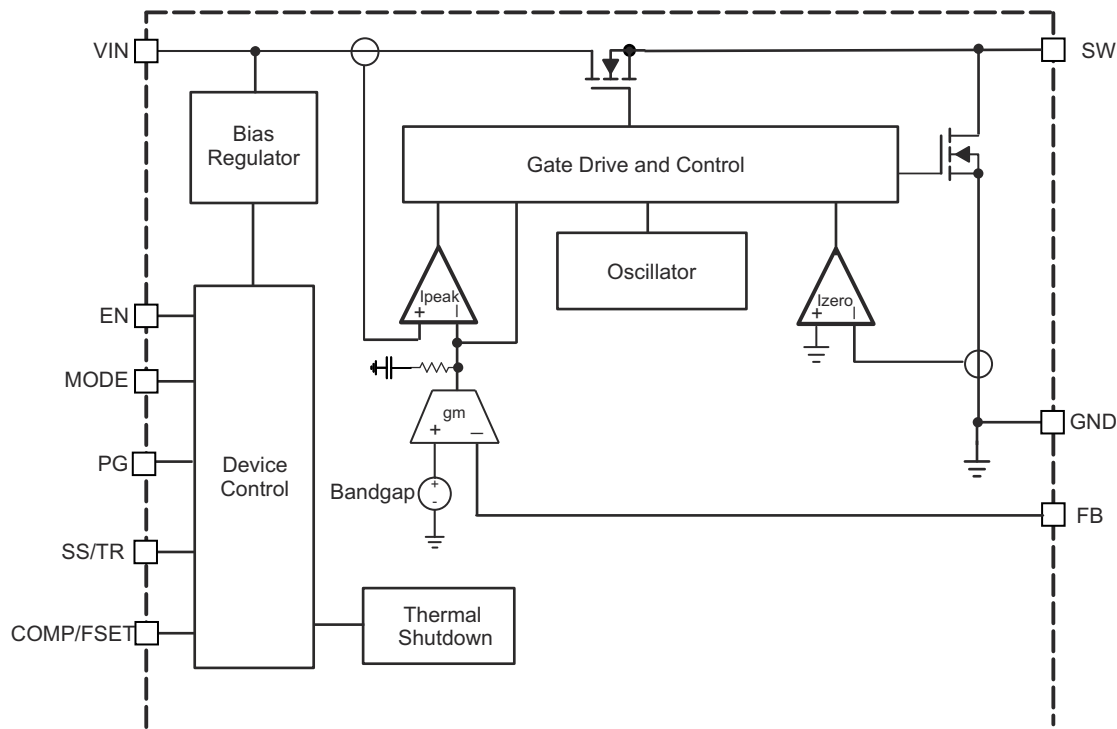
8 Detailed Description

8.1 Overview

The TPS6281x synchronous switch mode DC/DC converters are based on a peak current mode control topology. The control loop is internally compensated. To optimize the bandwidth of the control loop to the wide range of output capacitance that can be used with TPS6281x, one of three internal compensation settings can be selected. See [COMP/FSET](#). The compensation setting is selected either by a resistor from COMP/FSET to GND, or by the logic state of this pin. The regulation network achieves fast and stable operation with small external components and low ESR ceramic output capacitors. The device can be operated without a feedforward capacitor on the output voltage divider, however, using a typically 10pF feedforward capacitor improves transient response.

The devices support forced fixed frequency PWM operation with the MODE pin tied to a logic high level. The frequency is defined as either 2.25MHz internally fixed when COMP/FSET is tied to GND or VIN, or in a range of 1.8MHz to 4MHz defined by a resistor from COMP/FSET to GND. Alternatively, the devices can be synchronized to an external clock signal in a range from 1.8MHz to 4MHz, applied to the MODE pin with no need for additional passive components. External synchronization is only possible if a resistor from COMP/FSET to GND is used. If COMP/FSET is directly tied to GND or VIN, the TPS6281x cannot be synchronized externally. An internal PLL allows to change from internal clock to external clock during operation. The synchronization to the external clock is done on a falling edge of the clock applied at MODE to the rising edge on the SW pin. This allows a roughly 180° phase shift when the SW pin is used to generate the synchronization signal for a second converter. When the MODE pin is set to a logic low level, the device operates in power save mode (PFM) at low output current and automatically transfers to fixed frequency PWM mode at higher output current. In PFM mode, the switching frequency decreases linearly based on the load to sustain high efficiency down to very low output current.

8.2 Functional Block Diagram



8.3 Feature Description

8.3.1 Precise Enable

The voltage applied at the Enable pin of the TPS6281x is compared to a fixed threshold of 1.1V for a rising voltage. This allows to drive the pin by a slowly changing voltage and enables the use of an external RC network to achieve a power-up delay.

The Precise Enable input provides a user-programmable undervoltage lockout by adding a resistor divider to the input of the Enable pin.

The enable input threshold for a falling edge is typically 100mV lower than the rising edge threshold. The TPS6281x starts operation when the rising threshold is exceeded. For proper operation, the EN pin must be terminated and must not be left floating. Pulling the EN pin low forces the device into shutdown, with a shutdown current of typically 1µA. In this mode, the internal high-side and low-side MOSFETs are turned off and the entire internal control circuitry is switched off.

8.3.2 COMP/FSET

This pin allows to set two different parameters independently:

- Internal compensation settings for the control loop
- The switching frequency in PWM mode from 1.8MHz to 4MHz

A resistor from COMP/FSET to GND changes the compensation as well as the switching frequency. The change in compensation allows you to adapt the device to different values of output capacitance. The resistor must be placed close to the pin to keep the parasitic capacitance on the pin to a minimum. The compensation setting is sampled at start-up of the converter, so a change in the resistor during operation only has an effect on the switching frequency but not on the compensation.

To save external components, the pin can also be directly tied to VIN or GND to set a pre-defined switching frequency / compensation. Do not leave the pin floating.

The switching frequency has to be selected based on the input voltage and the output voltage to meet the specifications for the minimum on-time and minimum off-time.

For example: $V_{IN} = 5V$, $V_{OUT} = 1V$ --> duty cycle (DC) = $1V / 5V = 0.2$

- with $t_{on} = DC \times T$ --> $t_{on,min} = 1 / f_{s,max} \times DC$
- --> $f_{s,max} = 1 / t_{on,min} \times DC = 1 / 0.075\mu s \times 0.2 = 2.67MHz$

The compensation range has to be chosen based on the minimum capacitance used. The capacitance can be increased from the minimum value as given in [Table 8-1](#) and [Table 8-2](#), up to the maximum of 470µF in all of the three compensation ranges. If the capacitance of an output changes during operation, for example, when load switches are used to connect or disconnect parts of the circuitry, the compensation has to be chosen for the minimum capacitance on the output. With large output capacitance, the compensation must be done based on that large capacitance to get the best load transient response. Compensating for large output capacitance but placing less capacitance on the output can lead to instability.

The switching frequency for the different compensation setting is determined by the following equations.

For compensation (comp) setting 1:

$$R_{CF}(k\Omega) = \frac{18MHz \cdot k\Omega}{f_s(MHz)} \quad (1)$$

For compensation (comp) setting 2:

$$R_{CF}(k\Omega) = \frac{60MHz \cdot k\Omega}{f_s(MHz)} \quad (2)$$

For compensation (comp) setting 3:

$$R_{CF}(k\Omega) = \frac{180MHz \cdot k\Omega}{f_s(MHz)} \quad (3)$$

Table 8-1. Switching Frequency and Compensation for TPS62810 (4A) and TPS62813 (3A)

COMPENSATION	R _{CF}	SWITCHING FREQUENCY	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} < 1V	MINIMUM OUTPUT CAPACITANCE FOR 1V ≤ V _{OUT} < 3.3V	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} ≥ 3.3V
for smallest output capacitance (comp setting 1)	10kΩ ... 4.5kΩ	1.8MHz (10kΩ) ... 4MHz (4.5kΩ) according to Equation 1	53μF	32μF	27μF
for medium output capacitance (comp setting 2)	33kΩ ... 15kΩ	1.8MHz (33kΩ) ... 4MHz (15kΩ) according to Equation 2	100μF	60μF	50μF
for large output capacitance (comp setting 3)	100kΩ ... 45kΩ	1.8MHz (100kΩ) ... 4MHz (45kΩ) according to Equation 3	200μF	120μF	100μF
for smallest output capacitance (comp setting 1)	tied to GND	internally fixed 2.25MHz	53μF	32μF	27μF
for large output capacitance (comp setting 3)	tied to V _{IN}	internally fixed 2.25MHz	200μF	120μF	100μF

Table 8-2. Switching Frequency and Compensation for TPS62812 (2A) (1A)

COMPENSATION	R _{CF}	SWITCHING FREQUENCY	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} < 1V	MINIMUM OUTPUT CAPACITANCE FOR 1V ≤ V _{OUT} < 3.3V	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} ≥ 3.3V
for smallest output capacitance (comp setting 1)	10kΩ ... 4.5kΩ	1.8MHz (10kΩ) ... 4MHz (4.5kΩ) according to Equation 1	30μF	18μF	15μF
for medium output capacitance (comp setting 2)	33kΩ ... 15kΩ	1.8MHz (33kΩ) ... 4MHz (15kΩ) according to Equation 2	60μF	36μF	30μF
for large output capacitance (comp setting 3)	100kΩ ... 45kΩ	1.8MHz (100kΩ) ... 4MHz (45kΩ) according to Equation 3	130μF	80μF	68μF
for smallest output capacitance (comp setting 1)	tied to GND	internally fixed 2.25MHz	30μF	18μF	15μF
for large output capacitance (comp setting 3)	tied to V _{IN}	internally fixed 2.25MHz	130μF	80μF	68μF

See also [Output Capacitor](#) for further details on the output capacitance required depending on the output voltage.

A too high resistor value for R_{CF} is decoded as "tied to V_{IN}", a value below the lowest range is decoded as "tied to GND". The minimum output capacitance in [Table 8-1](#) and [Table 8-2](#) is for capacitors close to the output of the device. If the capacitance is distributed, a lower compensation setting can be required. All values are effective capacitance, including all tolerances, aging, DC bias effect, and so forth.

8.3.3 MODE / SYNC

When MODE/SYNC is set low, the device operates in PWM or PFM mode, depending on the output current. The MODE/SYNC pin allows to force PWM mode when set high. The pin also allows the user to apply an external clock in a frequency range from 1.8MHz to 4MHz for external synchronization. Similar to COMP/FSET, the specifications for the minimum on-time and minimum off-time must be taken into account when setting the external frequency. For use with external synchronization on the MODE/SYNC pin, the internal switching frequency must be set by R_{CF} to a similar value than the externally applied clock. This action makes sure of a fast settling to the external clock and, if the external clock fails, the switching frequency stays in the same range

and the compensation settings are still valid. When there is no resistor from COMP/FSET to GND but the pin is pulled high or low, external synchronization is not possible.

8.3.4 Spread Spectrum Clocking (SSC)

For device versions with SSC enabled, the switching frequency is randomly changed in PWM mode when the internal clock is used. The frequency variation is typically between the nominal switching frequency and up to 288kHz above the nominal switching frequency. When the device is externally synchronized by applying a clock signal to the MODE/SYNC pin, the TPS6281x follows the external clock and the internal spread spectrum block is turned off. SSC is also disabled during soft start.

8.3.5 Undervoltage Lockout (UVLO)

If the input voltage drops, the undervoltage lockout prevents mis-operation of the device by switching off both the power FETs. The device is fully operational for voltages above the rising UVLO threshold and turns off if the input voltage trips below the threshold for a falling supply voltage.

8.3.6 Power Good Output (PG)

Power good is an open-drain output driven by a window comparator. PG is held low when the device is disabled, in undervoltage lockout, and in thermal shutdown. When the output voltage is in regulation hence, within the window defined in the electrical characteristics, the output is high impedance.

Table 8-3. PG Status

EN	DEVICE STATUS	PG STATE
X	$V_{IN} < 2V$	undefined
low	$V_{IN} \geq 2V$	low
high	$2V \leq V_{IN} \leq UVLO$ OR in thermal shutdown OR V_{OUT} not in regulation	low
high	V_{OUT} in regulation	high impedance

8.3.7 Thermal Shutdown

The junction temperature (T_J) of the device is monitored by an internal temperature sensor. If T_J exceeds 170°C (typ), the device goes into thermal shutdown. Both the high-side and low-side power FETs are turned off and PG goes low. When T_J decreases by the hysteresis amount of typically 15°C, the converter resumes normal operation, beginning with soft start. During a PFM pause, the thermal shutdown is not active. After a PFM pause, the device needs up to 9μs to detect a too high junction temperature. If the PFM burst is shorter than this delay, the device does not detect a too high junction temperature.

