

# DRV7308 Three Phase 650V, 5A, GaN Intelligent Power Module

## 1 Features

- Three-phase PWM motor driver with integrated 650V enhancement mode GaN FETs
- Up to 450V operating voltage
  - 650V absolute maximum voltage
- High output current capability: 5A Peak current
- Low conduction loss: Low on-state resistance per GaN FET:  $205\text{m}\Omega$   $R_{DS(ON)}$  at  $T_A = 25^\circ\text{C}$
- Low switching loss: Zero reverse recovery, low output capacitance, slew rate control
- Low distortion: Ultra-low propagation delay < 135ns, Ultra-low adaptive dead time < 200ns
- Integrated gate drives with slew rate control of phase node voltage
  - Slew rate options from 5V/ns to 40V/ns
- Integrated fast bootstrap GaN rectifier
- Low-side GaN FET open source pins to support 1- or 2- or 3-shunt current sensing
- Supports up to 100kHz hard switching
- Integrates an amplifier for current sensing
- Supports 3.3V and 5V logic inputs, up to 20V
- BRAKE pin to turn on all low side GaN FETs
- Integrated temperature sensor
- >1.6mm clearance of motor phase (OUTx) to the adjacent pins.
- 2mm clearance between VM and GND
- Integrated protection features
  - GVDD and bootstrap under voltage lockout
  - Over current protection for low-side GaN FET
  - Over temperature protection
  - PWM adaptive dead time insertion
  - Current limit protection for all three phases
  - Fault condition indication pin (nFAULT)

## 2 Applications

- Refrigerator & freezer
- Appliances and HVAC pumps and fans

- Dishwasher
- Small home appliances
- Residential air conditioners
- Cooker hood
- Brushless-DC motor modules

## 3 Description

The DRV7308 is a three-phase intelligent power module (IPM) that consists of 205mΩ, 650V e-mode Gallium-Nitride (GaN) for driving three-phase BLDC/PMSM motors up to 450V DC rails. The applications include field-oriented control (FOC), sinusoidal current control, and trapezoidal (six step) current control of BLDC motors. The device helps to achieve more than 99% efficiency for a 3-phase modulated, FOC-driven, 250W motor drive application in a QFN 12mm x 12mm package at 20kHz switching frequency, eliminating the need for heat sink. The device helps to achieve ultra quiet operation, with very low dead time. The integrated bootstrap rectifier with bootstrap current limit eliminates the need for an external bootstrap diode.

### Note

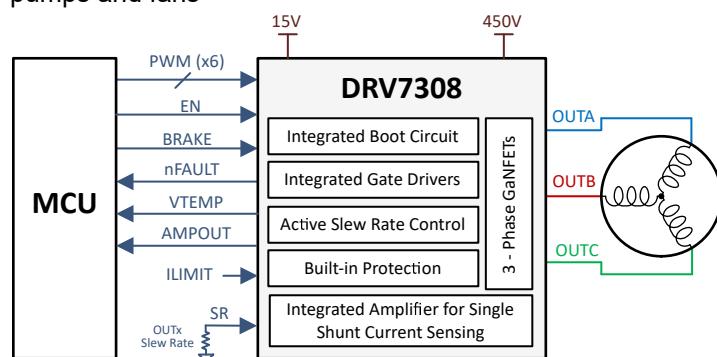
For safety, TI recommends the use of isolated test equipment with overvoltage and overcurrent protection. TI recommends using a safety enclosure when operating the device.

### Package Information

PART NUMBER	PACKAGE <sup>(1)</sup>	PACKAGE SIZE <sup>(2)</sup>
DRV7308	REN (VQFN, 65)	12.00mm x 12.00mm

(1) For more information, see the [Mechanical, Packaging, and Orderable Information](#).

(2) The package size (length x width) is a nominal value and includes pins, where applicable.



**Simplified Schematic**



An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. PRODUCTION DATA.

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## 4 Pin Configuration and Functions

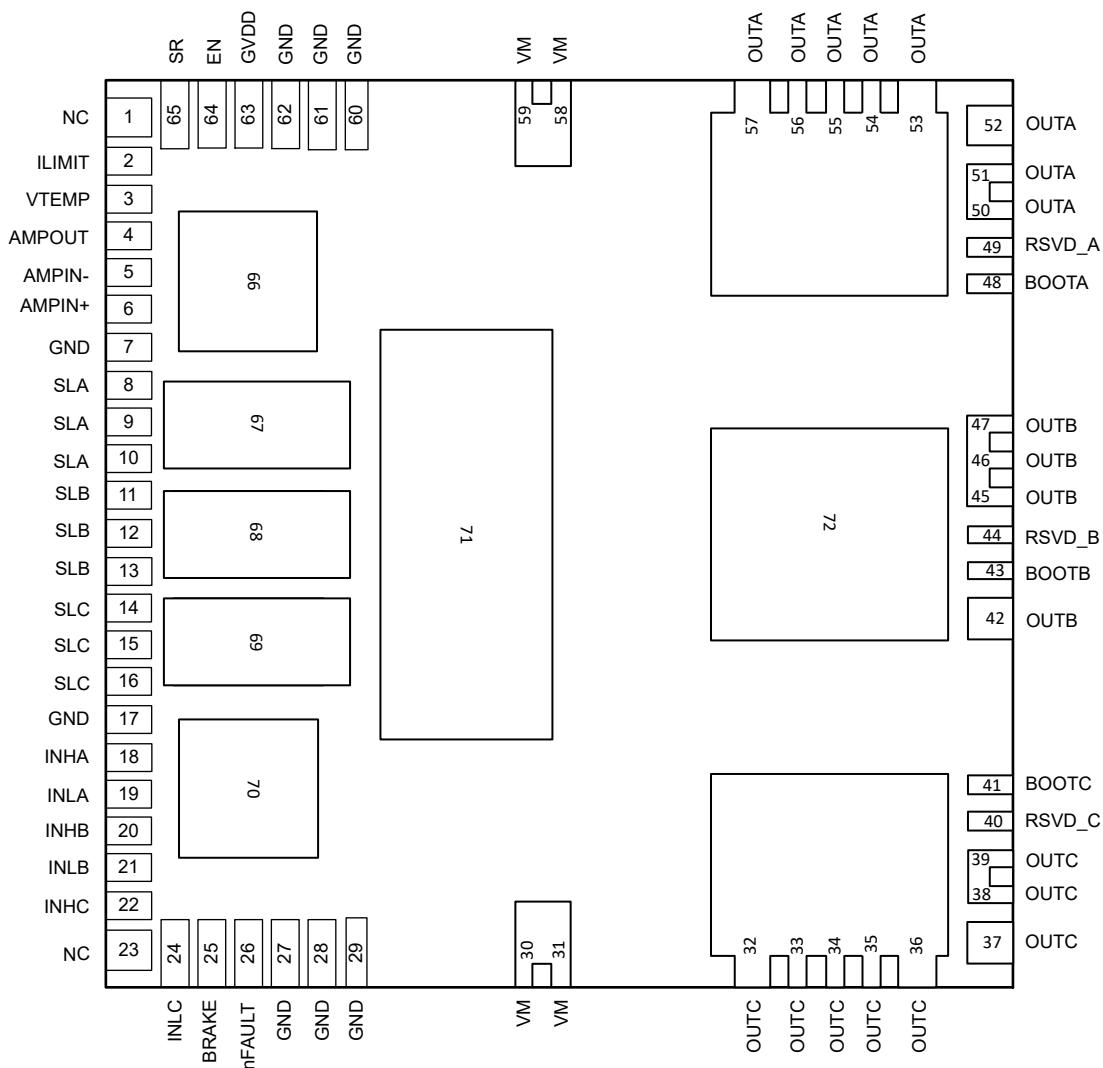


Figure 4-1. DRV7308 VQFN With Exposed Thermal Pad Top View

**Table 4-1. Pin Functions**

PIN		TYPE <sup>(1)</sup>	DESCRIPTION
NAME	NO.		
AMPIN-	5	I	Inverting input of the operational amplifier
AMPIN+	6	I	Non-inverting input of the operational amplifier
AMPOUT	4	O	Output terminal of the operational amplifier
BOOTA	48	P	Bootstrap supply for phase A; A GVDD rated capacitor must be placed between BOOTA and OUTA.
BOOTB	43	P	Bootstrap supply for phase B; A GVDD rated capacitor must be placed between BOOTB and OUTB.
BOOTC	41	P	Bootstrap supply for phase C; A GVDD rated capacitor must be placed between BOOTC and OUTC.
BRAKE	25	I	Motor Brake signal. Logic high on the pin turns on all the low side GaN FETs and turns off all the high side GaN FETs
EN	64	I	Driver enable pin. When this pin is logic low the device goes to shutdown mode and all the GaN FETs are turned off. A 20µs to 40µs low pulse can be used to reset fault conditions
nFAULT	26	O	Fault indication pin. Pulled logic-low on fault condition; Open-drain output requires an external pullup
ILIMIT	2	I	Reference voltage for internal overcurrent limit comparator
INHA	18	I	High-side driver control input for OUTA. This pin controls the output of the high-side GaN FET
INHB	20	I	High-side driver control input for OUTB. This pin controls the output of the high-side GaN FET
INHC	22	I	High-side driver control input for OUTC. This pin controls the output of the high-side GaN FET
INLA	19	I	Low-side driver control input for OUTA. This pin controls the output of the low-side GaN FET
INLB	21	I	Low-side driver control input for OUTB. This pin controls the output of the low-side GaN FET
INLC	24	I	Low-side driver control input for OUTC. This pin controls the output of the low-side GaN FET
NC	1, 23		No connect, can be connected to GND
RSVD_A	49	I	Reserved pin. Connect the pin to OUTA
RSVD_B	44	I	Reserved pin. Connect the pin to OUTB
RSVD_C	40	I	Reserved pin. Connect the pin to OUTC
OUTA	50-57	P	Half bridge output A
OUTB	42, 45-47, 72	P	Half bridge output B
OUTC	32-39	P	Half bridge output C
GND	7, 17, 27,28,29, 60,61,62,66, 70, 71	G	Device power and signal ground. Connect to system ground
SLA	8, 9, 10, 67	P	Phase A half bridge low side source
SLB	11, 12, 13, 68	P	Phase B half bridge low side source
SLC	14, 15, 16, 69	P	Phase C half bridge low side source
SR	65	I	OUTx voltage slew rate control. Connect a resistor between SR pin and GND or SR pin to GVDD to configure the slew rate
GVDD	63	P	Low voltage power supply. bypass to GND with one 1µF, GVDD rated ceramic capacitor plus one bulk capacitor rated for GVDD
VM	30, 31, 58, 59	P	Power supply. Connect to motor supply voltage; bypass to GND with a 0.1µF capacitor plus one bulk capacitor rated for VM. The pins 30 and 31 are internally connected to the pins 58 and 59.

**Table 4-1. Pin Functions (continued)**

PIN		TYPE <sup>(1)</sup>	DESCRIPTION
NAME	NO.		
VTEMP	3	O	Temperature Sensor Output

(1) I = Input, O = Output, I/O = Input or Output, G = Ground, P = Power.

## 5 Absolute Maximum Ratings

over operating temperature range (unless otherwise noted)<sup>(2)</sup>

	MIN	MAX	UNIT
Drain-source blocking voltage (FET off) ( $V_{DS}$ )		650 <sup>(1)</sup>	V
DC voltage applied between VM and GND		450	V
Drain DC current ( $I_{DC}$ ) @ $T_J = 150^\circ\text{C}$		4	A
Phase node pin voltage referred to GND (FETs OFF) (OUTA, OUTB, OUTC), SL = GND	$-V_{SD}$	650	V
BOOTx pin voltage referred to OUTx (BOOTA, BOOTB, BOOTC)	-0.5	20	V
Pin voltage - GVDD to GND	-0.5	20	V
Pin voltage - INx, EN, BRAKE, nFAULT to GND	-0.5	20	V
Pin voltage - SLx to GND (DC)	-2.5	+2.5	V
Pin voltage - AMPIN+, AMPIN-, AMPOUT, ILIMIT, SR to GND	-0.5	$V_{GVDD}+0.3$	V
Operational amplifier output current (AMPOUT)		20	mA
Operating ambient temperature	-40	125	$^\circ\text{C}$
Operating junction temperature ( $T_J$ )	-40	150	$^\circ\text{C}$
Storage temperature ( $T_{stg}$ )	-55	150	$^\circ\text{C}$

(1) Product lifetime depends on  $V_{DS}$  voltage.

(2) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

## 6 ESD Ratings

		VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	$\pm 2000$
		Charged device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	$\pm 500$

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

## 7 Recommended Operating Conditions

over operating temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT
$V_{VM}$	DC power supply voltage	VM	0		450	V
$V_{GVDD}$	Gate driver supply voltage	GVDD		10.8	18	V
$f_{PWM}$	PWM frequency	OUTA, OUTB, OUTC		20	100	kHz
$V_{IN}$	Logic Input Voltage	INHx, INLx, EN, BRAKE	-0.1		20	V
$V_{OD}$	Open drain pull up voltage	nFAULT	-0.1		20	V
$I_{OD}$	Open drain output sink current	nFAULT	0		5	mA

over operating temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT
$V_{SR}$	Slew rate pin voltage	SR			$V_{GVDD}$	V
$V_{SLx}$	SLx pin voltage	SLA, SLB, SLC	-1	1	V	
$V_{AMPINx}$	Amplifier input pin voltage	AMPIN+, AMPIN-	-0.1	5	V	
$V_{ILIMIT}$	Over current protection reference	ILIMIT	0.2	2	V	
$T_{PWIN\_ON}$	Minimum input pulse width	INH, INL <sup>(1)</sup>	0.5		$\mu s$	
$T_A$			-40	100	$^{\circ}C$	
$T_J$			-40	125	$^{\circ}C$	

(1) The device may not make response to the input if input pulse width is less than the recommended value.