8.4 Device Functional Modes

8.4.1 Pulse Width Modulation (PWM) Operation

TPS6281x has two operating modes: Forced PWM mode (discussed in this section) and PWM/PFM (discussed in [Power Save Mode Operation \(PWM/PFM\)](#)).

With the MODE/SYNC pin set to high, the TPS6281x operates with pulse width modulation in continuous conduction mode (CCM). The switching frequency is either defined by a resistor from the COMP pin to GND or by an external clock signal applied to the MODE/SYNC pin. With an external clock is applied to MODE/SYNC, the TPS6281x follows the frequency applied to the pin. To maintain regulation, the frequency must be in a range the TPS6281x can operate at, taking the minimum on-time into account.

8.4.2 Power Save Mode Operation (PWM/PFM)

When the MODE/SYNC pin is low, power save mode is allowed. The device operates in PWM mode as long as the peak inductor current is above the PFM threshold of about 1.2A. When the peak inductor current drops below the PFM threshold, the device starts to skip switching pulses. In power save mode, the switching frequency decreases with the load current maintaining high efficiency.

8.4.3 100% Duty-Cycle Operation

The duty cycle of a buck converter operated in PWM mode is given as $D = V_{OUT} / V_{IN}$. The duty cycle increases as the input voltage comes close to the output voltage and the off-time gets smaller. When the minimum off-time of typically 30ns is reached, the TPS6281x skips switching cycles while approaching 100% mode. In 100% mode, the device keeps the high-side switch on continuously. The high-side switch stays turned on as long as the output voltage is below the target. In 100% mode, the low-side switch is turned off. The maximum dropout voltage in 100% mode is the product of the on-resistance of the high-side switch plus the series resistance of the inductor and the load current.

8.4.4 Current Limit and Short-Circuit Protection

The TPS6281x is protected against overload and short circuit events. If the inductor current exceeds the current limit I_{LIMH} , the high-side switch is turned off and the low-side switch is turned on to ramp down the inductor current. The high-side switch turns on again only if the current in the low-side switch has decreased below the low-side current limit. Due to internal propagation delay, the actual current can exceed the static current limit. The dynamic current limit is given as:

$$I_{peak(typ)} = I_{LIMH} + \frac{V_L}{L} \cdot t_{PD} \quad (4)$$

where

- I_{LIMH} is the static current limit as specified in the electrical characteristics
- L is the effective inductance at the peak current
- V_L is the voltage across the inductor ($V_{IN} - V_{OUT}$)
- t_{PD} is the internal propagation delay of typically 50ns

The current limit can exceed static values, especially if the input voltage is high and very small inductances are used. The dynamic high-side switch peak current can be calculated as follows:

$$I_{peak(typ)} = I_{LIMH} + \frac{V_{IN} - V_{OUT}}{L} \cdot 50ns \quad (5)$$

8.4.5 Foldback Current Limit and Short-Circuit Protection

Foldback current limit and short-circuit protection is valid for devices where foldback current limit is enabled.

When the device detects current limit for more than 1024 subsequent switching cycles, the device reduces the current limit from the nominal value to typically 1.8A. Foldback current limit is left when the current limit indication goes away. For the case that device operation continues in current limit, the device can, after 3072 switching cycles, try again full current limit for again 1024 switching cycles.

8.4.6 Output Discharge

The purpose of the discharge function is to make sure of a defined down-ramp of the output voltage when the device is being disabled but also to keep the output voltage close to 0V when the device is off. The output discharge feature is only active after TPS6281x has been enabled at least once after the supply voltage is applied. The discharge function is enabled as soon as the device is disabled, in thermal shutdown, or in undervoltage lockout. The minimum supply voltage required for the discharge function to remain active typically is 2V. Output discharge is not activated during a current limit or foldback current limit event. When supply voltage is applied but the device has not been enabled yet, the discharge function is undefined. For applications where the output voltage discharge has to be off after supply voltage is applied and the enable pin is still at low level, use the versions that are stated as *Output discharge disconnected* in the [Device Comparison Table](#).

8.4.7 Soft Start / Tracking (SS/TR)

The internal soft-start circuitry controls the output voltage slope during start-up. This control avoids excessive inrush current and makes sure of a controlled output voltage rise time. This control also prevents unwanted

voltage drops from high impedance power sources or batteries. When EN is set high to start operation, the device starts switching after a delay of about 200µs then the internal reference and hence V_{OUT} rises with a slope controlled by an external capacitor connected to the SS/TR pin.

Leaving the SS/TR pin unconnected provides the fastest start-up ramp with 150µs typically. A capacitor connected from SS/TR to GND is charged with 2.5µA by an internal current source during soft start until reaching the reference voltage of 0.6V. The capacitance required to set a certain ramp-time (t_{ramp}) therefore is:

$$C_{SS}[nF] = \frac{2.5\mu A \cdot t_{ramp}[ms]}{0.6V} \quad (6)$$

If the device is set to shutdown (EN = GND), undervoltage lockout, or thermal shutdown, an internal resistor pulls the SS/TR pin to GND to make sure of a proper low level. Returning from those states causes a new start-up sequence.

A voltage applied at SS/TR can be used to track the voltage on external source. The output voltage follows this voltage in both directions up and down in forced PWM mode. In PFM mode, the output voltage decreases based on the load current. The SS/TR pin must not be connected to the SS/TR pin of other devices. An external voltage applied on SS/TR is internally clamped to the feedback voltage (0.6V). TI recommends to set the target for the external voltage on SS/TR slightly above the feedback voltage. Given the tolerances of the resistor divider R₅ and R₆ on SS/TR, this action makes sure the device *switches* to the internal reference voltage when the power-up sequencing is finished. See [Figure 9-58](#).

9 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

9.1 Application Information

9.1.1 Programming the Output Voltage

The output voltage of the TPS6281x is adjustable. The output voltage can be programmed for output voltages from 0.6V to 5.5V using a resistor divider from VOUT to GND. The voltage at the FB pin is regulated to 600mV. The value of the output voltage is set by the selection of the resistor divider from [Equation 7](#). TI recommends to choose resistor values which allow a current of at least 2μA, meaning the value of R₂ must not exceed 400kΩ. TI recommends lower resistor values for highest accuracy and most robust design.

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (7)$$

9.1.2 External Component Selection

9.1.2.1 Inductor Selection

The TPS6281x is designed for a nominal 0.47μH inductor with a switching frequency of typically 2.25MHz. Larger values can be used to achieve a lower inductor current ripple but can have a negative impact on efficiency and transient response. Smaller values than 0.47μH cause a larger inductor current ripple which causes larger negative inductor current in forced PWM mode at low or no output current. For a higher or lower nominal switching frequency, the inductance must be changed accordingly. See also [Recommended Operating Conditions](#)

The inductor selection is affected by several effects like inductor ripple current, output ripple voltage, PWM-to-PFM transition point, and efficiency. In addition, the inductor selected has to be rated for appropriate saturation current and DC resistance (DCR). [Equation 8](#) calculates the maximum inductor current.

$$I_{L(max)} = I_{OUT(max)} + \frac{\Delta I_{L(max)}}{2} \quad (8)$$

$$\Delta I_{L(max)} = \frac{V_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}} \right)}{L \min} \cdot \frac{1}{f_{SW}} \quad (9)$$

where

- I_{L(max)} is the maximum inductor current
- ΔI_{L(max)} is the peak-to-peak inductor ripple current
- Lmin is the minimum inductance at the operating point

Table 9-1. Typical Inductors

TYPE	INDUCTANCE [μH]	CURRENT [A] (1)	FOR DEVICE	NOMINAL SWITCHING FREQUENCY	DIMENSIONS [LxBxH] mm	MANUFACTURER(2)
XFL4015-471ME	0.47μH, ±20%	3.5	TPS62813, TPS62812	2.25MHz	4 × 4 × 1.6	Coilcraft
XEL4020-561ME	0.56μH, ±20%	9.9	TPS62810, TPS62813, TPS62812, TPS62811	2.25MHz	4 × 4 × 2.1	Coilcraft
XEL4030-471ME	0.47μH, ±20%	12.3	TPS62810, TPS62813, TPS62812	2.25MHz	4 × 4 × 3.1	Coilcraft
XEL3515-561ME	0.56μH, ±20%	4.5	TPS62813, TPS62812, TPS62811	2.25MHz	3.5 × 3.2 × 1.5	Coilcraft
XFL3012-331MEB	0.33μH, ±20%	2.6	TPS62812, TPS62811	≥ 3.5MHz	3 × 3 × 1.3	Coilcraft
XPL2010-681ML	0.68μH, ±20%	1.5	TPS62811	2.25MHz	2 × 1.9 × 1	Coilcraft
DFE252012PD-R47M	0.47μH, ±20%	See datasheet	TPS62813, TPS62812, TPS62811	2.25MHz	2.5 × 2 × 1.2	Murata

(1) Lower of I_{RMS} at 20°C rise or I_{SAT} at 20% drop.

(2) See the [Third-Party Products Disclaimer](#).

Calculating the maximum inductor current using the actual operating conditions gives the minimum saturation current of the inductor needed. TI recommends a margin of about 20% to add. A larger inductor value is also useful to get lower ripple current, but increases the transient response time and size as well.

9.1.3 Capacitor Selection

9.1.3.1 Input Capacitor

For most applications, 22μF nominal is sufficient and recommended. The input capacitor buffers the input voltage for transient events and also decouples the converter from the supply. TI recommends a low-ESR multilayer ceramic capacitor (MLCC) for best filtering and must be placed between VIN and GND as close as possible to those pins.

9.1.3.2 Output Capacitor

The architecture of the TPS6281x allows the use of tiny ceramic output capacitors with low equivalent series resistance (ESR). These capacitors provide low output voltage ripple and are recommended. To keep the low resistance up to high frequencies and to get narrow capacitance variation with temperature, TI recommends to use dielectric X7R, X7T, or an equivalent. Using a higher value has advantages like smaller voltage ripple and a tighter DC output accuracy in power save mode. By changing the device compensation with a resistor from COMP/FSET to GND, the device can be compensated in three steps based on the minimum capacitance used on the output. The maximum capacitance is 470μF in any of the compensation settings.

The minimum capacitance required on the output depends on the compensation setting as well as on the current rating of the device. TPS62810 and TPS62813 require a minimum output capacitance of 27μF while the lower current versions TPS62812 and TPS62811 require 15μF at minimum. The required output capacitance also changes with the output voltage.

For output voltages below 1V, the minimum increases linearly from 32μF at 1V to 53μF at 0.6V for the TPS62810, and the TPS62813 with the compensation setting for smallest output capacitance. Other compensation ranges for TPS62811 and TPS62812, or both are equivalent. See also [Table 8-1](#) and [Table 8-2](#).

9.2 Typical Application

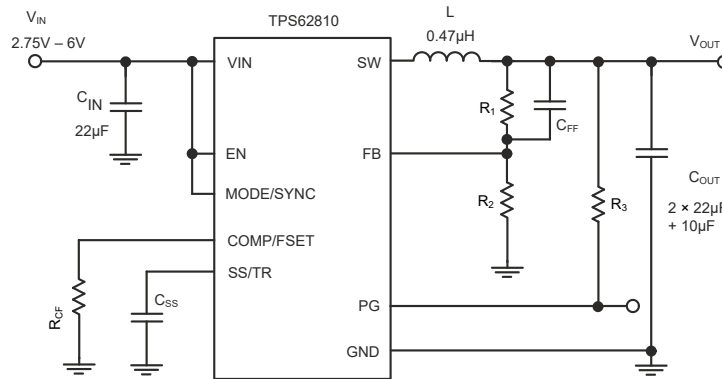


Figure 9-1. Typical Application

9.2.1 Design Requirements

The design guidelines provide a component selection to operate the device within the recommended operating conditions.

9.2.2 Detailed Design Procedure

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (10)$$

With $V_{FB} = 0.6V$:

Table 9-2. Setting the Output Voltage

NOMINAL OUTPUT VOLTAGE V_{OUT}	R_1	R_2	C_{FF}	EXACT OUTPUT VOLTAGE
0.8V	16.9kΩ	51kΩ	10pF	0.7988V
1.0V	20kΩ	30kΩ	10pF	1.0V
1.1V	39.2kΩ	47kΩ	10pF	1.101V
1.2V	68kΩ	68kΩ	10pF	1.2V
1.5V	76.8kΩ	51kΩ	10pF	1.5V
1.8V	80.6kΩ	40.2kΩ	10pF	1.803V
2.5V	47.5kΩ	15kΩ	10pF	2.5V
3.3V	88.7kΩ	19.6kΩ	10pF	3.315V

9.2.3 Application Curves

All plots have been taken with a nominal switching frequency of 2.25MHz when set to PWM mode, unless otherwise noted. The BOM is according to [Table 7-1](#).