## 8 Thermal Information

THERMAL METRIC <sup>(1)</sup>		DEVICE	UNIT
		REN (VQFN)	
		40 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	21.2	$^{\circ}C/W$
$R_{\theta JC(\text{top})}$	Junction-to-case (top) thermal resistance	5.5	$^{\circ}C/W$
$R_{\theta JB}$	Junction-to-board thermal resistance	6.0	$^{\circ}C/W$
$\Psi_{JT}$	Junction-to-top characterization parameter	4.0	$^{\circ}C/W$
$\Psi_{JB}$	Junction-to-board characterization parameter	5.8	$^{\circ}C/W$
$R_{\theta JC(\text{bot})}$	Junction-to-case (bottom) thermal resistance per GaNFET	1	$^{\circ}C/W$

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics application report](#).

## 9 Electrical Characteristics

$T_J = -40^{\circ}C$  to  $150^{\circ}C$ ,  $V_{GVDD} = 15V$ , EN = High (unless otherwise noted). Typical limits apply for  $T_A = 25^{\circ}C$ ,  $V_{GVDD} = 15V$

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>GaN POWER TRANSISTOR</b>					
$R_{DS(ON)}$	$V_{GVDD} = 15V$ , $I_{OUTx} = 1A$ , $T_J = 25^{\circ}C$ ,	205	320		$m\Omega$
$R_{DS(ON)}$	$V_{GVDD} = 15V$ , $I_{OUTx} = 1A$ , $T_J = 150^{\circ}C$ ,	370			$m\Omega$
$V_{SD}$	$INx = 0V$ , $ISD = 0.1A$ , $T_J = 25^{\circ}C$	1.5	2.5		V
$V_{SD}$	$INx = 0V$ , $ISD = 4A$ , $T_J = 25^{\circ}C$	2.8			V
$Q_{RR}$	$V_R = 300 V$ , $I_{SD} = 4 A$ , $dI_{SD}/dt = 0.2 A/ns$	0			$nC$
<b>SWITCHING CHARACTERISTICS</b>					
SR	Phase pin slew rate switching low to high (Rising from 20 % to 80 %)	$V_{VM} = 300V$ , SR setting = 0	4		$V/ns$
SR	Phase pin slew rate switching high to low (Falling from 80 % to 20 %)	$V_{VM} = 300V$ , SR setting = 0	4		$V/ns$
SR	Phase pin slew rate switching low to high (Rising from 20 % to 80 %)	$V_{VM} = 300V$ , SR setting = 1	10		$V/ns$
SR	Phase pin slew rate switching high to low (Falling from 80 % to 20 %)	$V_{VM} = 300V$ , SR setting = 1	10		$V/ns$
SR	Phase pin slew rate switching low to high (Rising from 20 % to 80 %)	$V_{VM} = 300V$ , SR setting = 2	20		$V/ns$
SR	Phase pin slew rate switching high to low (Falling from 80 % to 20 %)	$V_{VM} = 300V$ , SR setting = 2	20		$V/ns$

$T_J = -40^\circ\text{C}$  to  $150^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$ , EN = High (unless otherwise noted). Typical limits apply for  $T_A = 25^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SR	Phase pin slew rate switching low to high (Rising from 20 % to 80 %)	$V_{\text{VM}} = 300\text{V}$ , SR setting = 3		40		$\text{V/ns}$
SR	Phase pin slew rate switching high to low (Falling from 80 % to 20 %)	$V_{\text{VM}} = 300\text{V}$ , SR setting = 3		40		$\text{V/ns}$
$t_{\text{pd, on}}$	Propagation delay, turn on	$V_{\text{INHx}}, V_{\text{INLx}} = \text{logic low to high}$ , $V_{\text{VM}} = 300\text{V}$ , $I_D = 4\text{A}$ , SR = 0		125		$\text{ns}$
$t_{\text{delay, on}}$	Turn on delay time	$V_{\text{INHx}}, V_{\text{INLx}} = \text{logic low to high}$ , $V_{\text{VM}} = 300\text{V}$ , $I_D = 4\text{A}$ , SR = 0		75		$\text{ns}$
$t_{\text{pd, off}}$	Propagation delay, turn off	$V_{\text{INHx}}, V_{\text{INLx}} = \text{logic high to low}$ , $V_{\text{VM}} = 300\text{V}$ , $I_D = 4\text{A}$ , SR = 0		135		$\text{ns}$
$t_{\text{delay, off}}$	Turn off delay time	$V_{\text{INHx}}, V_{\text{INLx}} = \text{logic high to low}$ , $V_{\text{VM}} = 300\text{V}$ , $I_D = 4\text{A}$ , SR = 0		75		$\text{ns}$
$t_{\text{DEAD}}$	Output dead time (high to low)	$V_{\text{VM}} = 300\text{V}$ , $I_{\text{OUTx}} = 4\text{A}$ , Current going out of phase node (OUTx) SR = 0, 1		40		$\text{ns}$
$t_{\text{DEAD}}$	Output dead time (high to low)	$V_{\text{VM}} = 300\text{V}$ , $I_{\text{OUTx}} = 4\text{A}$ , Current going into phase node (OUTx), SR = 0		100		$\text{ns}$
$t_{\text{DEAD}}$	Output dead time (high to low)	$V_{\text{VM}} = 300\text{V}$ , $I_{\text{OUTx}} = 4\text{A}$ , Current going into phase node (OUTx), SR = 1 or 2 or 3		100		$\text{ns}$
$t_{\text{DEAD}}$	Output dead time (low to high)	$V_{\text{VM}} = 300\text{V}$ , $I_{\text{OUTx}} = 4\text{A}$ , Current going into phase node (OUTx)		40		$\text{ns}$
$t_{\text{start}}$	Start up time	$V_{\text{GVDD}} > V_{\text{GVDD\_UV\_ON}}$ , EN = low to high, INLx = 1, low side GaNFET turns ON		2		$\text{ms}$
$t_{\text{off}}$	Device turn off time - to sleep	$V_{\text{GVDD}} > V_{\text{GVDD\_UV\_ON}}$ , EN = high to low	40	80		$\text{us}$
$t_{\text{clr\_fit}}$	Time to clear any latched fault using EN	EN = low pulse width	15	40		$\text{us}$
$t_{\text{off}}$	Device turn off time- gate driver off	$V_{\text{GVDD}} > V_{\text{GVDD\_UV\_ON}}$ , EN = high to low, INLx = 1, low side GaNFET turns OFF		80		$\mu\text{s}$

#### GVDD POWER SUPPLY

$I_{\text{GVDD,Q}}$	GVDD operating current, driver enabled, no switching	EN = High, $V_{\text{VM}} = 300\text{V}$ , INx = 0	2.3	mA
$I_{\text{GVDD,3SW}}$	GVDD average operating current, driver enabled, GaN switching, No load at OUTx pins	EN = High, $F_{\text{sw}} = 20\text{kHz}$ , 3-half bridge switching at 50% complimentary PWM, $V_{\text{VM}} = 300\text{V}$ , $V_{\text{GVDD}} = 15\text{V}$ , SR = 0	3.7	mA
$V_{\text{GVDD\_UV\_R}}$	GVDD undervoltage threshold - rising	GVDD rising	10	V
$V_{\text{GVDD\_UV\_F}}$	GVDD undervoltage threshold - falling	GVDD falling	9	V
$V_{\text{GVDD\_UV\_HYS}}$	GVDD undervoltage detection hysteresis	GVDD rising to falling threshold	500	$\text{mV}$
$t_{\text{UVLO\_GVDD}}$	GVDD undervoltage deglitch time		20	$\mu\text{s}$

#### BOOTSTRAP POWER SUPPLY

$R_{\text{DS\_BST}}$	Bootstrap rectifier on resistance	$V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$	30	$\Omega$	
$I_{\text{LMT\_BST}}$	Bootstrap rectifier current limit	EN = High, $V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$ , INLx = High, INHx = Low, $V_{\text{BOOTx}} - V_{\text{OUTx}} = 12\text{V}$	150	250	mA
$I_{\text{BST\_PK}}$	Bootstrap rectifier peak transient current	EN = High, $V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$ , INLx = High, INHx = Low, $V_{\text{BOOTx}} - V_{\text{OUTx}} = 0\text{ V}$	350		mA
$I_{\text{BST\_Q}}$	Bootstrap quiescent current	EN = High, INHx = Low, INLx = Low, $V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{BOOTx}} - V_{\text{OUTx}} = 12\text{V}$	100	145	$\mu\text{A}$
$I_{\text{BST\_Q}}$	Bootstrap quiescent current	EN = High, INHx = High, INLx = Low, $V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{BOOTx}} - V_{\text{OUTx}} = 12\text{V}$	350		$\mu\text{A}$

$T_J = -40^\circ\text{C}$  to  $150^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$ , EN = High (unless otherwise noted). Typical limits apply for  $T_A = 25^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$V_{\text{BST\_UV}}$	Bootstrap supply undervoltage	BOOTx rising			9	V
$V_{\text{BST\_UV}}$	Bootstrap supply undervoltage	BOOTx falling		8		V
$V_{\text{BST\_UV\_HYS}}$	Bootstrap supply undervoltage hysteresis			500		mV
$t_{\text{BST\_UV}}$	Bootstrap supply undervoltage deglitch time				20	$\mu\text{s}$

#### LOGIC-LEVEL INPUTS (EN, INHx, INLx, BRAKE)

$V_{\text{IL}}$	Input logic low voltage	INHx, INLx, BRAKE, EN		0.8		V
$V_{\text{IH}}$	Input logic high voltage	INHx, INLx, BRAKE, EN	2.2			V
$V_{\text{HYS}}$	Input logic hysteresis	INHx, INLx, BRAKE, EN	300	450	650	mV
$I_{\text{IL}}$	Input logic low current (INHx, INLx, BRAKE, EN)	$V_I = 0\text{ V}$	-1		1	$\mu\text{A}$
$I_{\text{IL}}$	Input logic low current (BRAKE, EN)	$V_I = 0\text{ V}$	-1		1	$\mu\text{A}$
$R_{\text{PD}}$	Input pulldown resistance	INHx, INLx, EN	70	100	130	$\text{k}\Omega$
$R_{\text{PD}}$	Input pulldown resistance	BRAKE	15	20	25	$\text{k}\Omega$
$t_{\text{deg}}$	Input logic deglitch time	INHx, INLx	25		50	ns
$t_{\text{deg}}$	Input logic deglitch time	EN		80		$\mu\text{s}$
$t_{\text{deg}}$	Input logic deglitch time	BRAKE	1200		2000	ns

#### MULTI-LEVEL INPUT (SR)

$R_{\text{L1}}$	SR setting = 0	Tied to GND	0	1	$\text{k}\Omega$
$R_{\text{L2}}$	SR setting = 1	Tied to $V_{\text{GVDD}}$	0	1	$\text{k}\Omega$
$R_{\text{L3}}$	SR setting = 2	R tied to GND ( $R = 5\text{ k}\Omega$ to $15\text{ k}\Omega$ )	5	15	$\text{k}\Omega$
$R_{\text{L4}}$	SR setting = 3	R tied to GND ( $R = 40\text{ k}\Omega$ to $100\text{ k}\Omega$ )	40	100	$\text{k}\Omega$

#### OPEN-DRAIN OUTPUTS (nFAULT)

$V_{\text{OL}}$	Output logic low voltage	$I_{\text{OD}} = 5\text{ mA}$		0.4		V
$I_{\text{OH}}$	Output logic high current	$V_{\text{OD}} = 5\text{ V}$	-1	1		$\mu\text{A}$
$C_{\text{OD}}$	Output capacitance			30		pF

#### GaN PREDRIVER PROTECTION

$I_{\text{OCP\_GaN}}$	Low-side GaN FET overcurrent detection threshold	$V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$ , $T_J = 25^\circ\text{C}$	7.5	24		A
$I_{\text{OCP\_GaN}}$	Low-side GaN FET overcurrent detection threshold	$V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$ , $T_J = 125^\circ\text{C}$	5			A
$t_{\text{OCP\_GaN\_BT}}$	Blanking time (including deglitch)	$V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$		150		ns
$t_{\text{OCP\_GaN\_PD}}$	Propagation delay (to FET turn off)	$V_{\text{GVDD}} = 15\text{V}$ , $V_{\text{VM}} = 300\text{V}$		50		ns
$T_{\text{SD\_RISE}}$	Thermal shutdown rising	Die temperature ( $T_J$ )	145	165	185	$^\circ\text{C}$
$T_{\text{SD\_FALL}}$	Thermal shutdown falling	Die temperature ( $T_J$ )	125	145	165	$^\circ\text{C}$
$T_{\text{SD\_HYST}}$	Thermal shutdown hysteresis	Die temperature ( $T_J$ )	13	20		$^\circ\text{C}$

#### CURRENT LIMIT COMPARATOR (ILIMIT)

$I_b$	Input bias current (ILIMIT)	$V_{\text{ILIMIT}} = 0.5\text{V}$		1		$\mu\text{A}$
$V_{\text{off}}$	ILIMIT comparator input voltage offset	$V_{\text{ILIMIT}} = 1.0\text{V}$		$\pm 2.5$		mV
$V_{\text{ILIMIT\_DIS}}$	Minimum ILIMIT voltage to disable ILIMIT OCP		2.2	2.6		V
$V_{\text{ILIMIT}}$	Operational voltage range at ILIMIT			2		V
$t_{\text{blank}}$	Over current detection blanking on all SLx inputs, from any INHx/INLx turn on/off		400	620		ns
$t_{\text{deglitch}}$	Over current detection de-glitch time		190	330		ns

$T_J = -40^\circ\text{C}$  to  $150^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$ , EN = High (unless otherwise noted). Typical limits apply for  $T_A = 25^\circ\text{C}$ ,  $V_{\text{GVDD}} = 15\text{V}$

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{\text{filter}}$	ILIMIT comparator input RC filter time (SLx)	$V_{\text{SLx}} = 0$ to $1\text{V}$ step, $V_{\text{ILIMIT}} = 0.63\text{V}$	250	450		ns
$t_{\text{filter}}$	ILIMIT reference voltage input RC filter time (ILIMIT)	$V_{\text{ILIMIT}} = 1$ to $0\text{V}$ step, $V_{\text{SLx}} = 0.37\text{V}$	600	1000		ns
$t_{\text{pd\_OFF}}$	Propagation delay time from ILIMIT over current detection to all GaN FETs turn off	$V_{\text{ILIMIT}} = 0.63\text{V}$ , $V_{\text{SLx}} = 0$ to $1\text{V}$ step, $\text{INx} = \text{constant}$			1.2	$\mu\text{s}$
$t_{\text{pd\_FAULT}}$	Propagation delay time from ILIMIT over current detection to nFAULT pin report	$V_{\text{ILIMIT}} = 0.63\text{V}$ , $V_{\text{SLx}} = 0$ to $1\text{V}$ step, $\text{INx} = \text{constant}$			1	$\mu\text{s}$

**OPERATIONAL AMPLIFIER**

$V_{\text{LINEAR}}$	Output voltage swing	$R_L = 10\text{k}$ to GND	0.02	4.9	V
GBW	Gain bandwidth product	$\text{RL} = 10\text{k}$ , $\text{G} = +1$		11	MHz
$V_{\text{SR\_opamp}}$	Output voltage slew rate	$\text{RL} = 10\text{k}$ , $\text{G} = +1$		26	$\text{V}/\mu\text{s}$
$t_{\text{set}}$	Settling time to $\pm 1\%$	2-V step, $\text{G} = +1$ , $\text{CL} = 130\text{ pF}$ , $\text{RL} = 10\text{k}$		0.4	$\mu\text{s}$
$A_{\text{OL}}$	Open-loop voltage gain	$0.04\text{ V} < \text{VAMPOUT} < 4.8\text{ V}$ , $\text{RL} = 10\text{ k}\Omega$ to GND		106	dB
$\varphi_m$	Phase margin	$\text{G} = +1$ , $\text{RL} = 10\text{k}$		60	°
$V_{\text{COM}}$	Common mode input range		0	5	V
$V_{\text{OFF}}$	Input offset voltage error	$\text{TA} = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 1$	mV
$V_{\text{DRIIFT}}$	Drift offset	$\text{TA} = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 2$	$\mu\text{V}/^\circ\text{C}$
$I_{\text{bias}}$	Input bias current	$V_{\text{AMPIN-}} = V_{\text{AMPIN+}} = 2.5\text{V}$		$\pm 100$	nA
$I_{\text{bias\_off}}$	Input bias offset current	$V_{\text{AMPIN-}} = V_{\text{AMPIN+}} = 2.5\text{V}$		$\pm 10$	nA
CMRR	Common mode rejection ratio	$-0.1\text{ V} < V_{\text{CM}} < 5\text{ V}$ , $\text{TA} = -40^\circ\text{C}$ to $125^\circ\text{C}$		96	dB
$I_{\text{SC\_opamp}}$	Short-circuit current			$\pm 20$	mA
$Z_o$	Open-loop output impedance	$f = 5\text{ MHz}$		250	$\Omega$
$C_L$	Capacitive load drive			130	pF

**TEMPERATURE SENSOR**

$V_T$	Temperature sense element output (VTEMP) voltage	$\text{TA} = 25^\circ\text{C}$	1.98		V
$R_T$	Minimum load resistance on VTEMP pin	test condition of $V_T$	90		$\text{k}\Omega$
$C_T$	Maximum load capacitance at VTEMP pin	test condition of $V_T$		130	pF

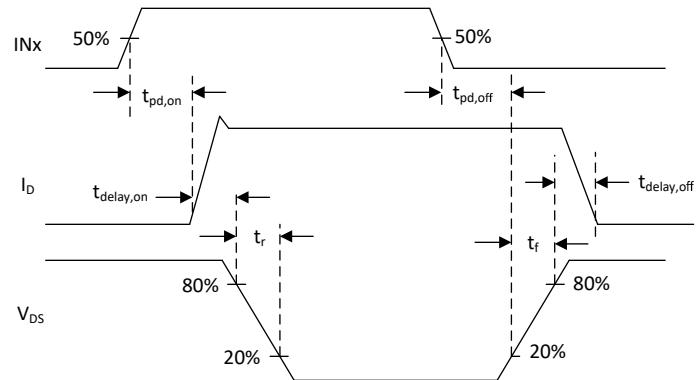


Figure 10-1. DRV7308 Turn On and Turn Off Switching Characteristics

## 11 Typical Characteristics

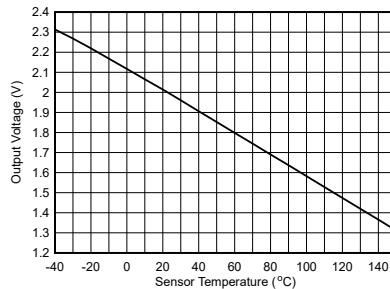


Figure 11-1. Temperature Sensor Output Across Sensor Temperature

## 12 Detailed Description

### 12.1 Overview

The DRV7308 is a three-phase IPM, with three integrated half-H-bridge 205mΩ, 650V e-mode Gallium-Nitride (GaN) for driving three-phase BLDC/PMSM motors up to 450V DC rails. The device applications include field-oriented control (FOC), sinusoidal current control, and trapezoidal current control of BLDC motors. The device integrates pre-drivers for all GaN FETs with slew rate control of phase node voltages. The low  $R_{DS\_ON}$ , slew rate control, zero reverse recovery, and low output capacitance help achieve more than 99% efficiency for a 3-phase modulated, FOC driven, 250W motor drive application, eliminating the need for heat sink.

The device integrates a suite of protections including overcurrent limit, overtemperature protection, overcurrent protection for low-side GaN FETs, undervoltage protection for the GVDD and bootstrap power supplies, and adaptive dead time insertion to avoid shoot through conditions.

The device integrates a bootstrap rectifier with an integrated GaN FET and a transient current limit, which eliminates the need for an external boot diode. The DRV7308 brings out all three low-side source pins of the GaN FETs to support 3-, 2-, or 1-shunt current sensing. The device integrates an 11MHz, 15V/μs operational amplifier for single shunt current sensing in FOC and trapezoidal control of BLDC motors.

The low dead time helps achieve ultra quiet operations in BLDC/PMSM motors. The low propagation delay helps achieve lower distortion and accurate average current sensing.

The DRV7308 is available in a VQFN 12mm x 12mm package.

## 12.2 Functional Block Diagram

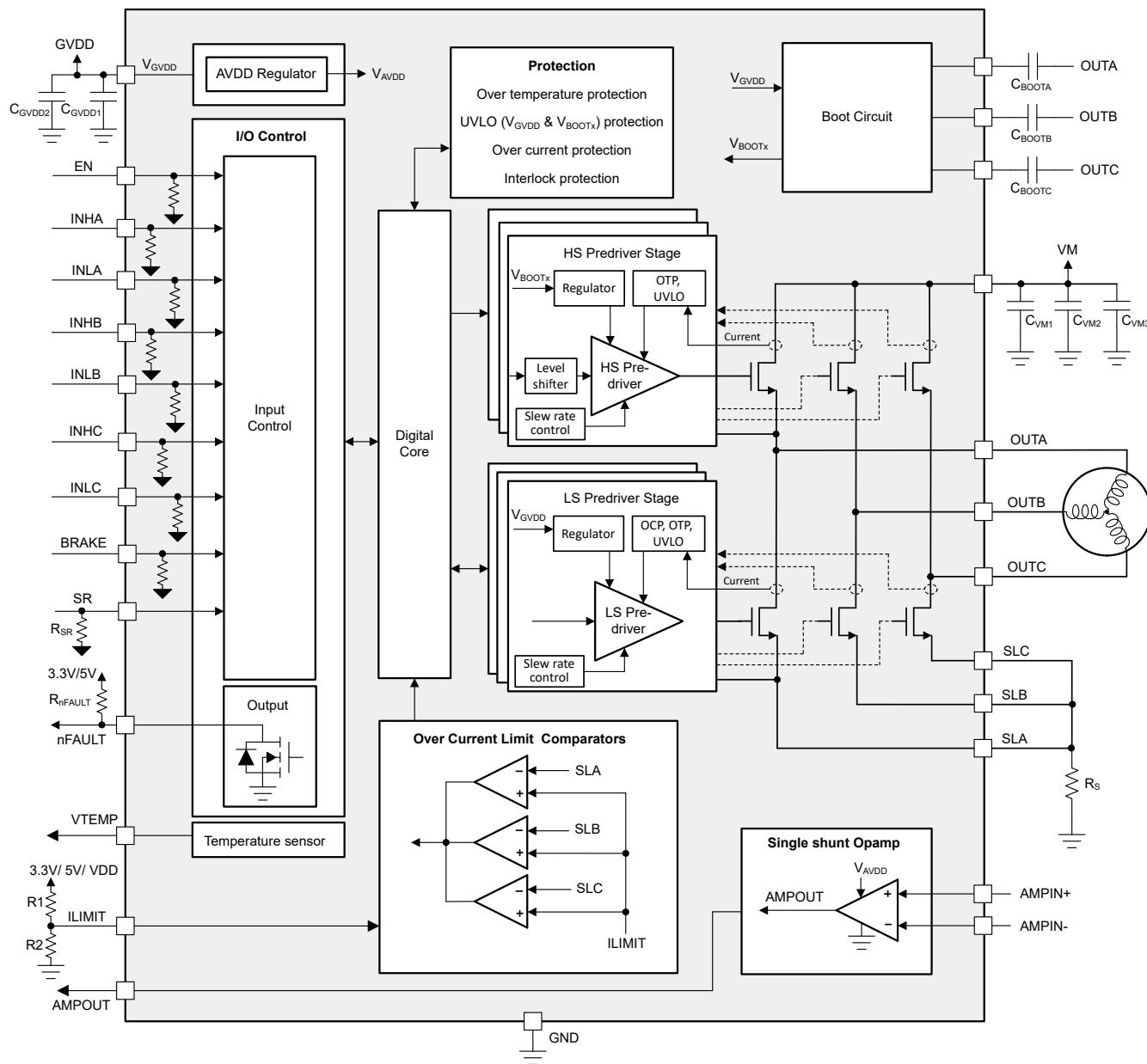


Figure 12-1. DRV7308 Block Diagram

## 12.3 Feature Description

### 12.3.1 Output Stage

The DRV7308 device consists of integrated  $205\text{m}\Omega$  (one GaN FET on-state resistance) enhancement mode GaN (EGaN) FETs connected in a three-phase bridge configuration. The device integrates a pre-driver for low-side and high-side GaN FETs using an integrated bootstrap controller and rectifier using a low voltage external power supply at  $\text{GVDD}$ . An appropriately used external bootstrap capacitor offers 100% duty cycle support for a defined time.

### 12.3.2 Input Control Logic

The DRV7308 controls the state of the GaN FET based on the PWM input signals at the INHx and INLx pins. The device uses the BRAKE signal to apply brake to motor drive. A logic high at the BRAKE signal overrides the INHx and INLx pins and turns on all low side GaN transistors. The device enters shutdown mode (all the gate drivers and GaN FETs in off state) and ignores the status of the INHx, INLx, and BRAKE pins when a logic low on the EN pin occurs. A 20-40 $\mu$ s logic low pulse at the EN pin resets the device from OCP and OTP faults. The truth table for the input control logic is shown in [Table 12-1](#).

**Table 12-1. Input Control Logic**

EN	BRAKE	INHx	INLx	HIGH SIDE GAN FET	LOW SIDE GAN FET	DESCRIPTION
0	X	X	X	OFF	OFF	Device in shutdown and all outputs in Hi-Z
1	1	X	X	OFF	ON	BRAKE. All low side GaN FETs are ON and all high-side GaN FETs are OFF
1	0	1	1	OFF	OFF	OUTx in Hi-Z
1	0	0	0	OFF	OFF	OUTx in Hi-Z
1	0	1	0	ON	OFF	OUTx connected to VM
1	0	0	1	OFF	ON	OUTx connected to SLx node

### 12.3.3 ENABLE (EN) Pin Function

When the EN pin is low, the device goes to a low-power sleep mode. In sleep mode, all GaNFETs are turned off—the Gan pre-drivers, integrated op amp, temperature sensor, GaN OCP, digital core LDO, and oscillators are all turned off. The  $t_{off}$  time must elapse after a falling edge on the EN pin before the device goes to sleep mode. The device comes out of sleep mode automatically if the EN pin is pulled high. The  $t_{start}$  time must elapse before the device is ready for inputs.

**Note**

During power up and power down of the device through the EN pin, the nFAULT pin is held low as the internal regulators are enabled or disabled. After the regulators have enabled or disabled, the nFAULT pin is automatically released.

### 12.3.4 Temperature Sensor Output (VTEMP)

DRV7308 incorporates a temperature sensor that senses the device temperature. The output of the temperature sensor is an analog voltage that varies across temperature.

### 12.3.5 Brake Function

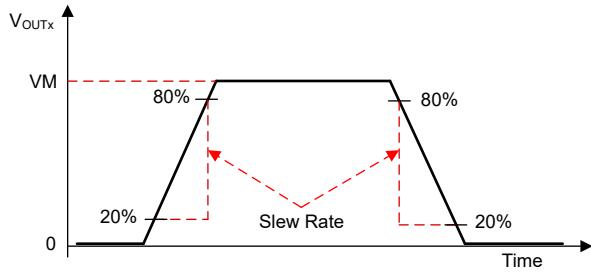
The BRAKE pin provides a means to turn on all the low-side GaNFETs, independent of INHx and INLx pin status. The brake pin has an internal pull down. Connect the BRAKE pin to GND externally if not used. A logic high on the BRAKE pin places the device into brake by turning on all the low-side GaNFETs.

**Note**

Use caution while applying the BRAKE high command, as this can cause very high current driven by the motor back EMF. During BRAKE operation, the maximum current through the GaNFET must be a value that is within the operating limits of the GaNFET current and junction temperature.

### 12.3.6 Slew Rate Control (SR)

The DRV7308 can optionally control the slew rate of the voltage rise and fall at the OUTx pins through the configuration of the SR pin. The user can set slew rates of 5V/ns, 10V/ns, 20V/ns, or 40V/ns by configuring the SR pin. The slew rate is controlled by adjusting the gate current of GaNFETs.



**Figure 12-2. DRV7308 Slew Rate Control**

**Note**

At higher slew rates of 20V/ns and 40V/ns, TI recommends adding a capacitor across the shunt resistors that have an RC time constant of 50ns.