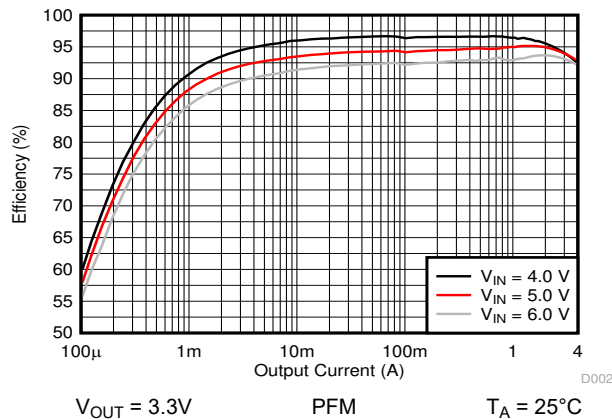


Figure 9-2. Efficiency versus Output Current

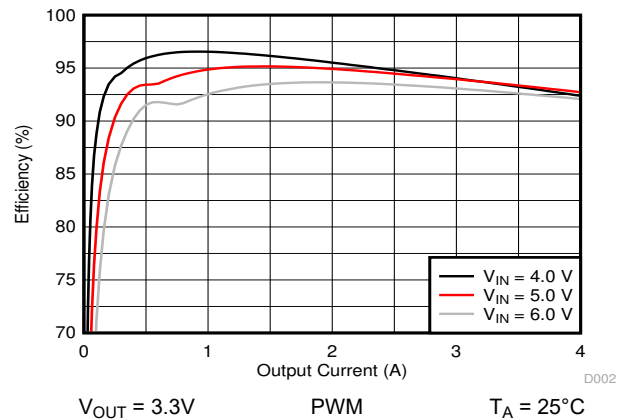


Figure 9-3. Efficiency versus Output Current

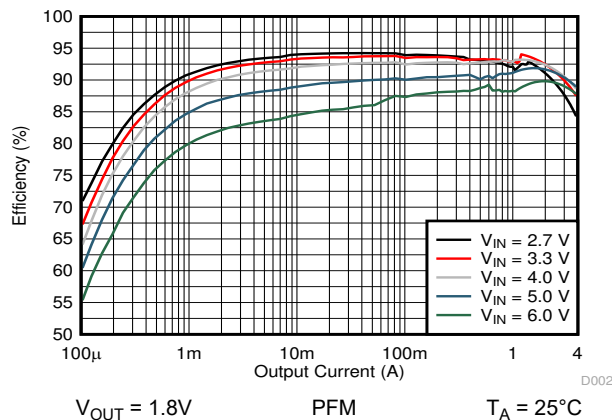


Figure 9-4. Efficiency versus Output Current

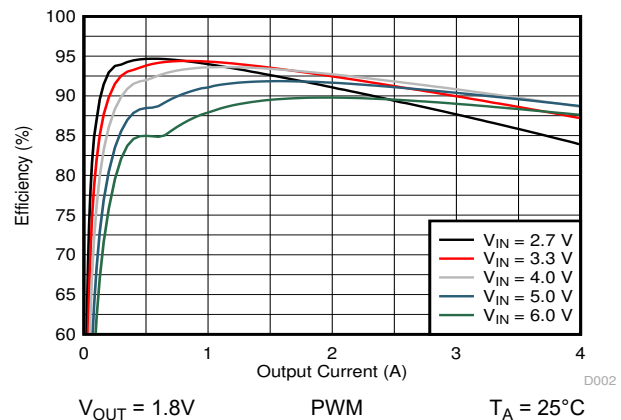


Figure 9-5. Efficiency versus Output Current

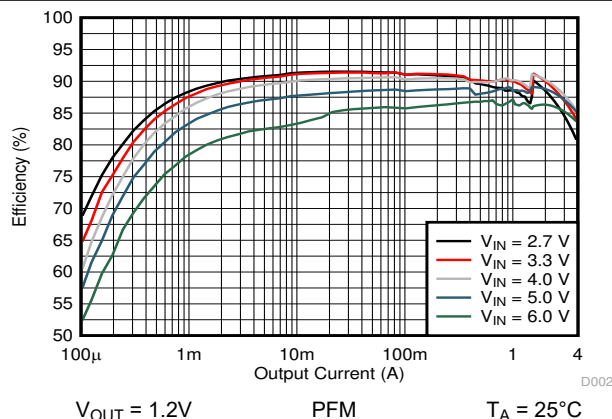


Figure 9-6. Efficiency versus Output Current

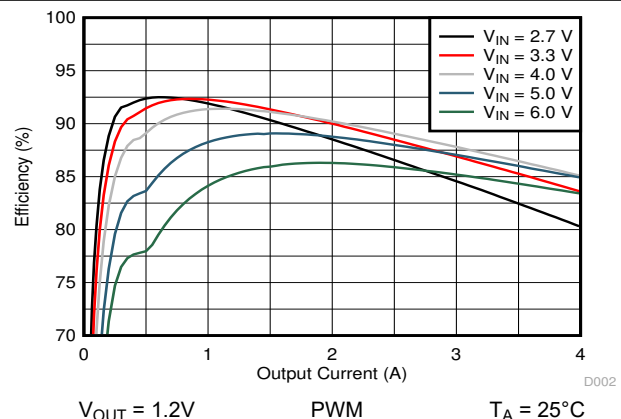


Figure 9-7. Efficiency versus Output Current

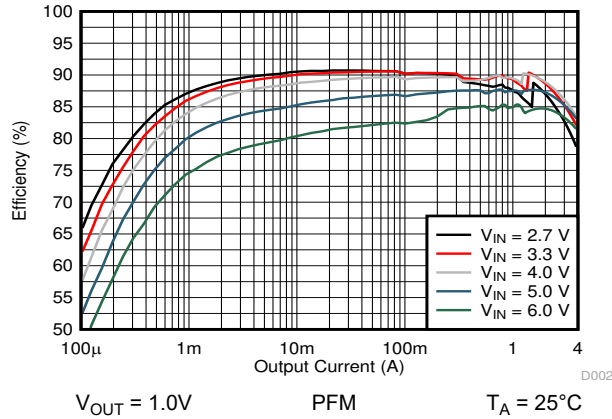


Figure 9-8. Efficiency versus Output Current

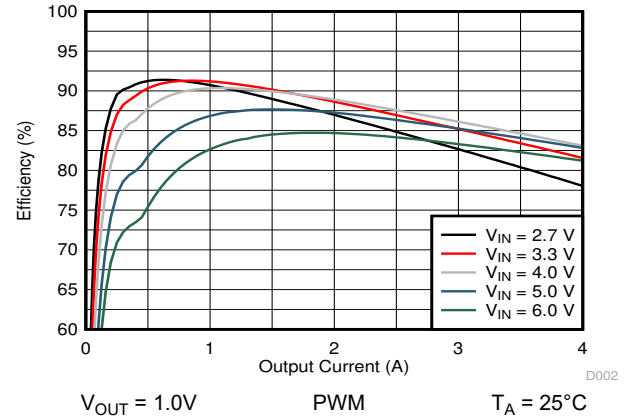


Figure 9-9. Efficiency versus Output Current

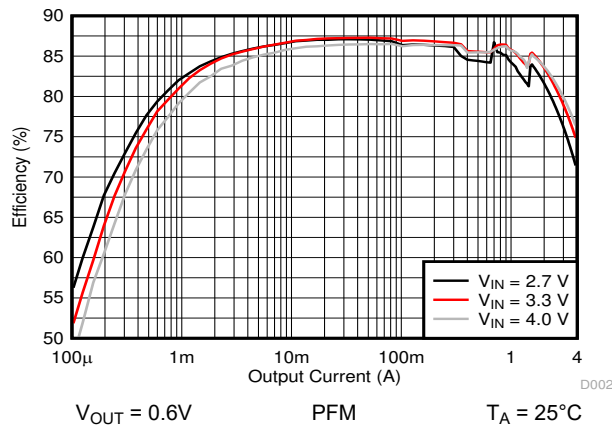


Figure 9-10. Efficiency versus Output Current

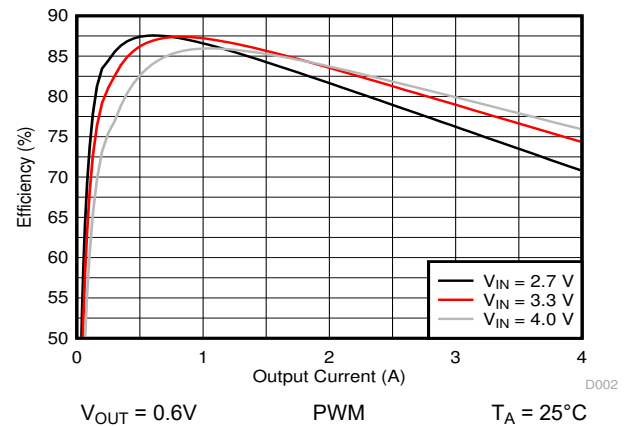


Figure 9-11. Efficiency versus Output Current

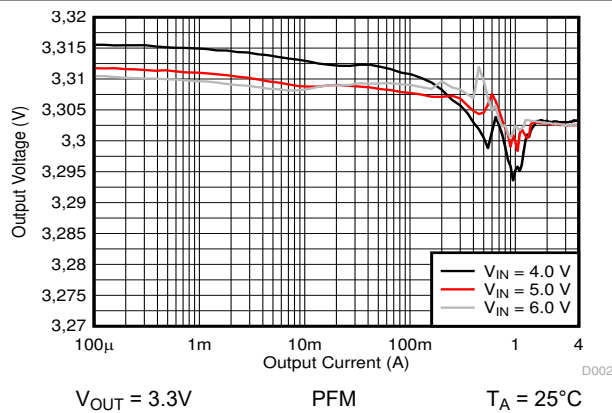


Figure 9-12. Output Voltage versus Output Current

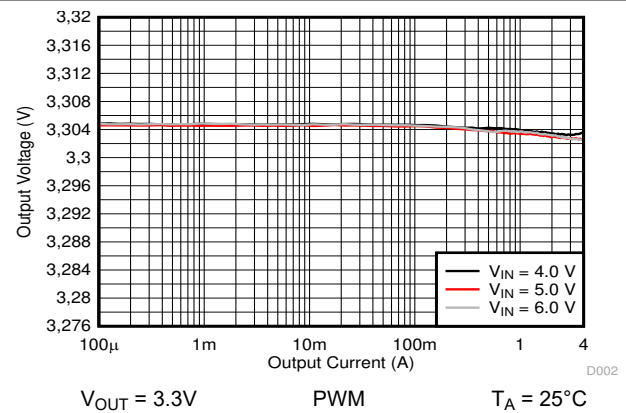


Figure 9-13. Output Voltage versus Output Current

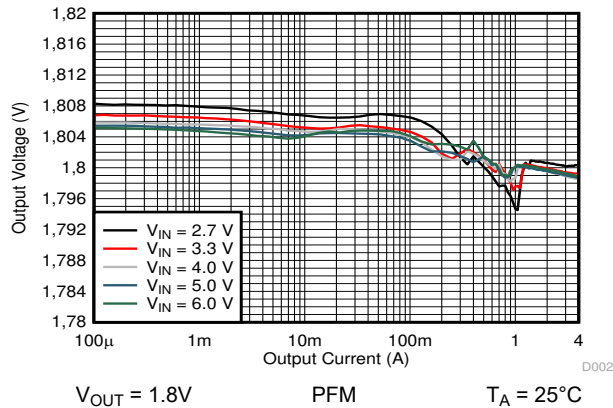


Figure 9-14. Output Voltage versus Output Current

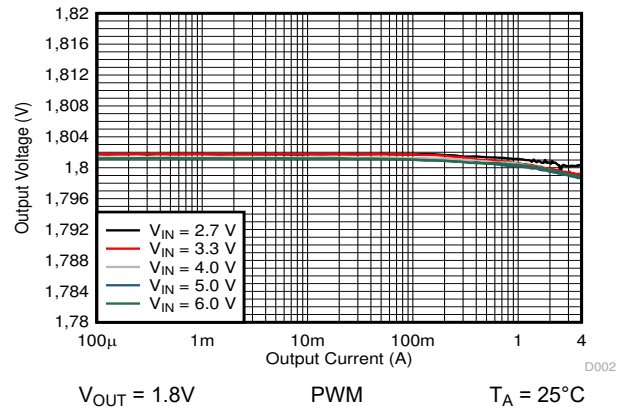


Figure 9-15. Output Voltage versus Output Current

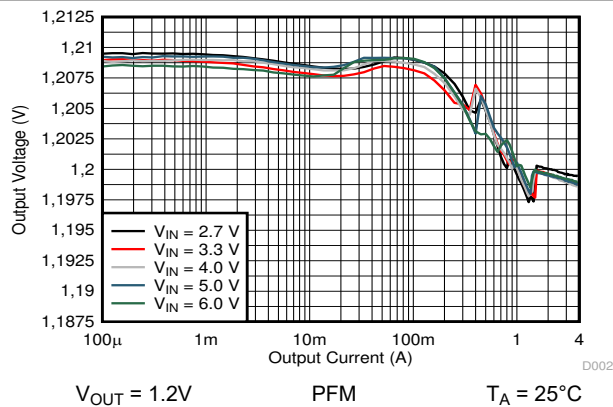


Figure 9-16. Output Voltage versus Output Current

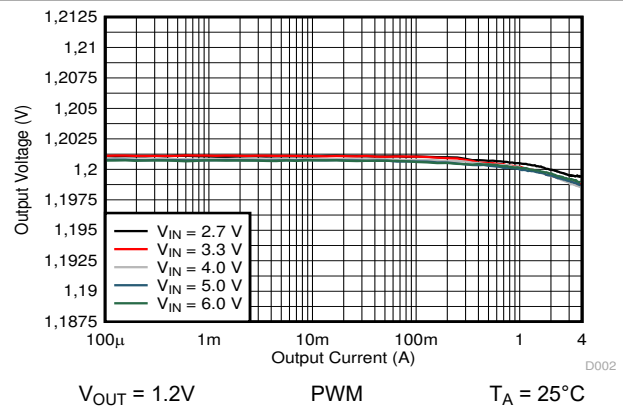