### 12.3.7 Dead Time

The device is fully protected for any cross conduction of GaNFETs. In half-bridge configuration, the operation of the high-side and low-side GaNFETs are controlled to avoid any shoot-through currents by inserting dead time ( $t_{DEAD}$ ). This process is implemented by using an adaptive dead time circuit that senses the gate-source voltage (VGS) of the low-side GaNFET and the phase node (OUTx) voltage of the same half-bridge.

### 12.3.8 Current Limit Functionality (ILIMIT)

The DRV7308 incorporates a current limit functionality that monitors SLx voltages. DRV7308 has three integrated comparators, each monitoring voltage at SLA, SLB, and SLC pins separately. The reference voltage of all three comparators is fed externally using the ILIMIT pin. A voltage less than 2V at the ILIMIT pin enables the current limit circuitry and when the SLx voltage goes beyond the ILIMIT pin voltage, the device turns off all GaNFETs for a time  $t_{FCLR}$ . The GaNFETs turn on again after  $t_{F_CLR}$  time elapses, depending on the status of input control signals. The ILIMIT functionality can be disabled by pulling up the ILIMIT pin voltage to more than  $V_{ILIMIT\_DIS}$ .

The overcurrent comparator has a blanking time of  $t_{blank}$  on every edge of INHx and INLx. The comparator also has a deglitch time of  $t_{deglitch}$ , when the comparator output toggles from low to high.

**Note**

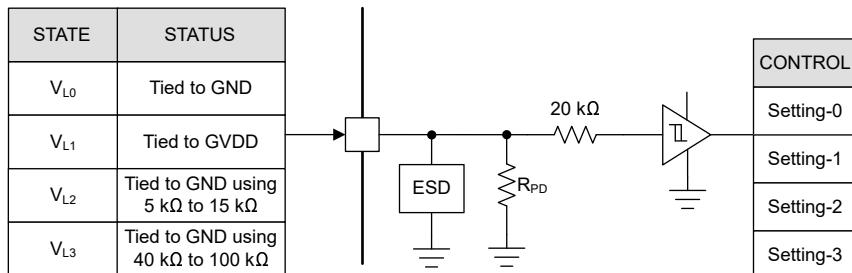
TI recommends an ILIMIT voltage of more than 0.2V to eliminate false trips due to noise. Use system-level design considerations by selecting an appropriate voltage at ILIMIT to eliminate any noise impact and select the shunt resistor value at SLx pins accordingly.

### 12.3.9 Pin Diagrams

This section presents the I/O structure of all digital input and output pins.

#### 12.3.9.1 Four-Level Input Pin

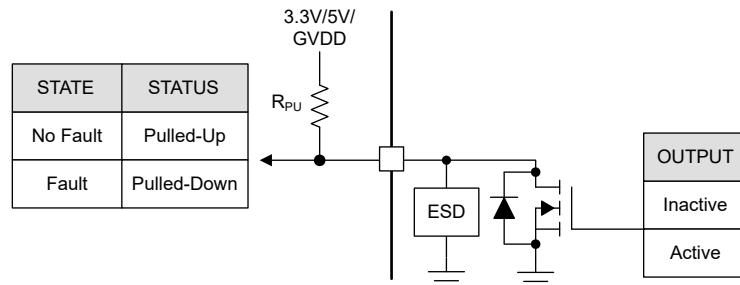
Figure 12-3 shows the structure of the four-level SR pin.



**Figure 12-3. Four-Level Input Pin**

### 12.3.9.2 Open-Drain Pin

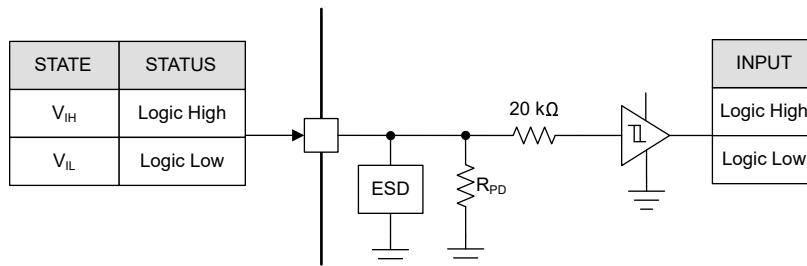
Figure 12-4 shows the structure of the open-drain output pin, nFAULT in open-drain mode. The open-drain output requires an external pullup resistor to function properly.



**Figure 12-4. Open-Drain Pin Structure**

### 12.3.9.3 Logic-Level Input Pin (Internal Pulldown)

Figure 12-5 shows the input structure for the logic level pins EN, INHx, INLx, ILIMIT, BRAKE. The input can be with a voltage or external resistor.



**Figure 12-5. Logic-Level Input Pin Structure**

## 12.4 Protections

The DRV7308 integrates GaN FET overcurrent protection (GaN\_OCP), overtemperature shutdown (OTSD), GVDD and bootstrap supply undervoltage protection (GVDD\_UVLO and VBOOT\_UVLO), and current limit (ILIMIT). Table 12-2 summarizes various faults in details.

**Table 12-2. Fault Action and Response**

FAULT	CONDITION	REPORT	GaN BRIDGE	RECOVERY
GaN overcurrent protection (GaN_OCP) <sup>(1)</sup>	Low-side GaN FET current > $I_{OCP\_GaN}$	nFAULT	All GaN pre-drivers turn off resulting Hi-Z (all three phases)	Latched. 20μs to 40μs toggling pulse on EN pin or GVDD power recycling
SLx overcurrent limit (ILIMIT)	$V_{SLx} > V_{ILIMIT}$	nFAULT	All GaN pre-drivers turn off resulting Hi-Z (all three phases)	Retry <sup>(2)</sup> . After a fault clear time > $t_{F\_CLR}$
GVDD undervoltage	$V_{GVDD} < V_{GVDD\_UV}$	nFAULT	All GaN pre-drivers turn off resulting Hi-Z (all three phases)	Automatic: $V_{GVDD} > V_{GVDD\_UVLO}$
Boot supply undervoltage (voltage between BOOTx and OUTx pin)	$V_{BOOTx} < V_{BST\_UV}$	-	The impacted high-side GaN pre-drivers turn off. All other GaNFETs continue to operate.	Automatic: $V_{BOOTx} > V_{BST\_UV}$
Thermal shutdown (OTSD)	$T_J > T_{SD}$ , for low-side GaNFET	nFAULT	All GaN pre-drivers turn off resulting Hi-Z (all three phases)	Automatic $T_J < T_{SD}$
	$T_J > T_{SD}$ , for high-side GaNFET			Latched. 20μs to 40μs toggling pulse on EN pin or GVDD power recycling

(1) Over current detection for low-side GaN FETs only.

(2) PWM inputs (INHx, INLx) must be low before the falling edge of nFAULT.

**Note**

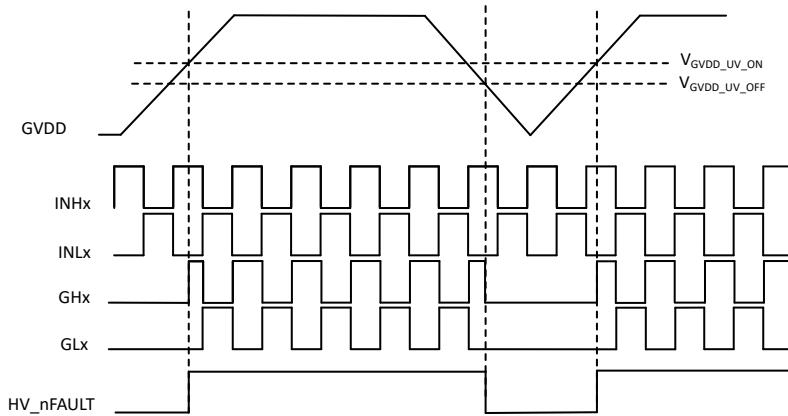
The GaN over current protection (GaN OCP) is available for low-side GaN FETs.

**WARNING**

The recovery condition of SL over current limit (ILIMIT) is valid if the PWM inputs (INHx, INLx) are low before the falling edge of nFAULT.

**12.4.1 GVDD Undervoltage Lockout**

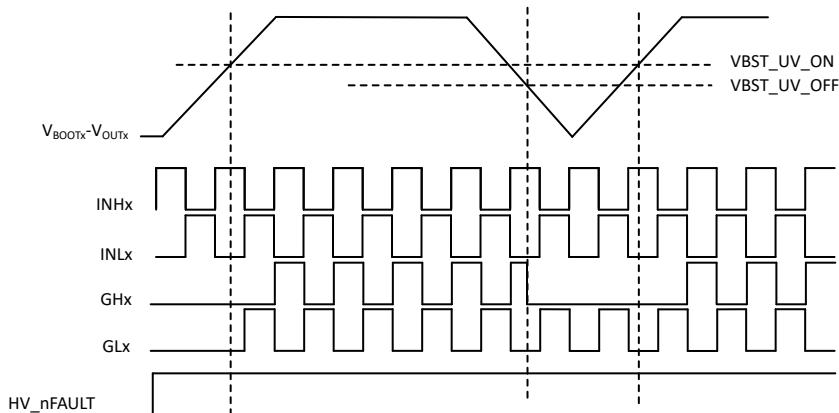
If at any time the voltage on the GVDD pin falls lower than the  $V_{GVDD\_UV}$  threshold, all integrated GaNFETs are turned off by turning off the GaN FET pre-drivers. Normal operation starts again when the GVDD\_UV condition clears. The GVDD\_UV is reported by driving the nFAULT pin low.



**Figure 12-6. GVDD Under voltage Lockout**

**12.4.2 Bootstrap Undervoltage Lockout**

If at any time the voltage across the bootstrap capacitor (BOOTx to OUTx voltage) pin falls lower than the  $V_{BST\_UV}$  threshold, the corresponding high-side GaN FET is turned off by turning off the high-side pre-driver. All the other GaN FETs continue to work as commanded by the INx pin. Normal operation starts again at the next rising edge of INHx pulse after the BST\_UV condition clears. The BOOTx undervoltage is not reported on nFAULT pin.

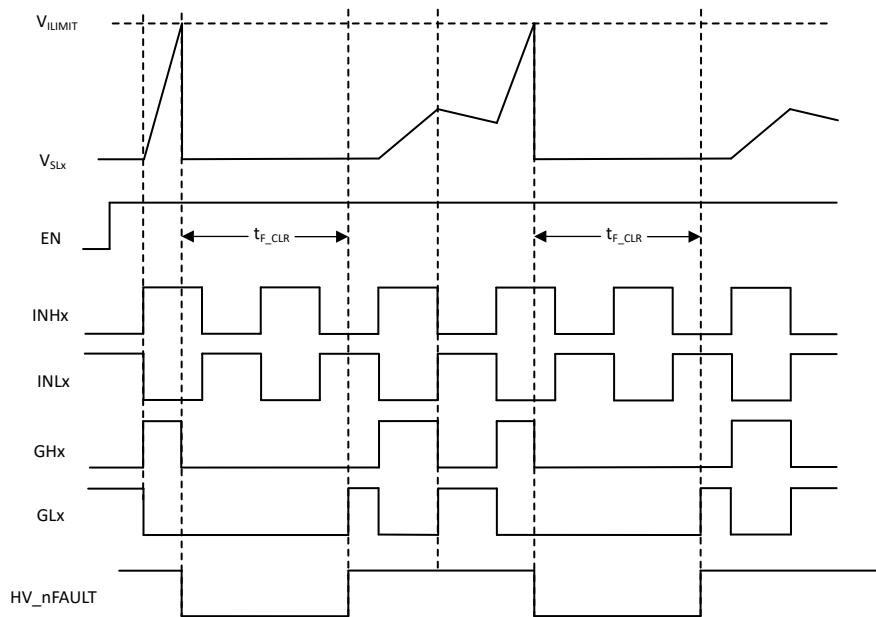


**Figure 12-7. Bootstrap Undervoltage Lockout**

**12.4.3 Current Limit Protection**

The DRV7308 integrates three comparators to protect the device, and external motor load, due to overload scenarios. DRV7308 has three integrated comparators, each monitoring voltage at SLA, SLB, and SLC pins

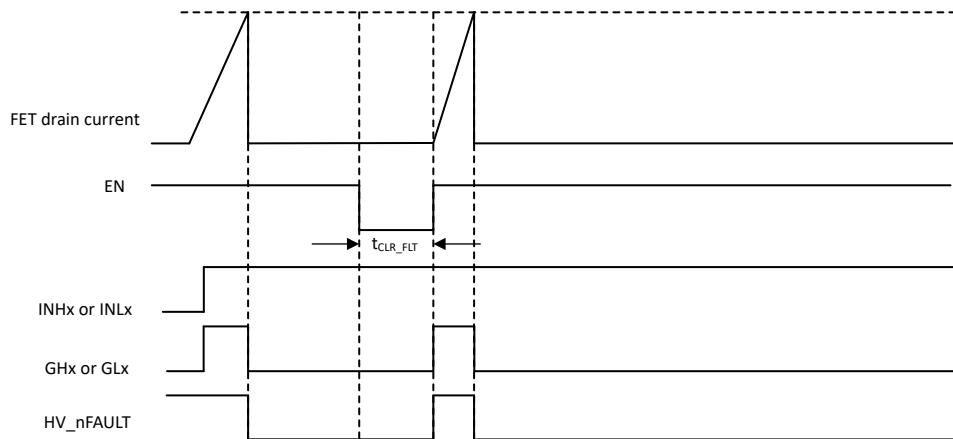
separately. A voltage less than 2V at the ILIMIT pin enables the current limit circuitry and when the SLx voltage goes beyond the ILIMIT pin voltage, the device turns off all GaN FETs for a time  $t_{F\_CLR}$ . The GaNFETs turn on again after  $t_{F\_CLR}$  time elapses, depending on the status of input control signals. The current limit is reported by driving the nFAULT pin low.



**Figure 12-8. Current Limit Operation**

#### 12.4.4 GaNFET Overcurrent Protection

The DRV7308 integrates overcurrent protection for each low-side GaN FET by monitoring the VDS of the GaN FETs. If at any time, the GaN FET current goes more than  $I_{OCP\_GaN}$ , all of the integrated GaNFETs are turned off by turning off the GaN FET pre-driver, and latched until cleared through a 20 $\mu$ s to 40 $\mu$ s toggling pulse on the EN pin or by a GVDD power recycling. The overcurrent event is reported by driving the nFAULT pin low.



**Figure 12-9. GaNFET Over current Protection**

#### 12.4.5 Thermal Shutdown (OTS)

If the die temperature near GaN FET exceeds the trip point of the thermal shutdown limit ( $T_{OTSD}$ ), all the GaNFETs are disabled, and the nFAULT pin is driven low. If OTSD event is detected due to high-side GaN FET temperature rise, the normal operation starts again (driver operation and the nFAULT pin is released) when the overtemperature condition clears and the fault is cleared through a 20 $\mu$ s to 40 $\mu$ s toggling pulse on the EN pin

or by GVDD power recycling. If OTSD event is detected due to low-side GaN FET temperature rise, the normal operation starts again when the over temperature condition clears.

## 13 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 13.1 Application Information

The DRV7308 is primarily used in applications for three-phase brushless DC motor control. The design procedures in the highlight how to use and configure the DRV7308 device.

### 13.2 Typical Application

#### 13.2.1 Application

Figure 13-1 shows a typical 3-phase motor drive application diagram of DRV7308.

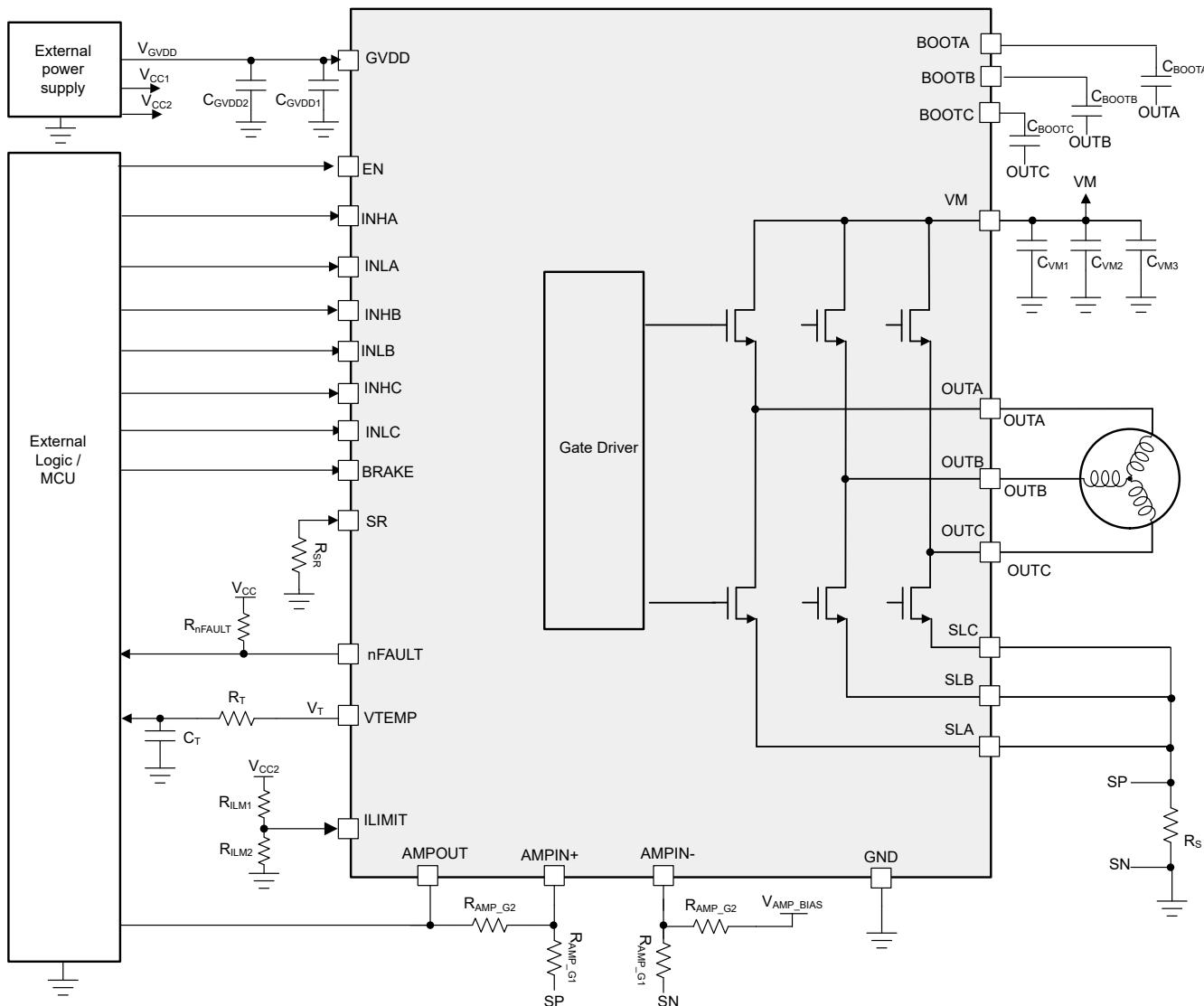


Figure 13-1. DRV7308 Typical Application Schematic

### 13.2.1.1 Application Information

Table 13-1 lists the recommended values of the external components for the driver.

**Table 13-1. DRV7308 External Components**

COMPONENTS	PIN1	PIN2	RECOMMENDED
$C_{VM1}$	VM	GND	X5R or X7R, 0.1 $\mu$ F, VM-rated capacitor
$C_{VM2}$	VM	GND	X5R or X7R, 0.1 $\mu$ F, VM-rated capacitor (optional)
$C_{VM3}$	VM	GND	$\geq 10\mu$ F, VM-rated capacitor
$C_{GVDD1}$	GVDD	GND	X5R or X7R, 0.1 $\mu$ F, GVDD-rated capacitor
$C_{GVDD2}$	GVDD	GND	$\geq 10\mu$ F, GVDD-rated capacitor
$C_{BOOTA}$	BOOTA	OUTA	X5R or X7R, 1 $\mu$ F to 220 $\mu$ F, GVDD-rated capacitor
$C_{BOOTB}$	BOOTB	OUTB	X5R or X7R, 1 $\mu$ F to 220 $\mu$ F, GVDD-rated capacitor
$C_{BOOTC}$	BOOTC	OUTC	X5R or X7R, 1 $\mu$ F to 220 $\mu$ F, GVDD-rated capacitor
$R_{SR}$	SR	GND	Resistor to determine slew rate setting
$R_{nFAULT}$	nFAULT	3.3V/ 5.5V / GVDD	5.1k $\Omega$ , Pullup resistor
$R_{ILM1}$	ILIMIT	3.3V/ 5.5V / GVDD	Based on required ILIMIT threshold
$R_{ILM2}$	ILIMIT	GND	Based on required ILIMIT threshold
$R_{VTEMP}$	VTEMP	system	Optional. VTEMP output filter resistor. 100 $\Omega$ , and application dependent.
$C_{VTEMP}$	VTEMP	GND	Optional. VTEMP output filter capacitor < 130pF.
$R_{AMP\_G2}$	AMPOUT	AMPIN+	Amplifier Gain Resistor 2. Application dependent.
$R_{AMP\_G1}$	AMPIN+	$V_{AMP\_REF}$	Amplifier Gain Resistor 1. Application dependent.
$R_S$	SLx (SP)	GND(SN)	Low-side Rshunt resistor to measure motor phase current ( $I_{LS\_PHASE}$ ). The expected current sense output voltage = $R_S \times I_{LS\_PHASE} \times R_{AMP\_G2}/R_{AMP\_G1} + V_{AMP\_REF}$
$V_{CC1}$	system	GND	System I/O reference voltage. 3.3V, 5V, or GVDD
$V_{CC2}$	system	GND	System I/O reference voltage. 3.3V, 5V. VCC2 needs to be separated from VCC1 only if VCC1 is higher than 5V.
$V_{AMP\_bias}$	$R_{AMP\_G2}$	system	Optional. System Current Sense measurement bias voltage

**Note**

TI recommends connecting pull up on nFAULT pin even if not used.

### 13.2.2 Application Curves

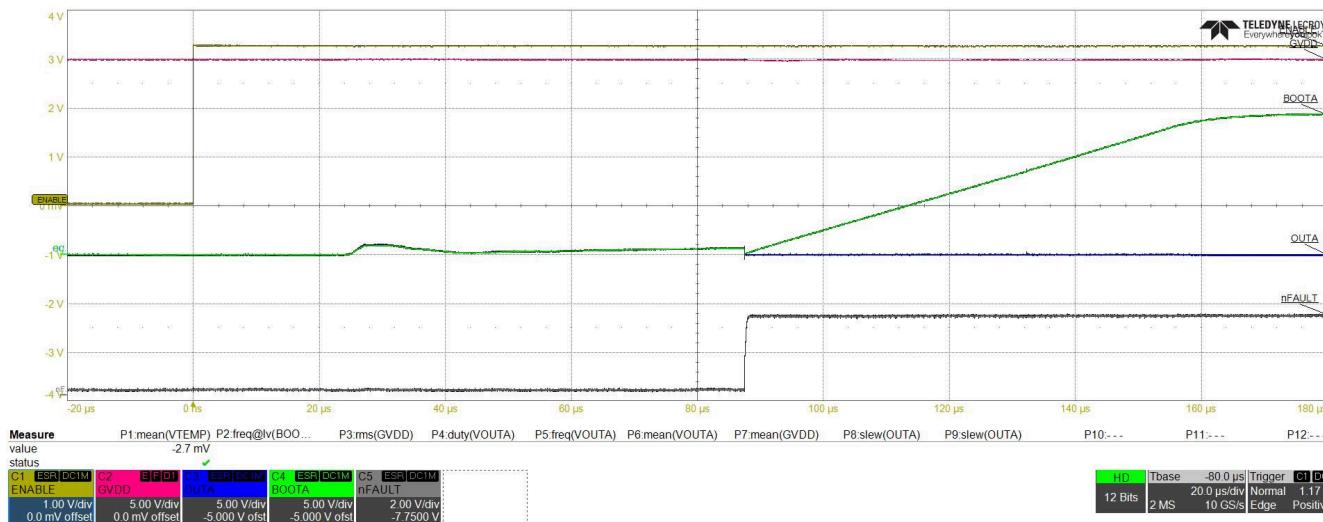


Figure 13-2. Device power up (EN pin low to high)

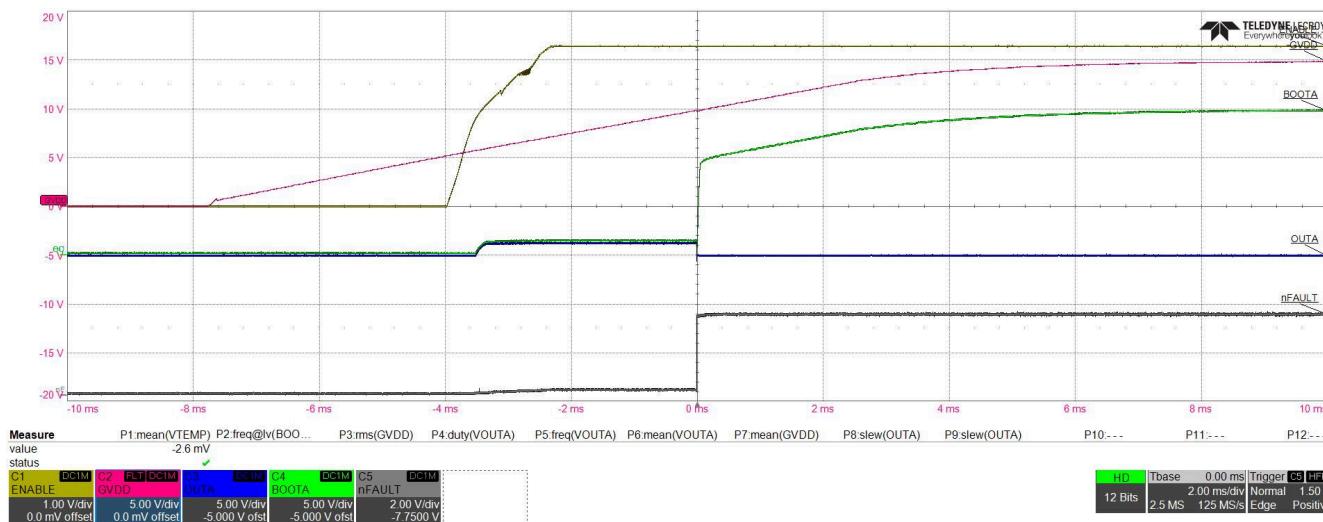


Figure 13-3. Device power up (GVDD start up)

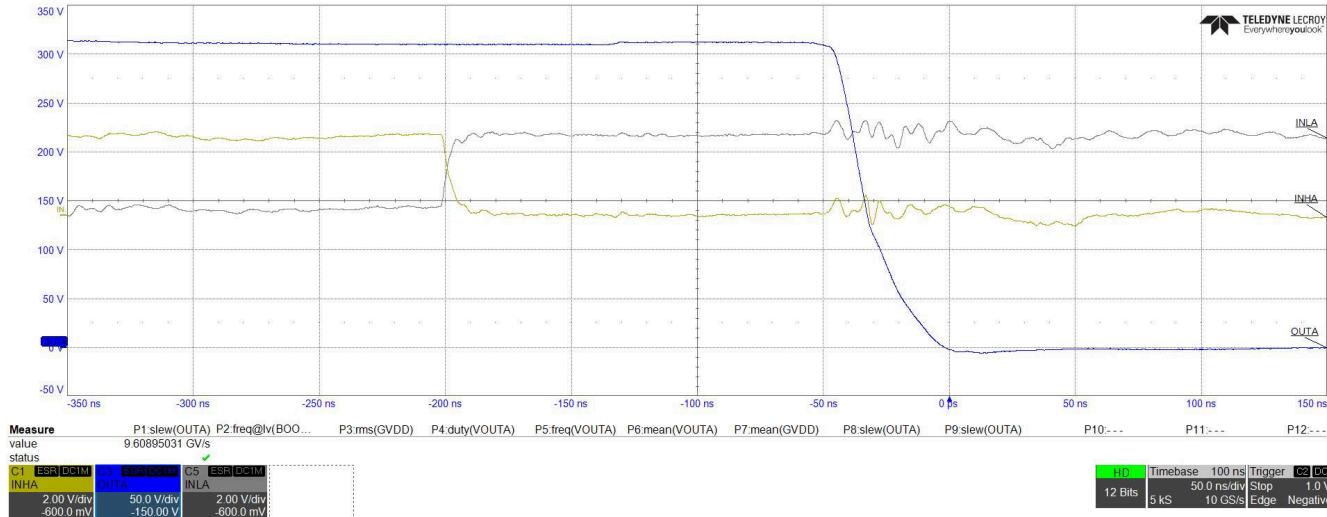


Figure 13-4. Motor phase node OUTA switching - falling edge (phase current from motor load to device)