Figure 9-17. Output Voltage versus Output Current

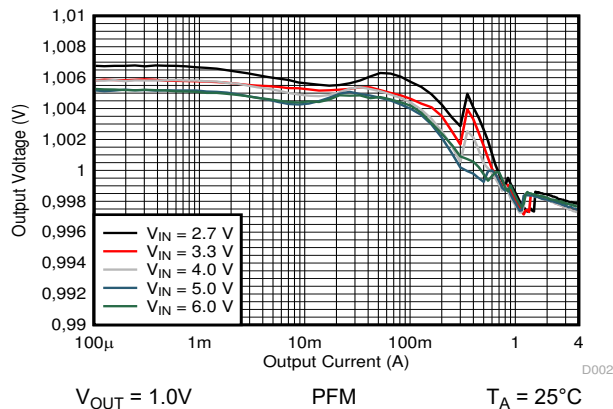


Figure 9-18. Output Voltage versus Output Current

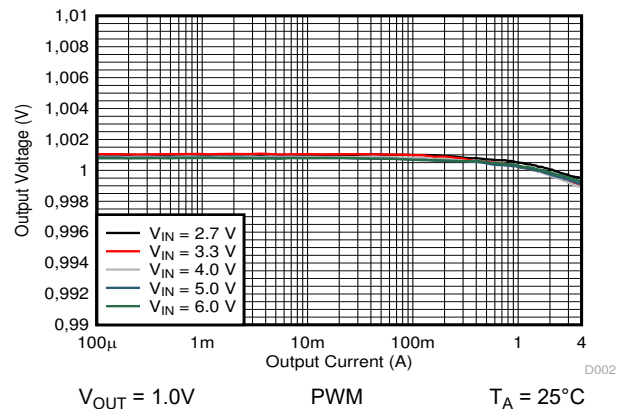


Figure 9-19. Output Voltage versus Output Current

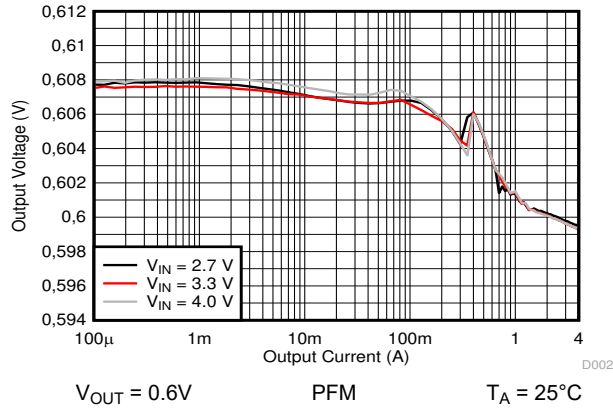


Figure 9-20. Output Voltage versus Output Current

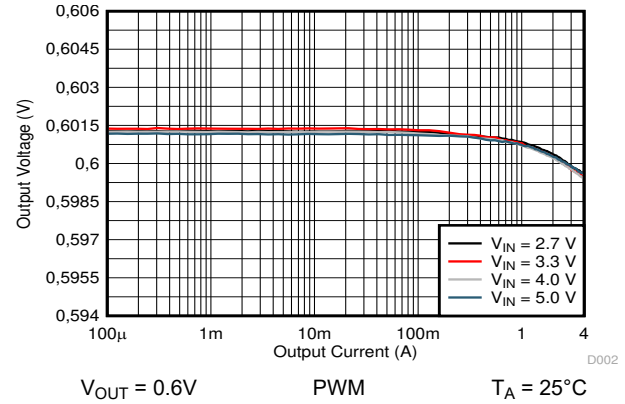


Figure 9-21. Output Voltage versus Output Current

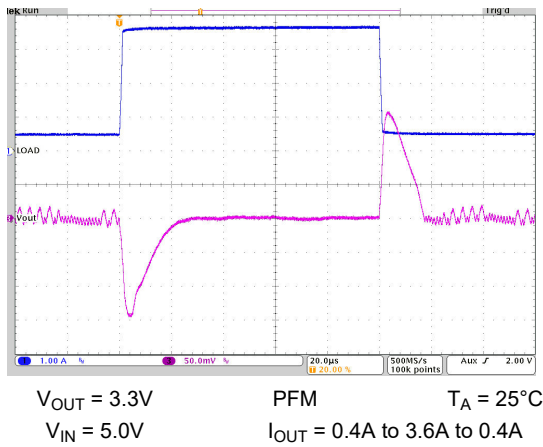


Figure 9-22. Load Transient Response

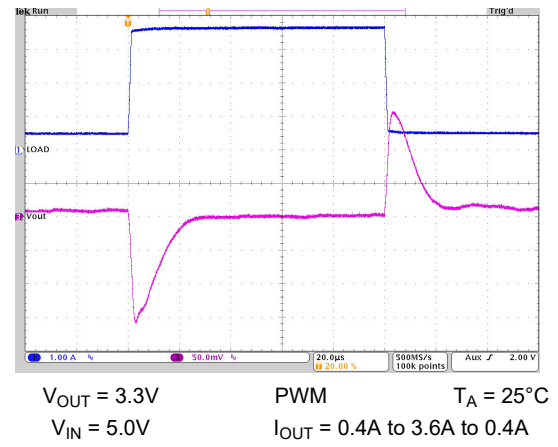


Figure 9-23. Load Transient Response

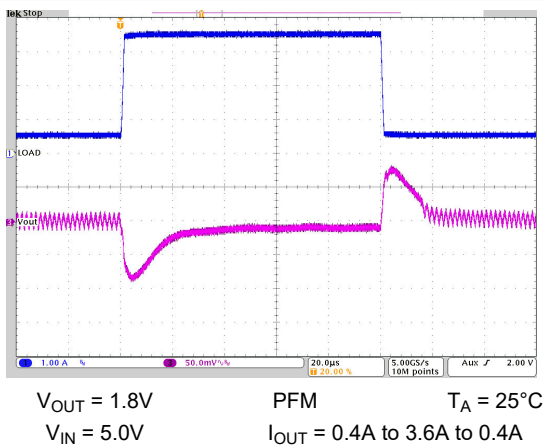


Figure 9-24. Load Transient Response

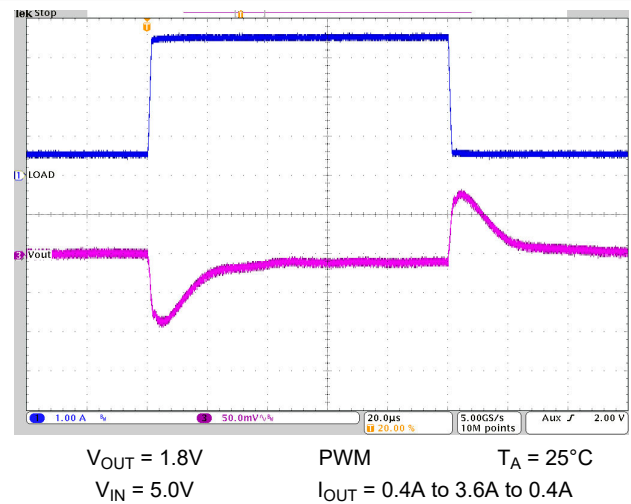
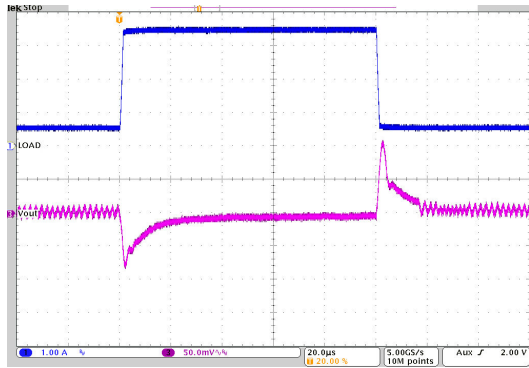
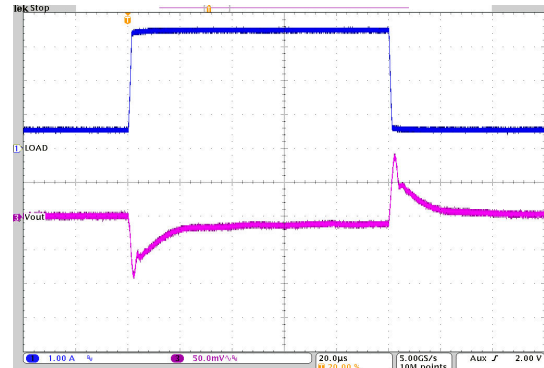


Figure 9-25. Load Transient Response



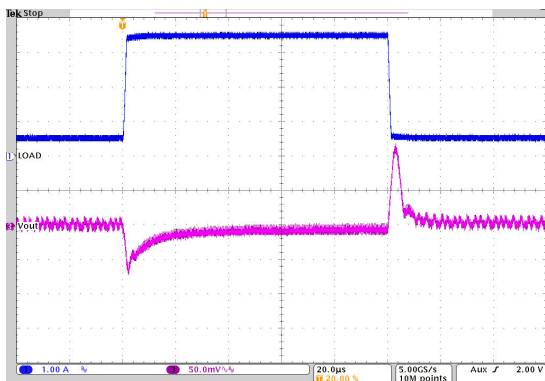
$V_{OUT} = 1.2V$ PFM $T_A = 25^\circ C$
 $V_{IN} = 5.0V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-26. Load Transient Response



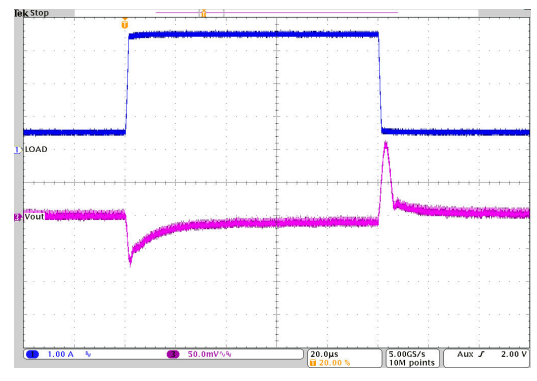
$V_{OUT} = 1.2V$ PWM $T_A = 25^\circ C$
 $V_{IN} = 5.0V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-27. Load Transient Response



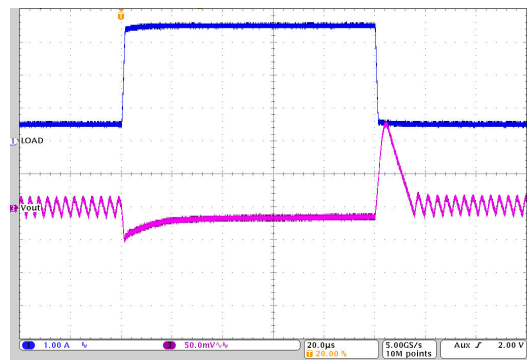
$V_{OUT} = 1.0V$ PFM $T_A = 25^\circ C$
 $V_{IN} = 5.0V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-28. Load Transient Response



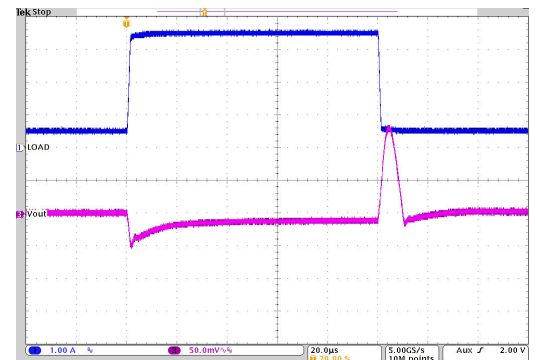
$V_{OUT} = 1.0V$ PWM $T_A = 25^\circ C$
 $V_{IN} = 5.0V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-29. Load Transient Response



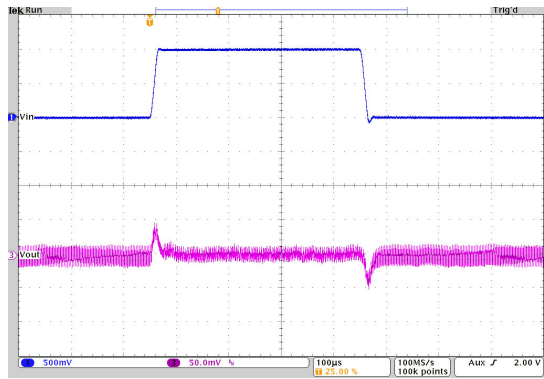
$V_{OUT} = 0.6V$ PFM $T_A = 25^\circ C$
 $V_{IN} = 3.3V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-30. Load Transient Response



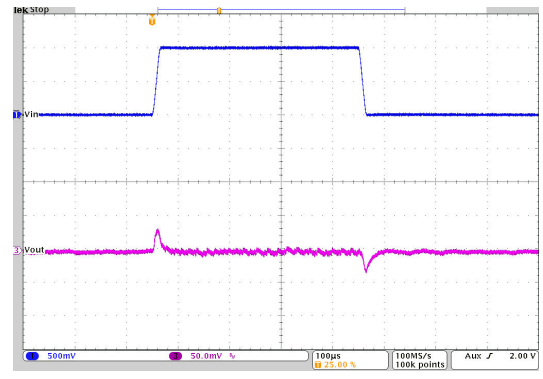
$V_{OUT} = 0.6V$ PWM $T_A = 25^\circ C$
 $V_{IN} = 3.3V$ $I_{OUT} = 0.4A$ to $3.6A$ to $0.4A$

Figure 9-31. Load Transient Response



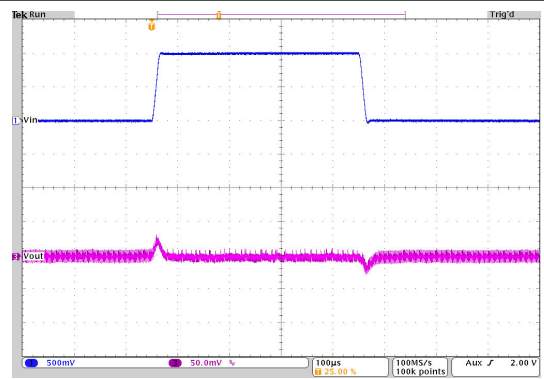
$V_{OUT} = 3.3V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-32. Line Transient Response



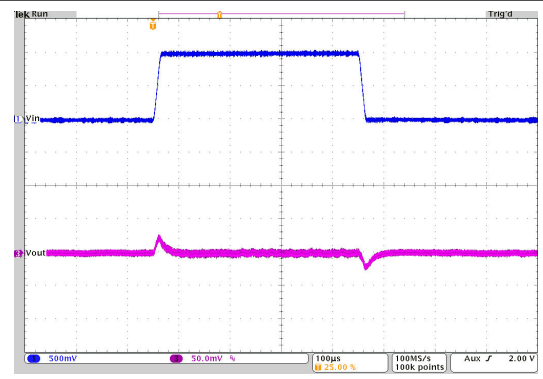
$V_{OUT} = 3.3V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-33. Line Transient Response



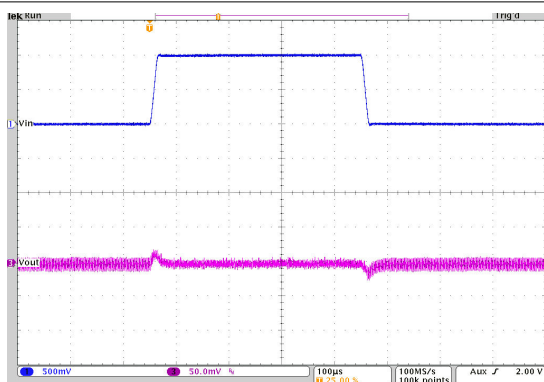
$V_{OUT} = 1.8V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-34. Line Transient Response



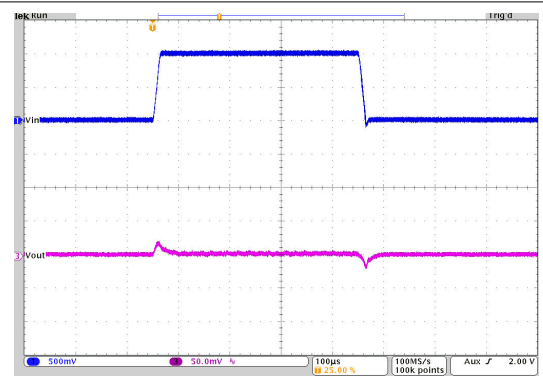
$V_{OUT} = 1.8V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-35. Line Transient Response



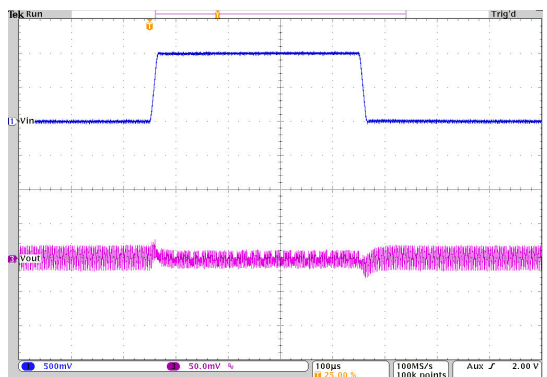
$V_{OUT} = 1.2V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-36. Line Transient Response



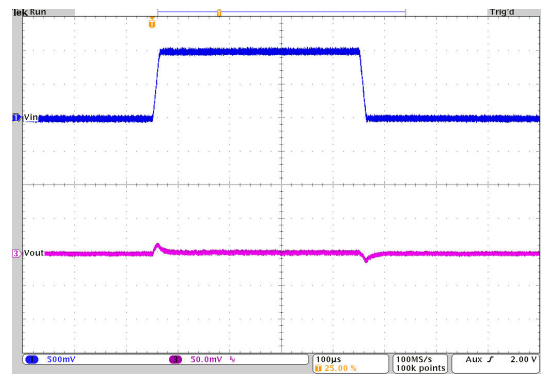
$V_{OUT} = 1.2V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-37. Line Transient Response



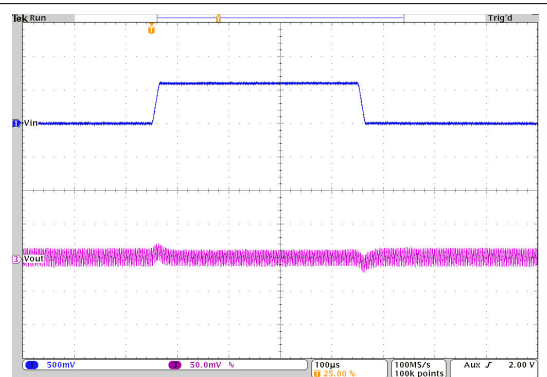
$V_{OUT} = 1.0V$ PFM $T_A = 25^\circ C$
 $I_{OUT} = 0.5A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-38. Line Transient Response



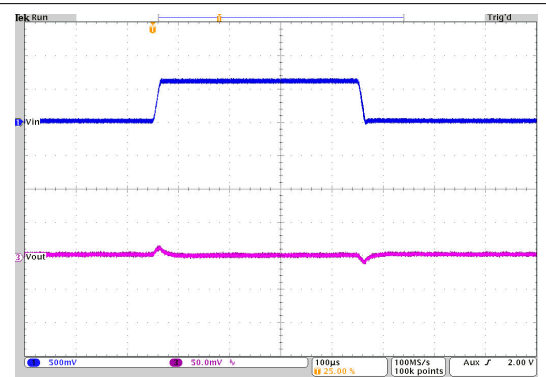
$V_{OUT} = 1.0V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 4.5V \text{ to } 5.5V \text{ to } 4.5V$

Figure 9-39. Line Transient Response



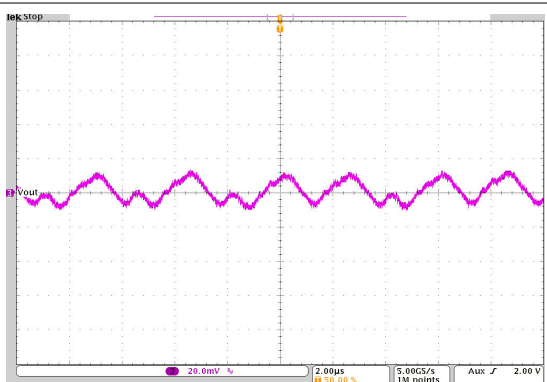
$V_{OUT} = 0.6V$ PFM $T_A = 25^\circ C$
 $I_{OUT} = 0.5A$ $V_{IN} = 3.0V \text{ to } 3.6V \text{ to } 3.0V$

Figure 9-40. Line Transient Response



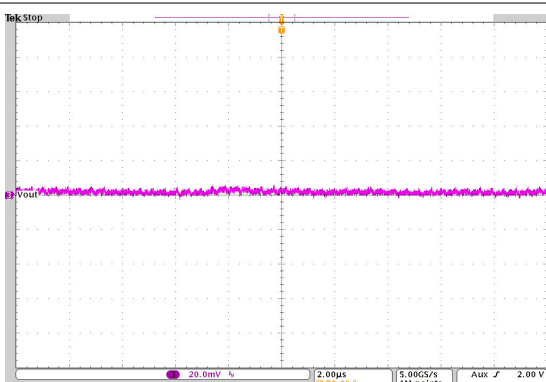
$V_{OUT} = 0.6V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 3.0V \text{ to } 3.6V \text{ to } 3.0V$

Figure 9-41. Line Transient Response



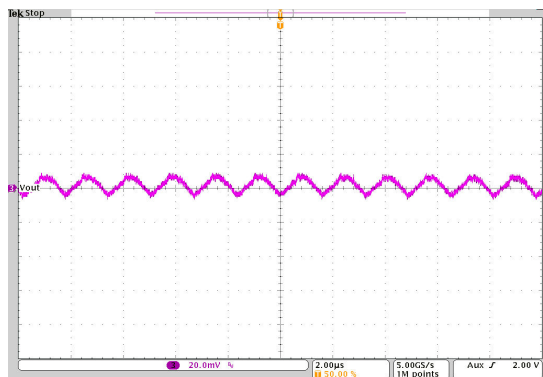
$V_{OUT} = 3.3V$ PFM $T_A = 25^\circ C$
 $I_{OUT} = 0.5A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-42. Output Voltage Ripple



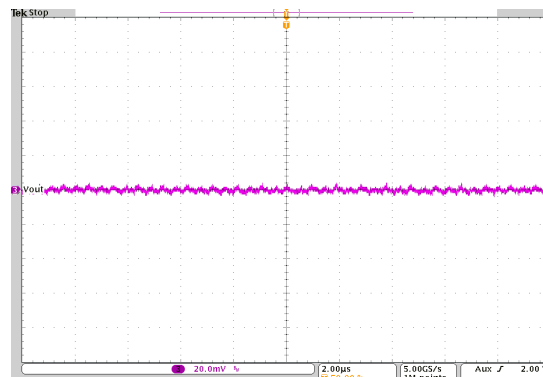
$V_{OUT} = 3.3V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-43. Output Voltage Ripple