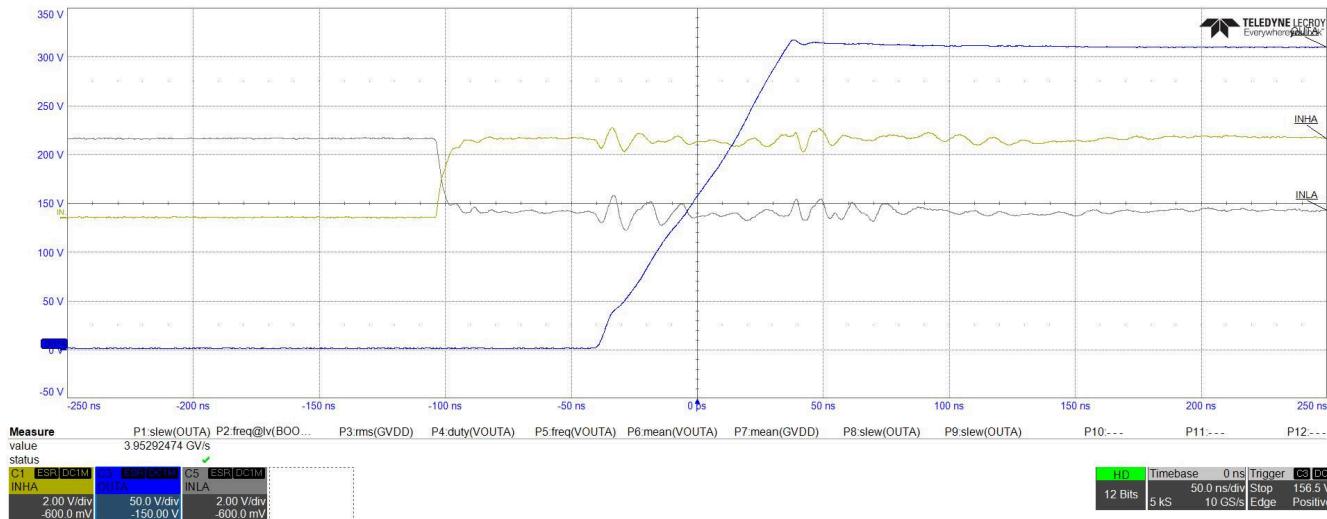


Figure 13-5. Motor phase node OUTA switching - rising edge (phase current from motor load to device)

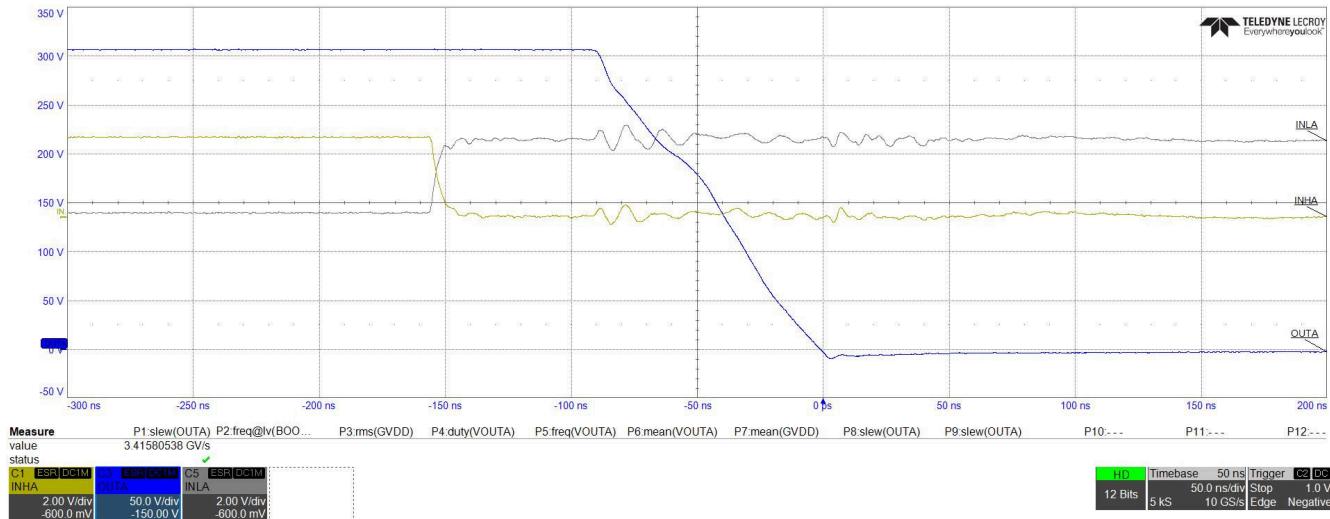


Figure 13-6. Motor phase node OUTA switching - falling edge (phase current from device to motor load)

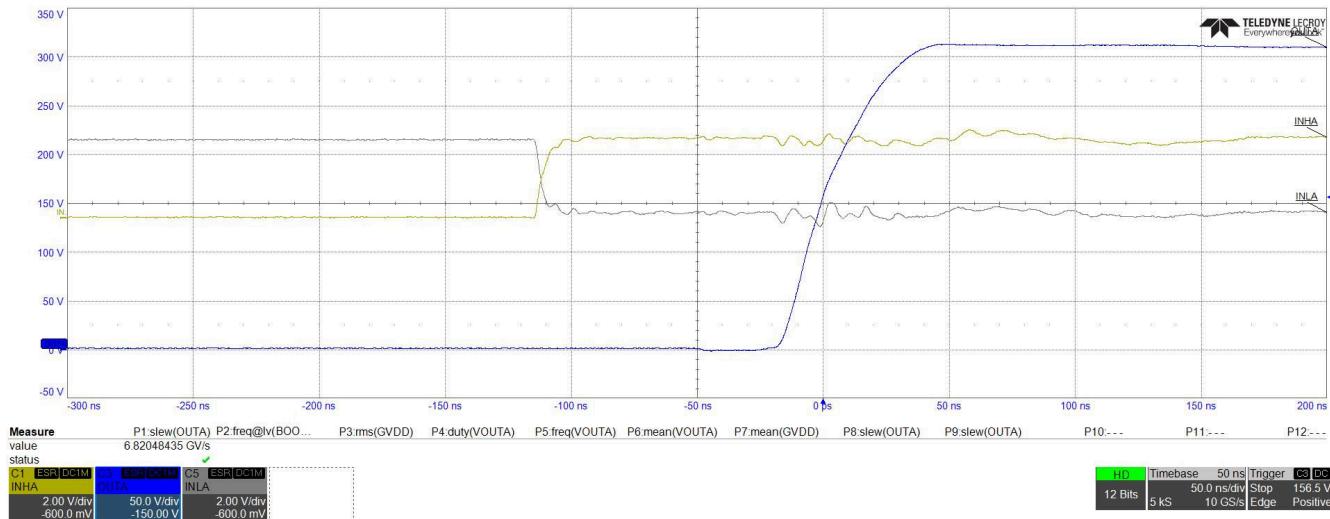
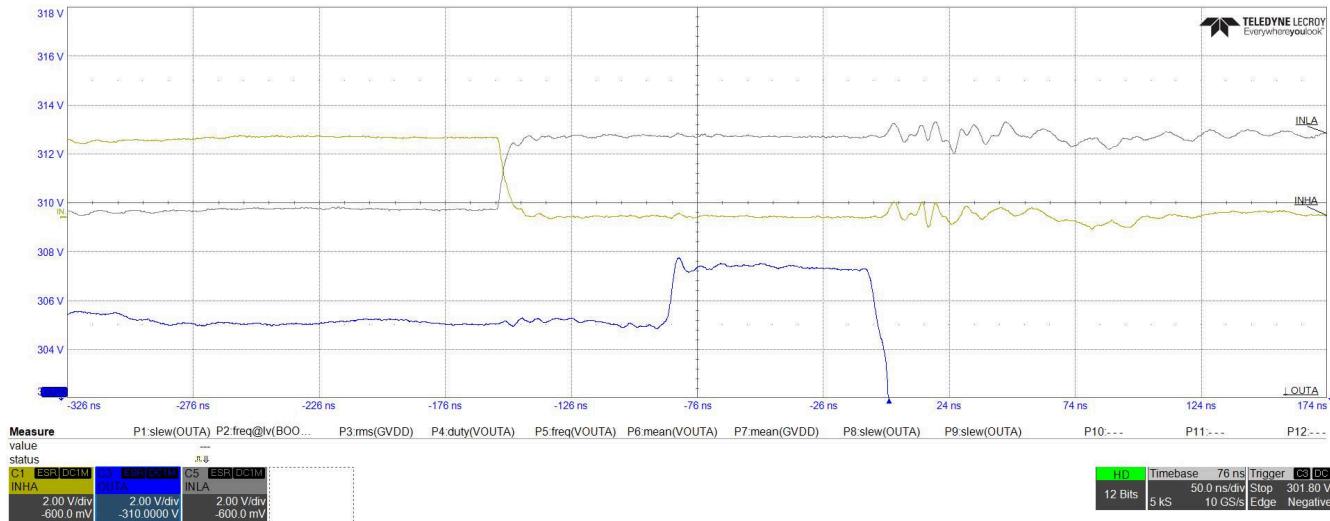
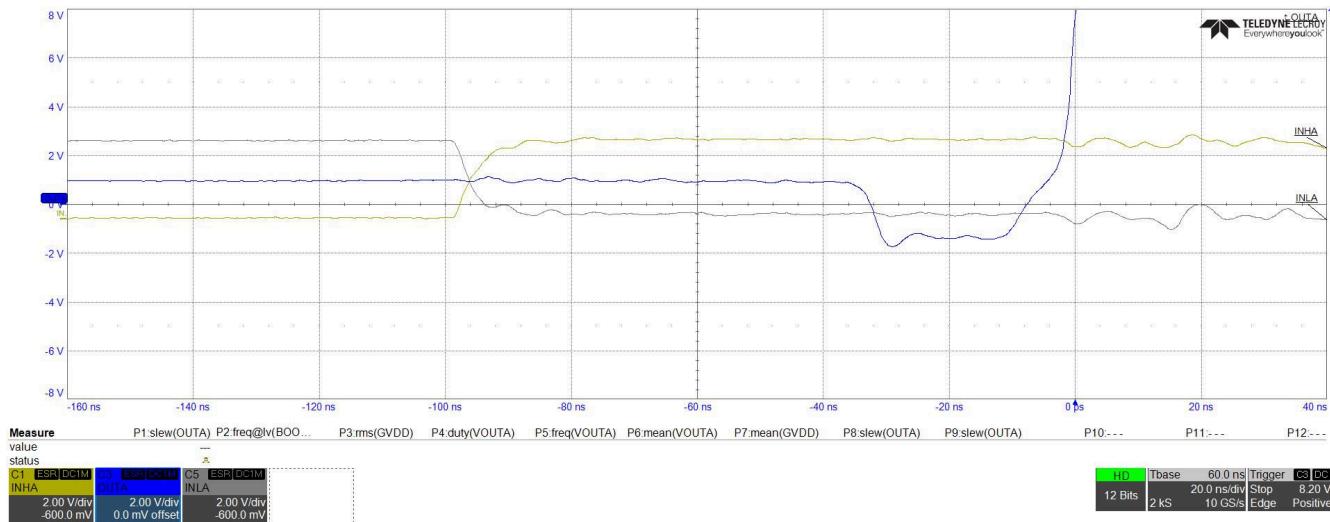


Figure 13-7. Motor phase node OUTA switching -rising edge (phase current from device to motor load)



**Figure 13-8. Motor phase node OUTA switching - High-side GaN FET Third Quadrant operation (phase current from motor load to device)**



**Figure 13-9. Motor phase node OUTA switching - Low-side GaN FET Third Quadrant operation (phase current from device to motor load)**

## 14 Layout

### 14.1 Layout Guidelines

The bulk capacitor must be placed to minimize the distance of the high-current path through the motor driver device. The connecting metal trace widths must be as wide as possible and numerous vias must be used when connecting PCB layers. These practices minimize inductance and allow the bulk capacitor to deliver high current.