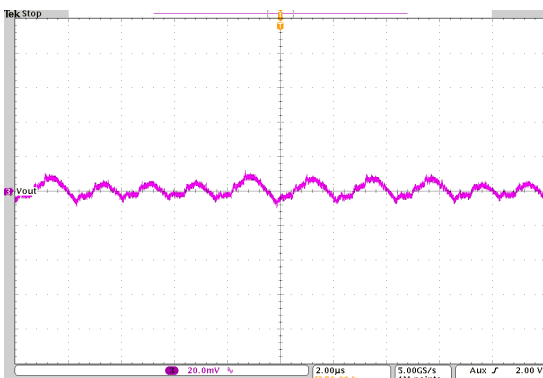
$V_{OUT} = 1.8V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-44. Output Voltage Ripple



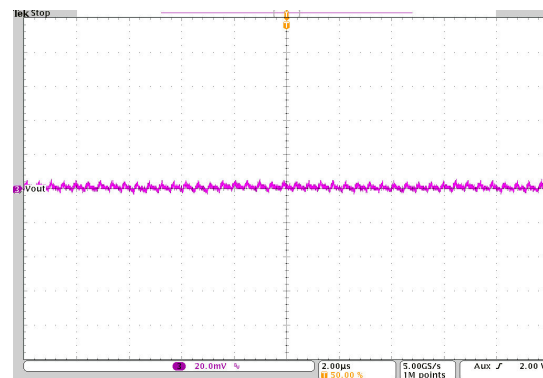
$V_{OUT} = 1.8V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-45. Output Voltage Ripple



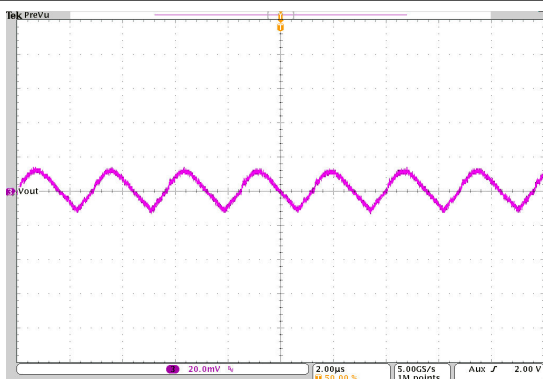
$V_{OUT} = 1.2V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-46. Output Voltage Ripple



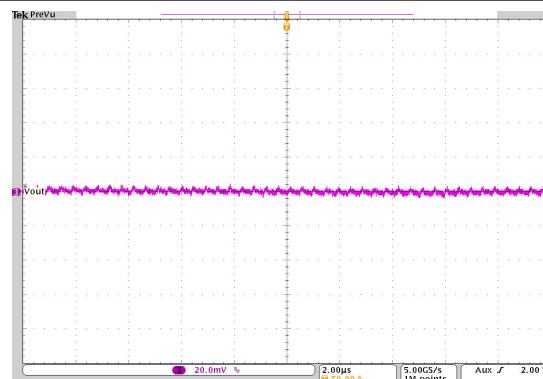
$V_{OUT} = 1.2V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-47. Output Voltage Ripple



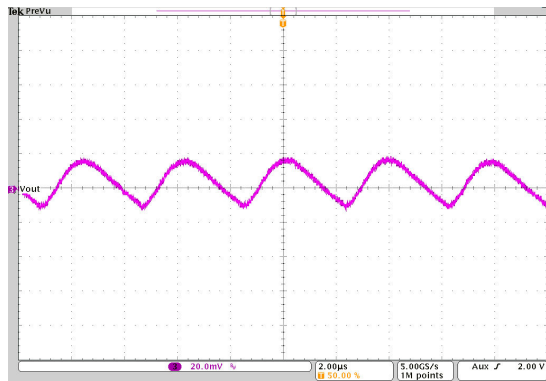
$V_{OUT} = 1.0V$ PFM $T_A = 25^{\circ}C$
 $I_{OUT} = 0.5A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-48. Output Voltage Ripple



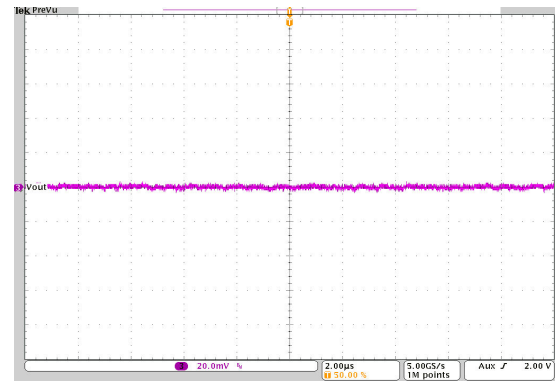
$V_{OUT} = 1.0V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 5.0V$ BW = 20MHz

Figure 9-49. Output Voltage Ripple



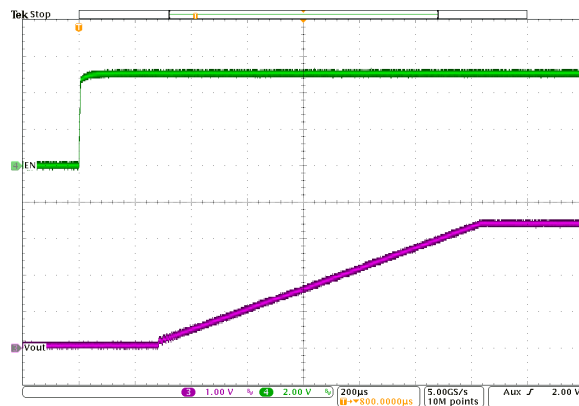
$V_{OUT} = 0.6V$ PFM $T_A = 25^\circ C$
 $I_{OUT} = 0.5A$ $V_{IN} = 3.3V$ BW = 20MHz

Figure 9-50. Output Voltage Ripple



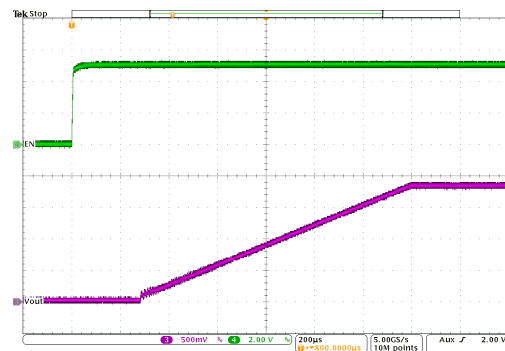
$V_{OUT} = 0.6V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 3.3V$ BW = 20MHz

Figure 9-51. Output Voltage Ripple



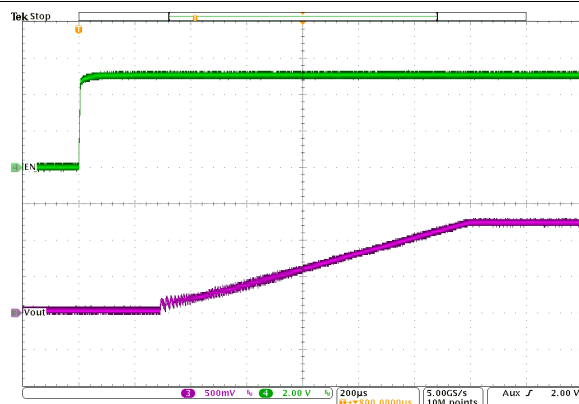
$V_{OUT} = 3.3V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 5V$ $C_{SS} = 4.7nF$

Figure 9-52. Start-Up Timing



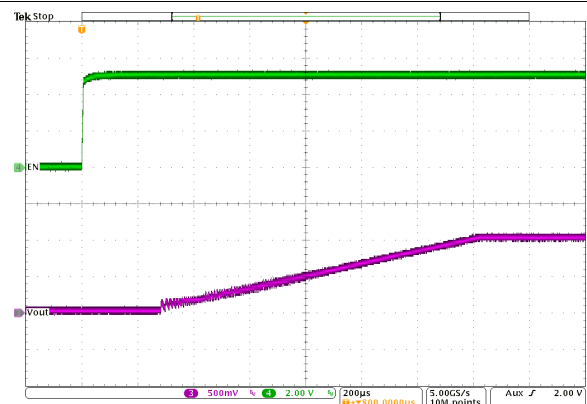
$V_{OUT} = 1.8V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 5V$ $C_{SS} = 4.7nF$

Figure 9-53. Start-Up Timing



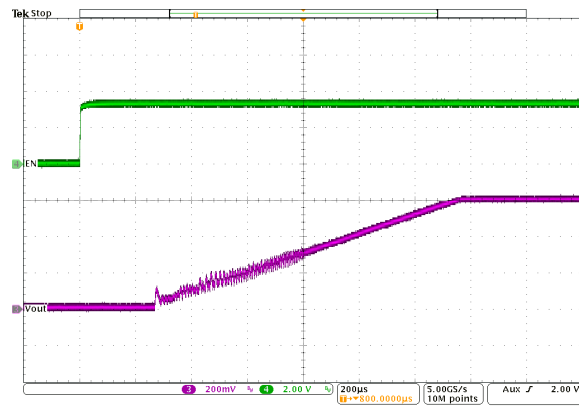
$V_{OUT} = 1.2V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 5V$ $C_{SS} = 4.7nF$

Figure 9-54. Start-Up Timing



$V_{OUT} = 1.0V$ PWM $T_A = 25^\circ C$
 $I_{OUT} = 4A$ $V_{IN} = 5V$ $C_{SS} = 4.7nF$

Figure 9-55. Start-Up Timing



$V_{OUT} = 0.6V$ PWM $T_A = 25^{\circ}C$
 $I_{OUT} = 4A$ $V_{IN} = 3.3V$ $C_{SS} = 4.7nF$

Figure 9-56. Start-up Timing

9.3 System Examples

9.3.1 Fixed Output Voltage Versions

Versions with an internally fixed output voltage allow the user remove the external feedback voltage divider. This ability not only allows the user reduce the total design size but also provides higher accuracy as there is no additional error caused by the external resistor divider. The FB pin must be tied to the output voltage directly as shown in Figure 9-57. Independent of that, the application shown runs with an internally defined switching frequency of 2.25MHz by connecting COMP/FSET to GND.

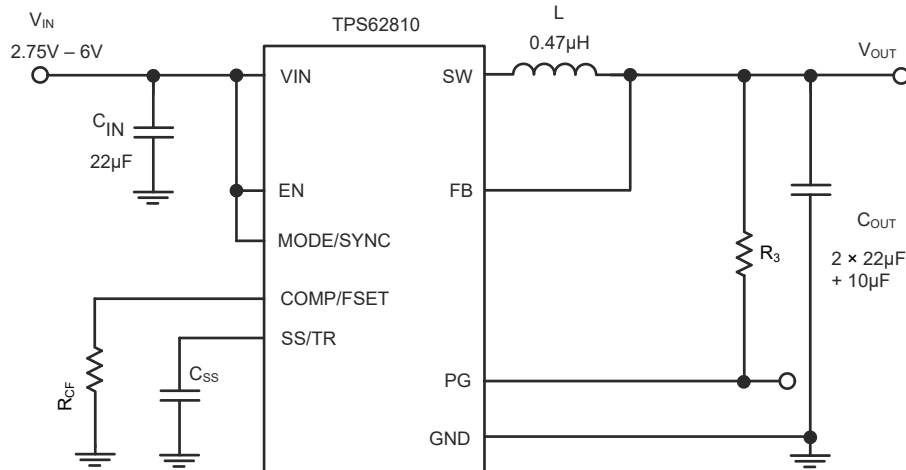


Figure 9-57. Schematic for Fixed Output Voltage Versions

9.3.2 Voltage Tracking

The TPS6281x follows the voltage applied to the SS/TR pin. A voltage ramp on SS/TR to 0.6V ramps the output voltage according to the 0.6V feedback voltage.

Tracking the 3.3V of device 1, such that both rails reach the target voltage at the same time, requires a resistor divider on SS/TR of device 2 equal to the output voltage divider of device 1. The output current of 2.5µA on the SS/TR pin causes an offset voltage on the resistor divider formed by R_5 and R_6 . The equivalent resistance of $R_5 \parallel R_6$, so keep below 15kΩ. The current from SS/TR causes a slightly higher voltage across R_6 than 0.6V, which is desired because device 2 switches to the internal reference as soon as the voltage at SS/TR is higher than 0.6V.

In case both devices must run in forced PWM mode, TI recommends to tie the MODE pin of device 2 to the output voltage or the power good signal of device 1, the primary device. The TPS6281x has a duty cycle limitation defined by the minimum on-time. For tracking down to low output voltages, device 2 cannot follow the minimum duty cycle is reached. Enabling PFM mode while tracking is in progress allows the user to ramp down the output voltage close to 0V.