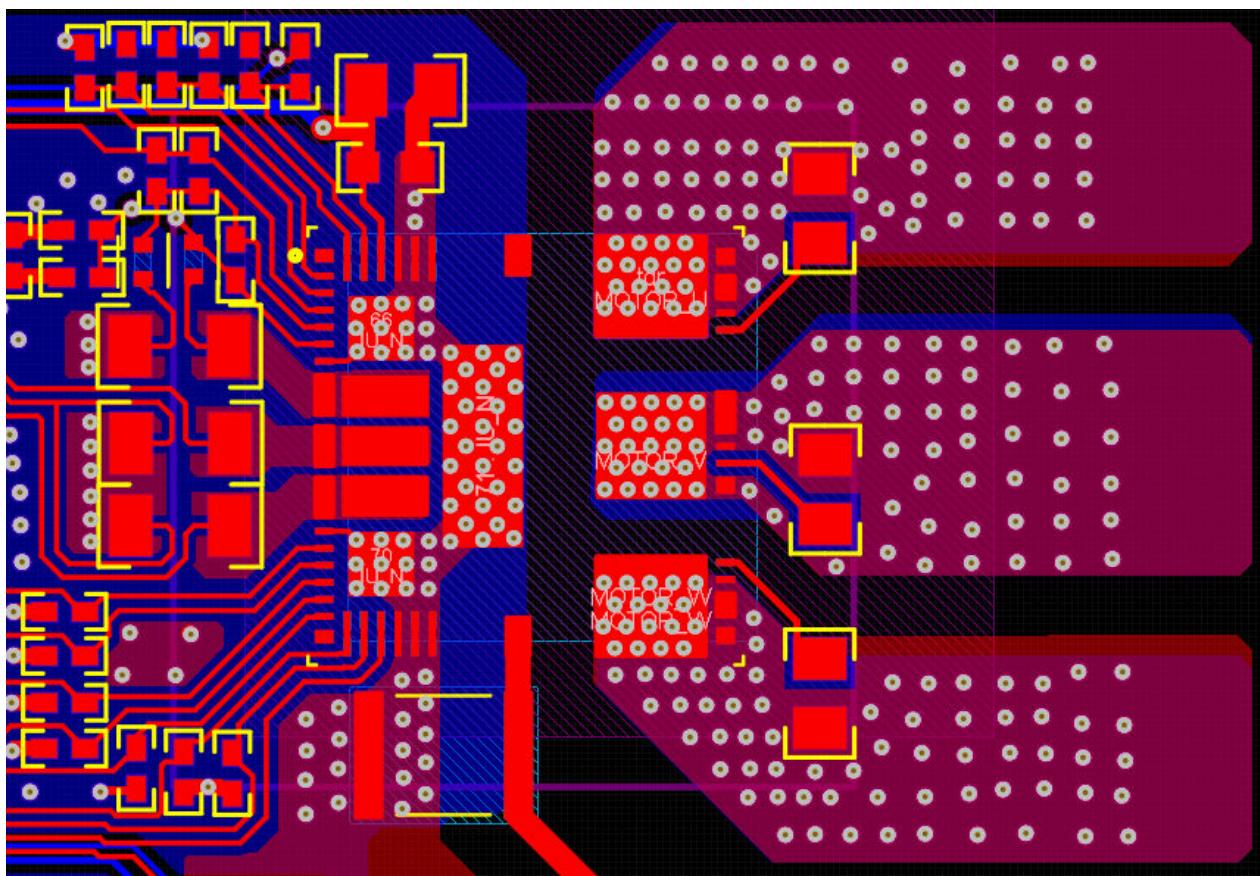
Small-value capacitors such as the GVDD decoupling capacitor, high frequency capacitor on VM pin to GND, and the bootstrap capacitors must be placed close to device pins.

To minimize the power loop area, place the shunt resistors close to the device SL<sub>x</sub> pins and use copper polygon on the end of the shunt resistor, and return the current pack to the decoupling capacitor on the VM pin with a wider trace on the top layer, or through a copper polygon on the bottom layer with a sufficient number of stitching vias.

To improve thermal performance, maximize the copper planes on OUT<sub>x</sub> and GND nets. To maximize the thermal performance, use multiple stitching vias on the OUT<sub>x</sub> pads and GND pads and use larger copper planes on the top and bottom layers, as shown in the [Figure 14-1](#).

The decoupling capacitor on the VM pin can be connected to any one side VM pin or to both the pins. The VM pins are internally shorted in the device and there is no need to short externally on the PCB.

### 14.2 Layout Example



**Figure 14-1. Recommended Layout for VQFN Package**

## 15 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

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<b>Changes from Revision * (May 2024) to Revision A (October 2025)</b>	<b>Page</b>
• Updated device status to production data.....	1

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## 16 Device and Documentation Support

TI offers an extensive line of development tools. Tools and software to evaluate the performance of the device, generate code, and develop solutions are listed below.

### 16.1 Documentation Support

#### 16.1.1 Related Documentation

- Texas Instruments, [Layout Design Guide with DRV7308 for Improved Thermal Performance application note, application note](#)
- Texas Instruments, [How Three-Phase Integrated GaN Technology Maximizes Motor-Drive Performance, white paper](#)
- Texas Instruments, [DRV7308 Evaluation Module User's Guide](#)
- Texas Instruments, [Achieving household energy efficiency and cost savings with GaN-based motor system designs, technical article](#)
- Texas Instruments, [Thermal calculator for the DRV7308 to estimate power loss and device temp, design tool & simulation](#)

### 16.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](http://ti.com). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 16.3 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 16.4 Trademarks

TI E2E™ is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

### 16.5 Electrostatic Discharge Caution

 This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

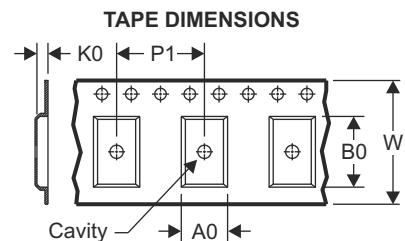
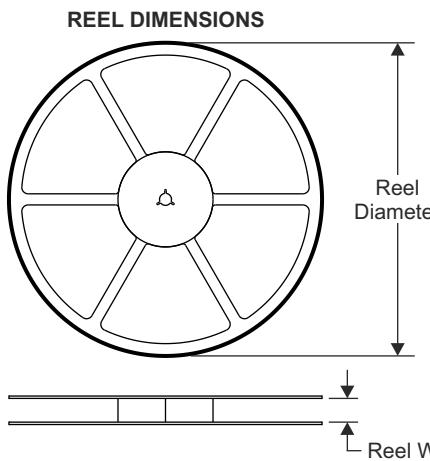
### 16.6 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

## 17 Mechanical, Packaging, and Orderable Information

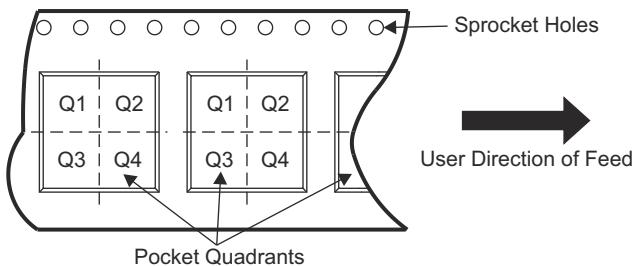
The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## 17.1 Tape and Reel Information



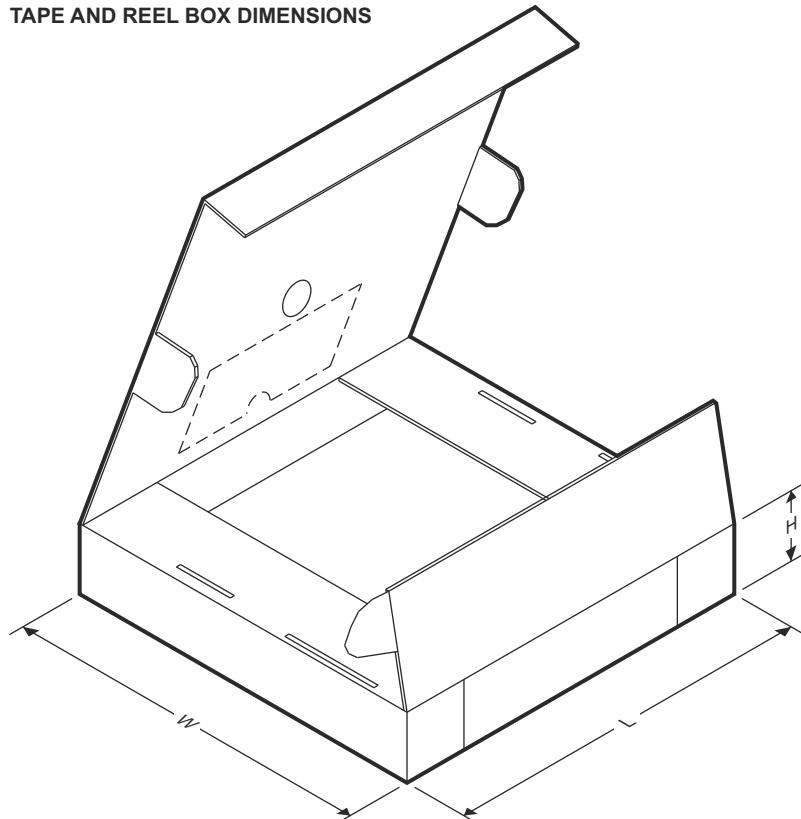
A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

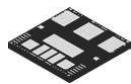


Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
DRV7308HRENR	VQFN	REN	65	2000	330.0	24.4	12.4	12.4	1.5	1.5	24.4	Q1

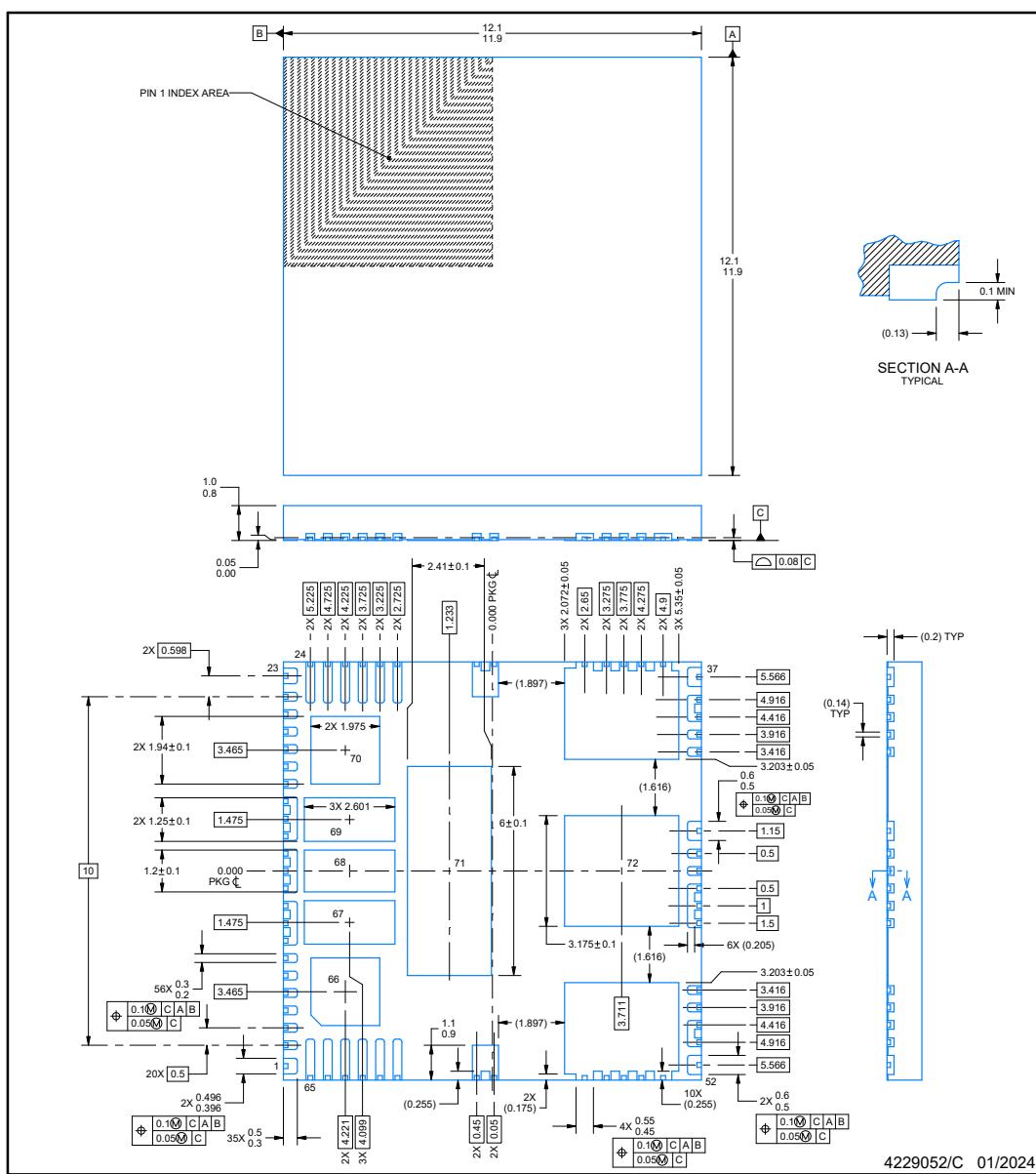
TAPE AND REEL BOX DIMENSIONS



Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
DRV7308HRENR	VQFN	REN	65	2000	12.4	12.4	1.5

**REN0065A****PACKAGE OUTLINE****VQFN - 1 mm max height**

PLASTIC QUAD FLATPACK - NO LEAD



## NOTES:

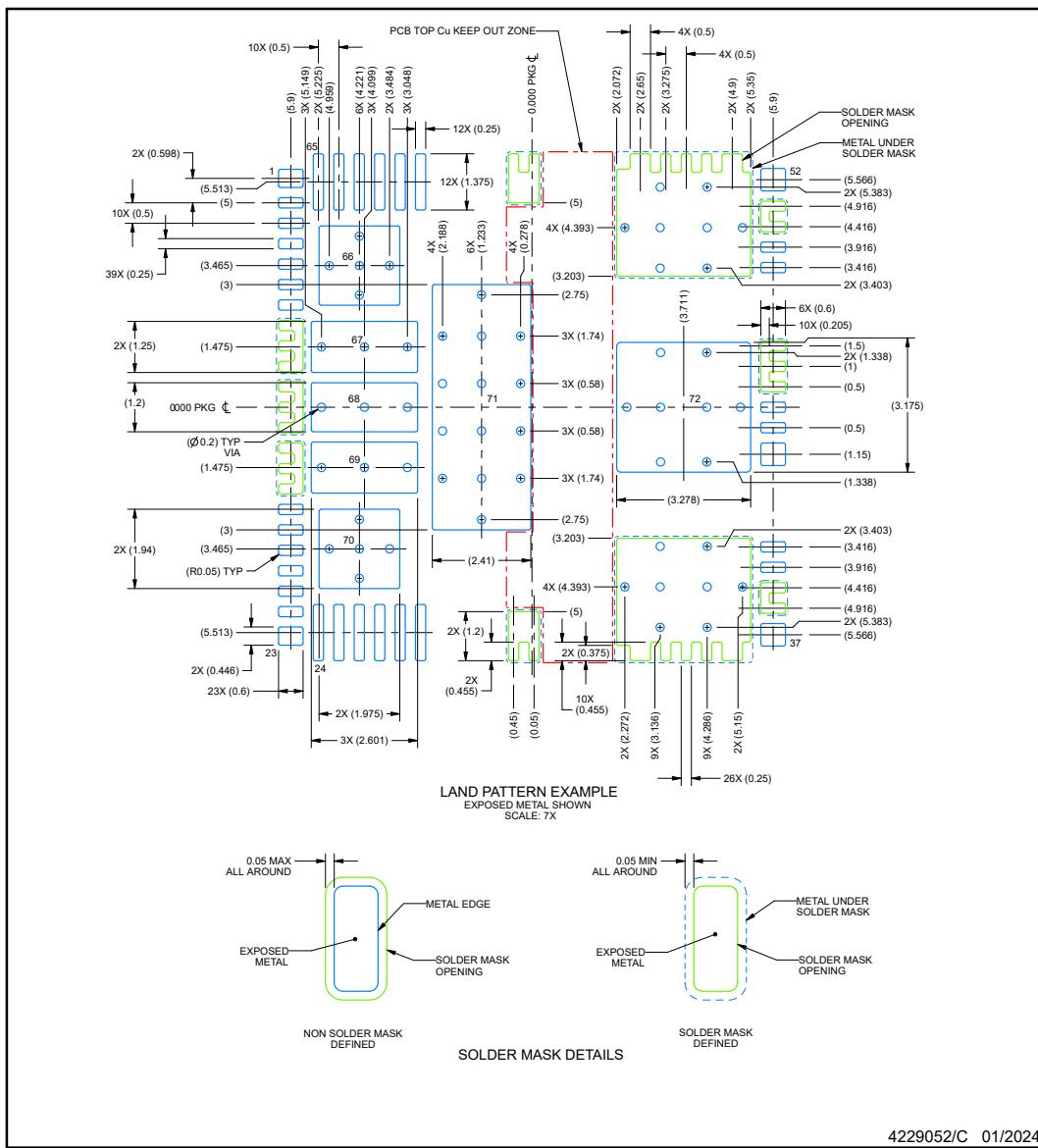
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad(s) must be soldered to the printed circuit board for thermal and mechanical performance.