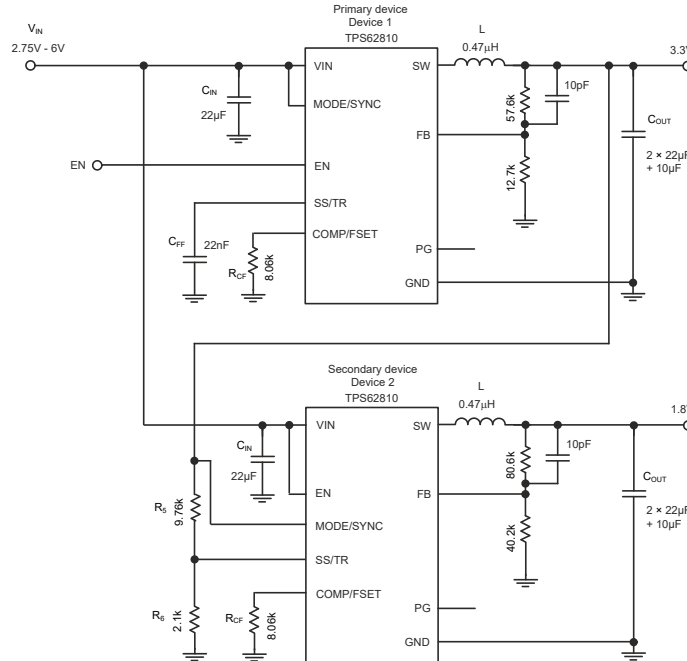


Figure 9-58. Schematic for Output Voltage Tracking

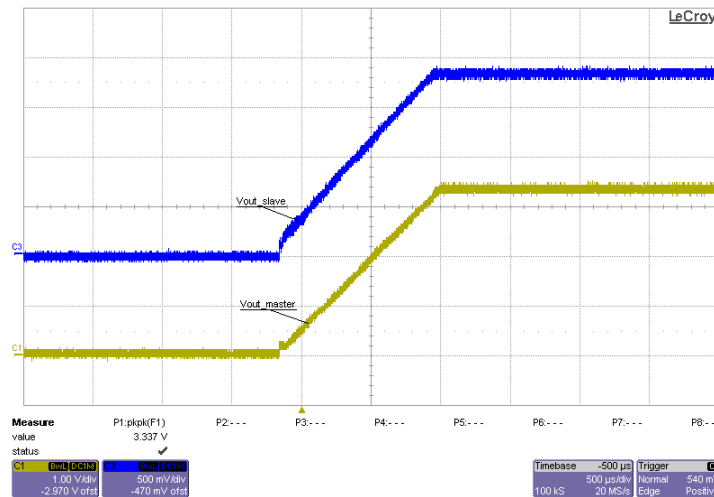


Figure 9-59. Scope Plot for Output Voltage Tracking

9.3.3 Synchronizing to an External Clock

The TPS6281x can be externally synchronized by applying an external clock on the MODE/SYNC pin. There is no need for any additional circuitry as long as the input signal meets the requirements given in the electrical specifications. The clock can be applied, removed during operation, allowing the user to switch from an externally-defined fixed frequency to power-save mode or to internal fixed frequency operation. The value of the R_{CF} resistor must be chosen so that the internally defined frequency and the externally applied frequency are close to each other. This action makes sure of a smooth transition from internal to external frequency and vice versa.

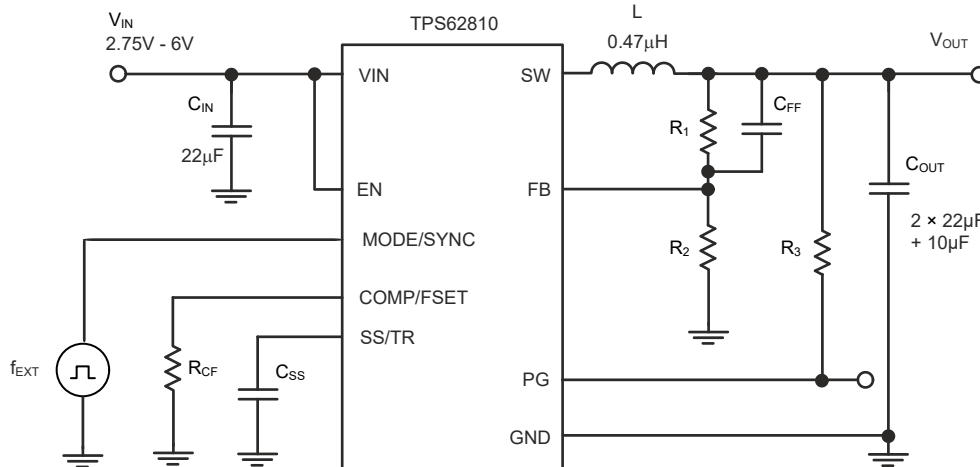


Figure 9-60. Schematic Using External Synchronization

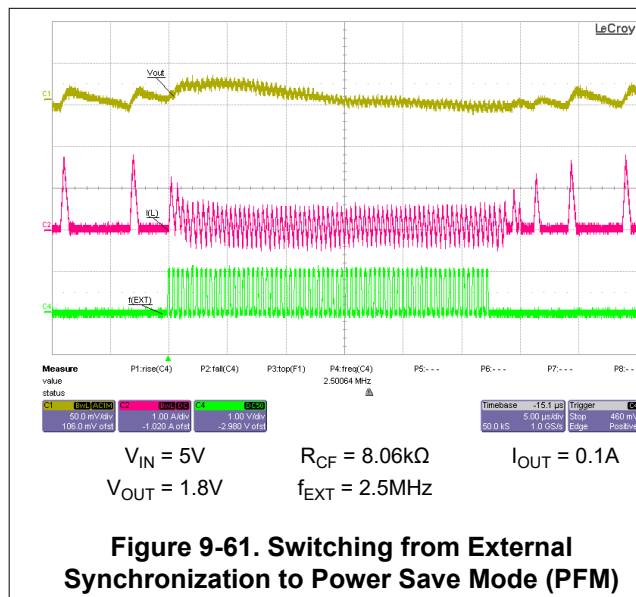


Figure 9-61. Switching from External Synchronization to Power Save Mode (PFM)

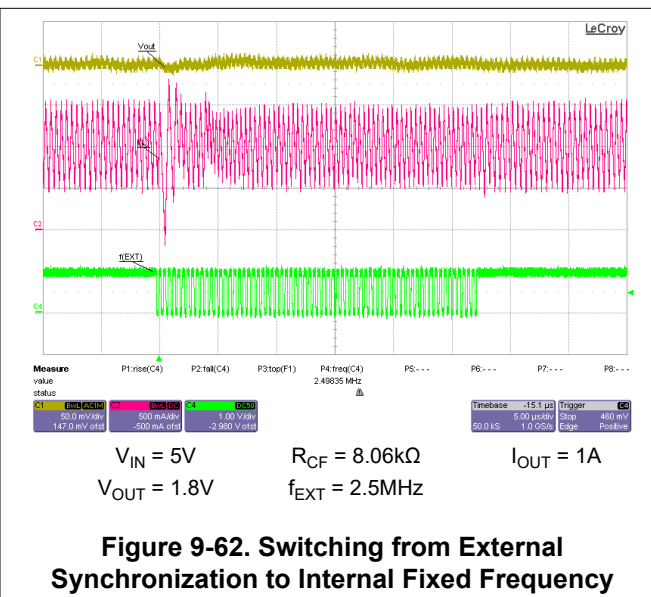


Figure 9-62. Switching from External Synchronization to Internal Fixed Frequency

9.4 Power Supply Recommendations

The TPS6281x device family has no special requirements for the input power supply. The output current of the input power supply must be rated according to the supply voltage, output voltage, and output current of the TPS6281x.

9.5 Layout

9.5.1 Layout Guidelines

A proper layout is critical for the operation of a switched mode power supply, even more at high switching frequencies. Therefore, the PCB layout of the TPS6281x demands careful attention to make sure of operation and to get the performance specified. A poor layout can lead to issues like poor regulation (both line and load), stability and accuracy weaknesses increased EMI radiation and noise sensitivity.

See [Layout Example](#) for the recommended layout of the TPS6281x, which is designed for common external ground connections. The input capacitor must be placed as close as possible between the VIN and GND pin.

Provide low inductive and resistive paths for loops with high di/dt. Therefore, paths conducting the switched load current must be as short and wide as possible. Provide low capacitive paths (with respect to all other nodes) for

wires with high dv/dt . Therefore, the input and output capacitance must be placed as close as possible to the IC pins and parallel wiring over long distances as well as narrow traces must be avoided. Loops that conduct an alternating current must outline an area as small as possible, as this area is proportional to the energy radiated.

Sensitive nodes like FB must be connected with short wires and not nearby high dv/dt signals (for example, SW). Because sensitive nodes carry information about the output voltage, sensitive nodes must be connected as close as possible to the actual output voltage (at the output capacitor). The capacitor on the SS/TR pin as well as the FB resistors, R_1 and R_2 , must be kept close to the IC and connect directly to those pins and the system ground plane.

The package uses the pins for power dissipation. Thermal vias on the VIN and GND pins help spread the heat into the pcb.

The recommended layout is implemented on the EVM and shown in the [TPS62810EVM-015 Evaluation Module user's guide](#).

9.5.2 Layout Example

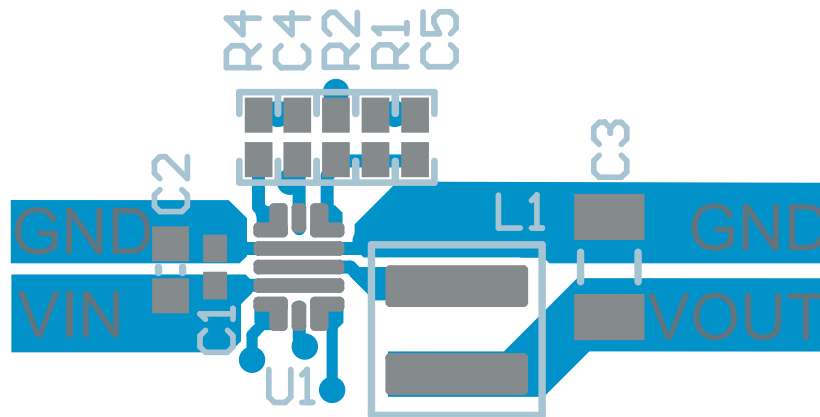


Figure 9-63. Example Layout

10 Device and Documentation Support

10.1 Device Support

10.1.1 Third-Party Products Disclaimer

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

10.2 Documentation Support

10.2.1 Related Documentation

For related documentation see the following:

Texas Instruments, [TPS62810EVM-015 Evaluation Module user's guide](#)

10.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

10.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

10.5 Trademarks

TI E2E™ is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

10.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

10.7 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

11 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision * (November 2022) to Revision A (August 2026)	Page
• First public release of the datasheet.....	1
• Changed document status from Production Mix to full Production Data.....	1
• Updated all instances of legacy terminology to primary device and secondary device.....	1
• Added Functional Safety-Capable bullets and external links to the <i>Features</i>	1
• Updated the <i>Applications</i> list for industrial devices.....	1
• Added TPS62811 to the document.....	1
• Changed the status of TPS62810 and TPS62812 from Product Preview to Production Data.....	1
• Updated the device name in all schematic figures throughout the document.....	1
• Added new output current versions to the <i>Device Comparison Table</i>	3
• Added description to RCF parameter.....	5

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS62810RWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	810
TPS62811RWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	811
TPS62812RWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	812

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

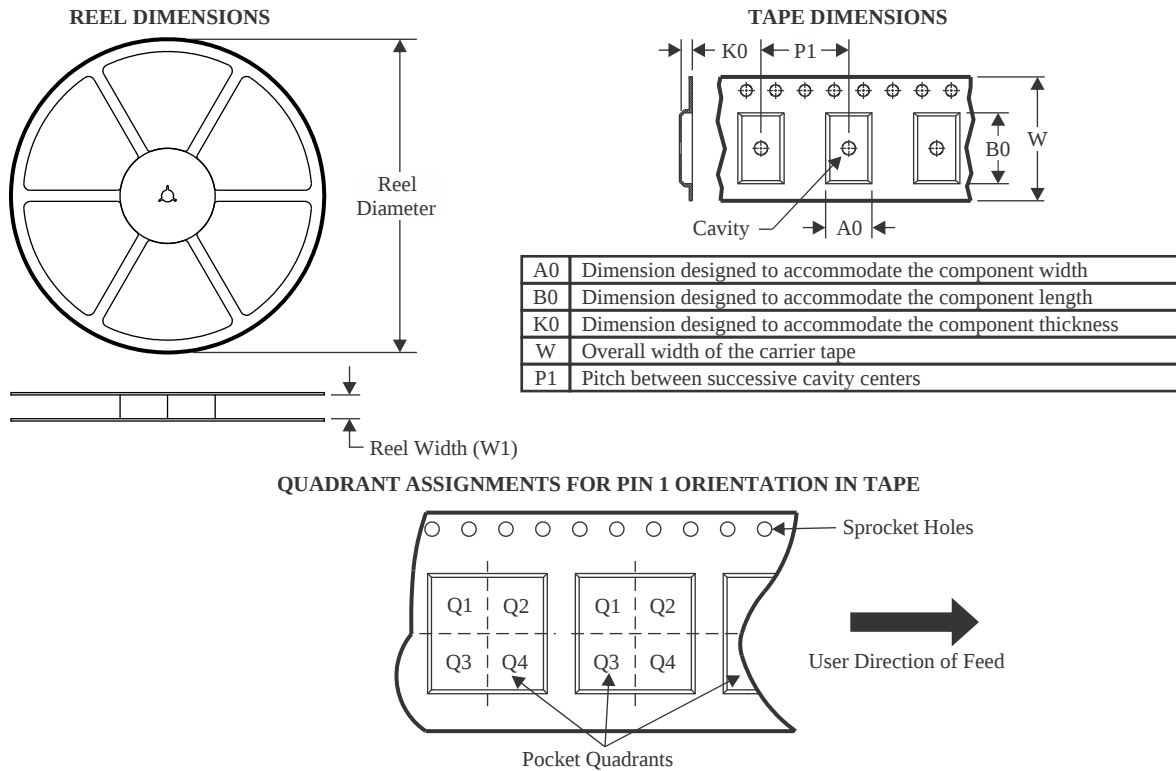
OTHER QUALIFIED VERSIONS OF TPS62810, TPS62811, TPS62812 :

- Automotive : [TPS62810-Q1](#), [TPS62811-Q1](#), [TPS62812-Q1](#)

- Enhanced Product : [TPS62810-EP](#), [TPS62811-EP](#), [TPS62812-EP](#)

NOTE: Qualified Version Definitions:

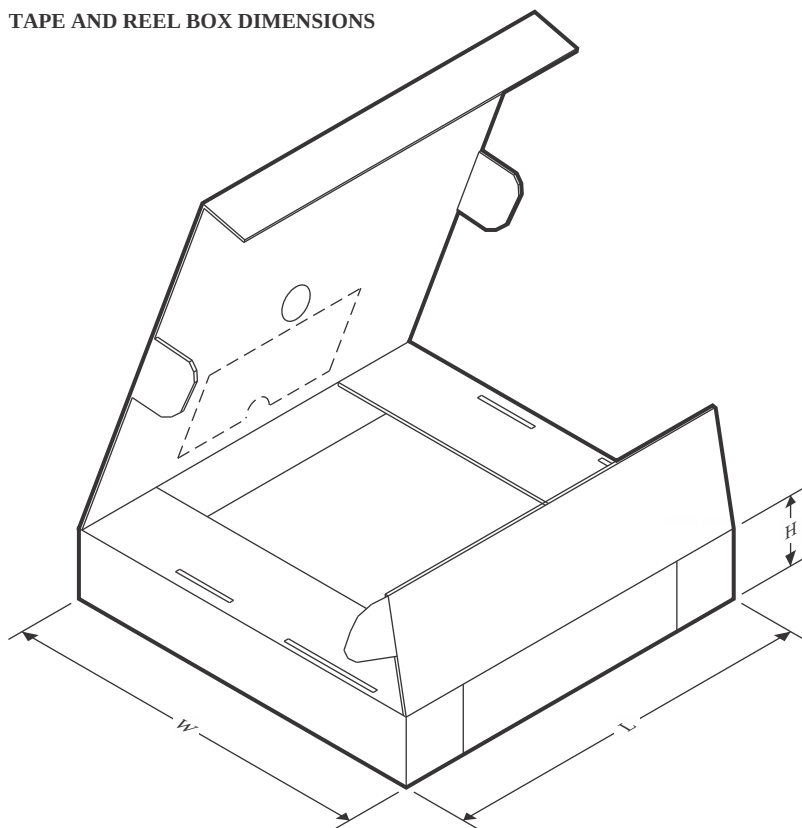
- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects
- Enhanced Product - Supports Defense, Aerospace and Medical Applications

TAPE AND REEL INFORMATION


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS62810RWYR	VQFN-HR	RWY	9	3000	180.0	8.4	2.25	3.25	1.05	4.0	8.0	Q1
TPS62811RWYR	VQFN-HR	RWY	9	3000	180.0	8.4	2.25	3.25	1.05	4.0	8.0	Q1
TPS62812RWYR	VQFN-HR	RWY	9	3000	180.0	8.4	2.25	3.25	1.05	4.0	8.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS62810RWYR	VQFN-HR	RWY	9	3000	210.0	185.0	35.0
TPS62811RWYR	VQFN-HR	RWY	9	3000	210.0	185.0	35.0
TPS62812RWYR	VQFN-HR	RWY	9	3000	210.0	185.0	35.0

GENERIC PACKAGE VIEW

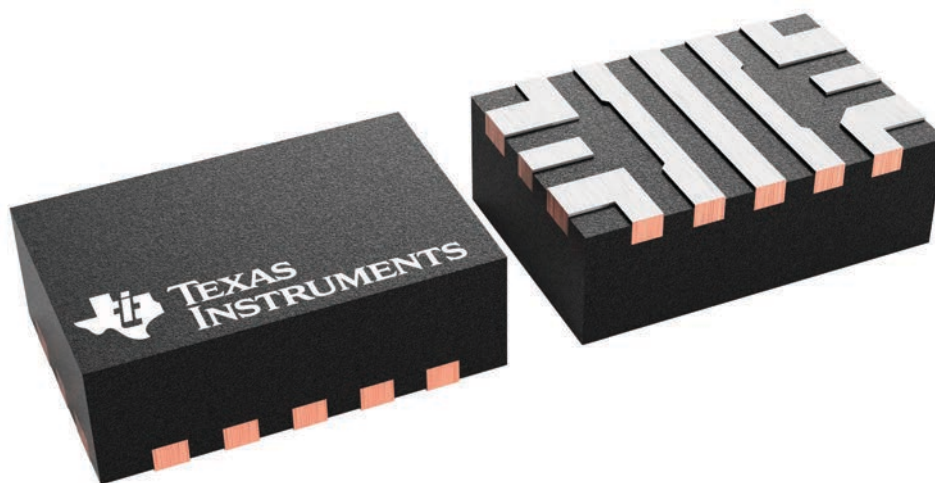
RWY 9

VQFN-HR - 1 mm max height

2 x 3, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



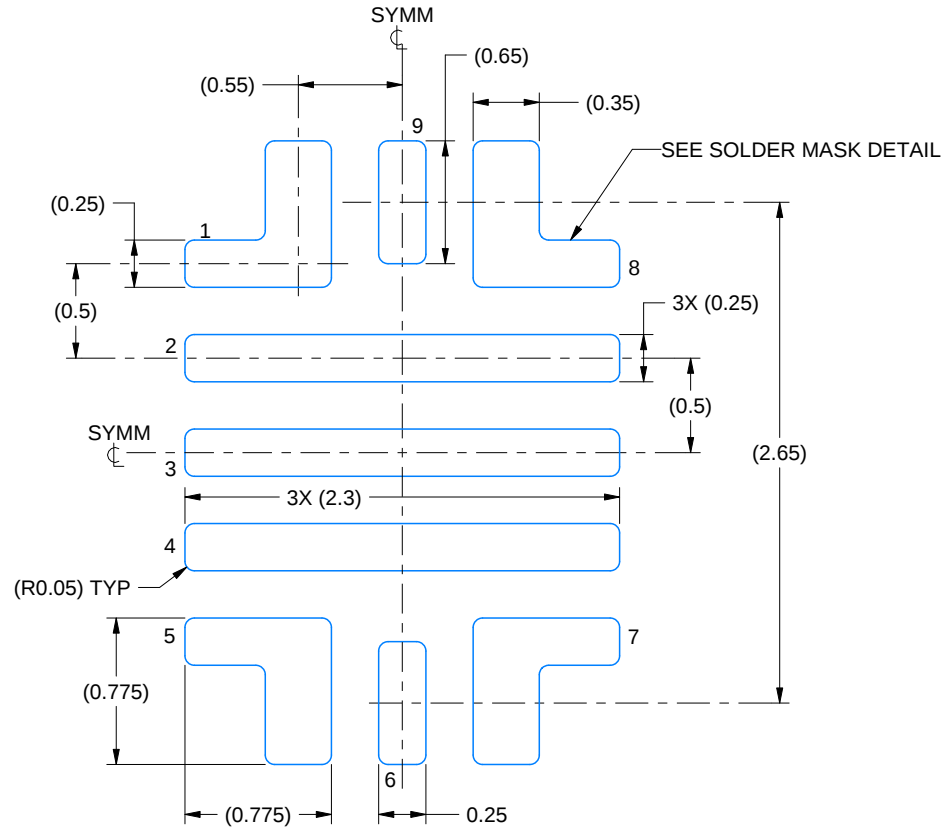
4226729/A

EXAMPLE BOARD LAYOUT

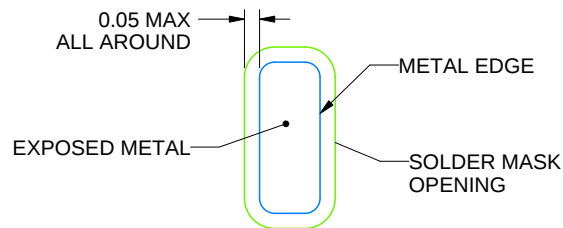
RWY0009B

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 25X



NON SOLDER MASK
DEFINED
SOLDER MASK DETAIL

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NOTES: (continued)

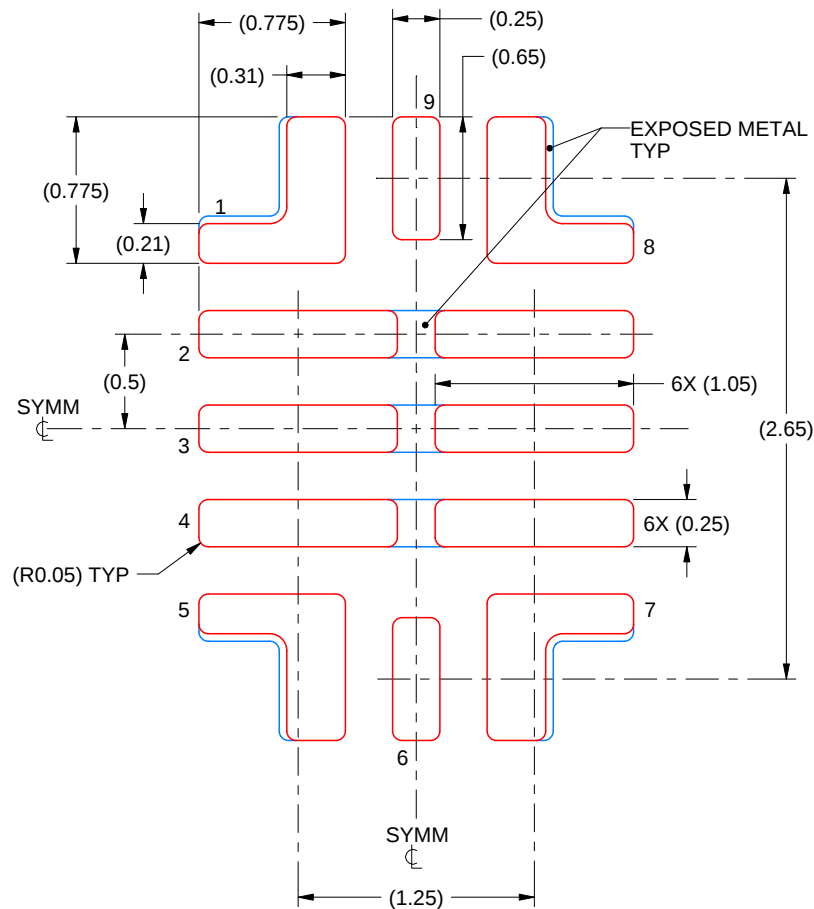
3. This package is designed to be soldered to thermal pads on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/sluea271).
4. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RWY0009B

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



SOLDER PASTE EXAMPLE
BASED ON 0.1 mm THICK STENCIL
PADS 1, 5, 7 & 8:
90% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE
SCALE: 25X

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NOTES: (continued)

5. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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