## EXAMPLE BOARD LAYOUT

### REN0065A

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

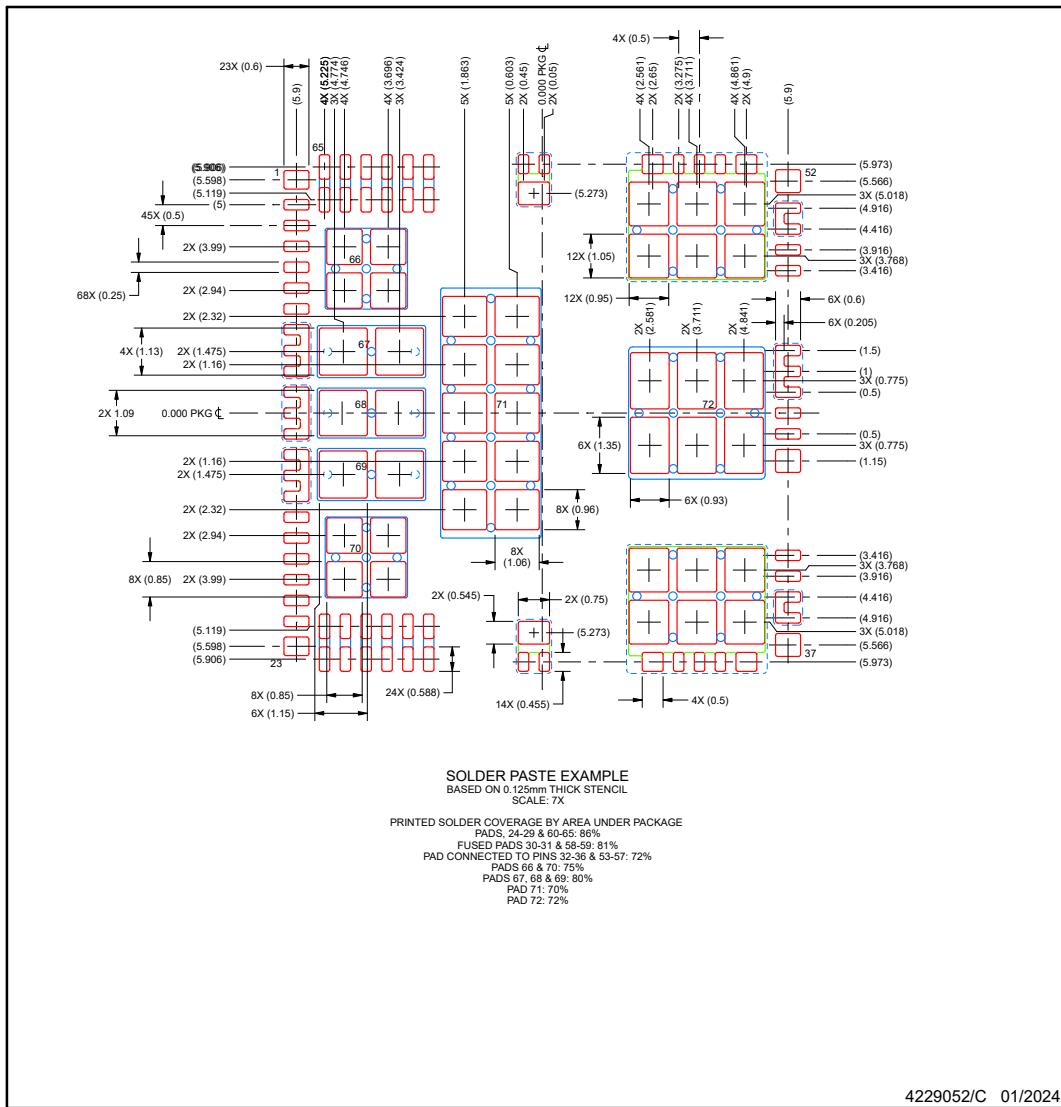


## EXAMPLE STENCIL DESIGN

**REN0065A**

## VQFN - 1 mm max height

## PLASTIC QUAD FLATPACK - NO LEAD



NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
DRV7308RENR	Active	Production	VQFN (REN)   65	3000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168HRS	-40 to 125	7308 NNNNC
PDRV7308HRENR.A	Active	Preproduction	VQFN (REN)   68	3000   LARGE T&R	-	Call TI	Call TI	-40 to 125	

<sup>(1)</sup> **Status:** For more details on status, see our [product life cycle](#).

<sup>(2)</sup> **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

<sup>(4)</sup> **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

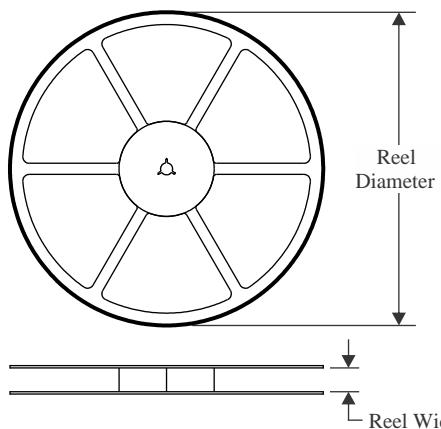
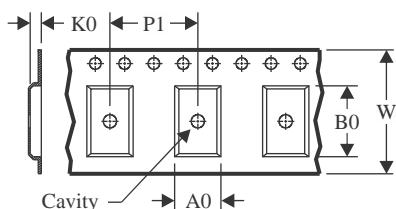
<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

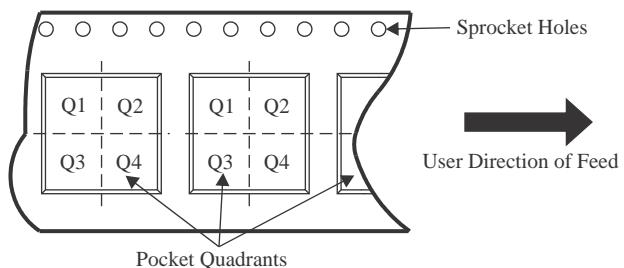
Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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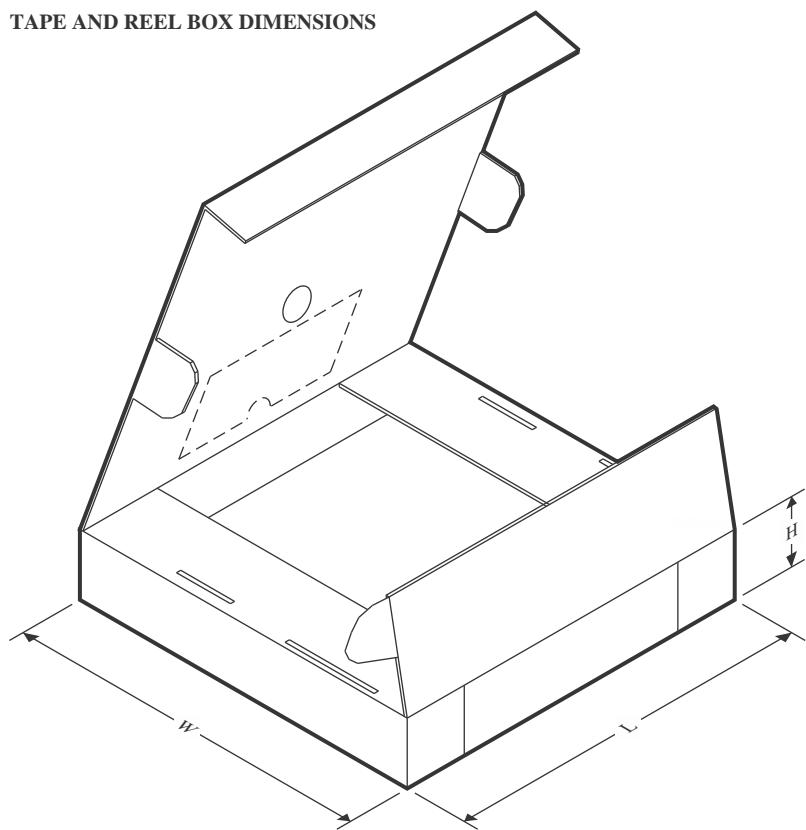
**TAPE AND REEL INFORMATION**
**REEL DIMENSIONS**

**TAPE DIMENSIONS**


A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
DRV7308RENR	VQFN	REN	65	3000	330.0	24.4	12.3	12.3	1.1	16.0	24.0	Q2

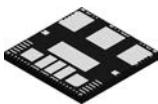
**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
DRV7308RENR	VQFN	REN	65	3000	367.0	367.0	45.0

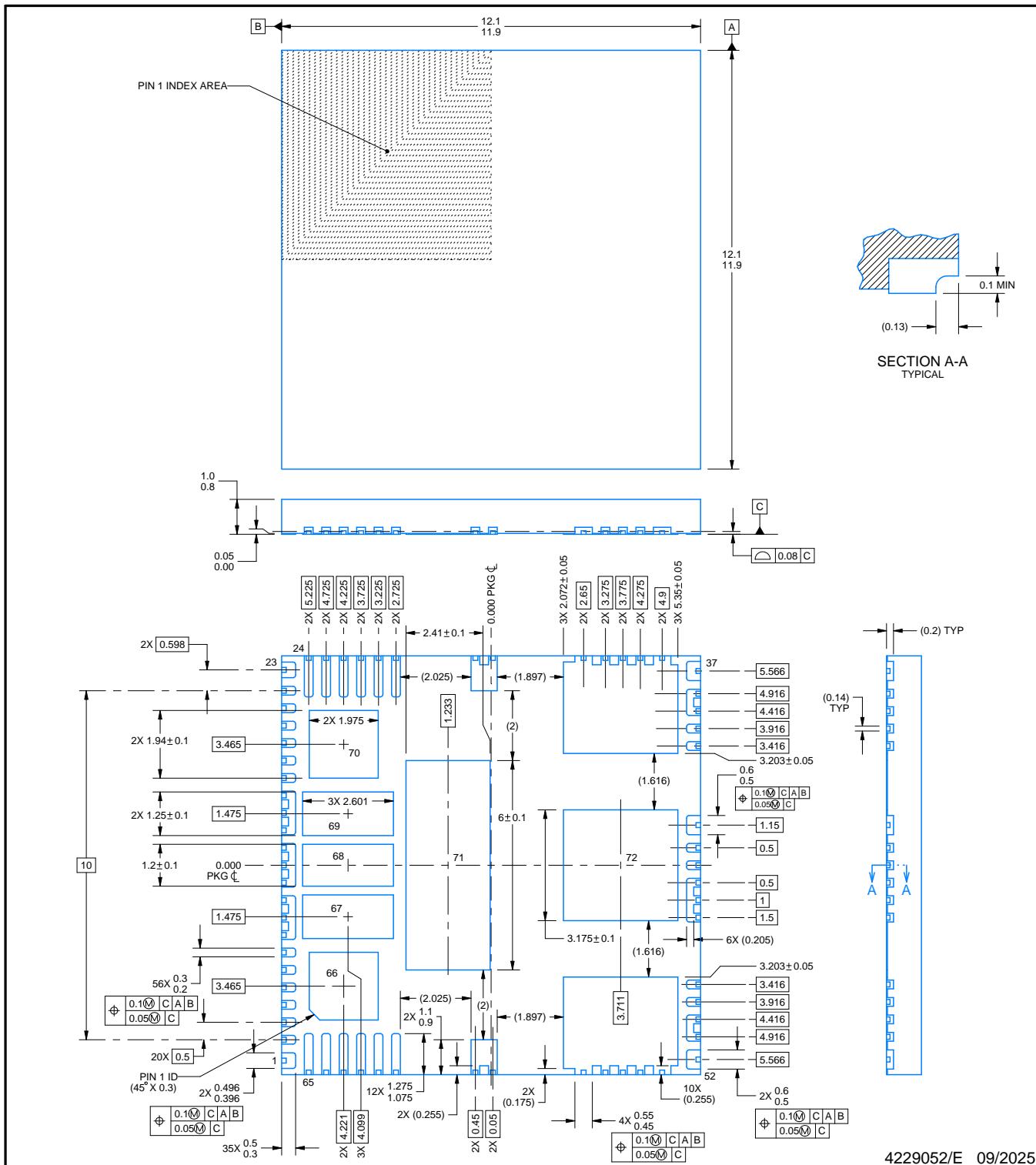
## PACKAGE OUTLINE

**REN0065A**



## VQFN - 1 mm max height

## PLASTIC QUAD FLATPACK - NO LEAD



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**NOTES:**

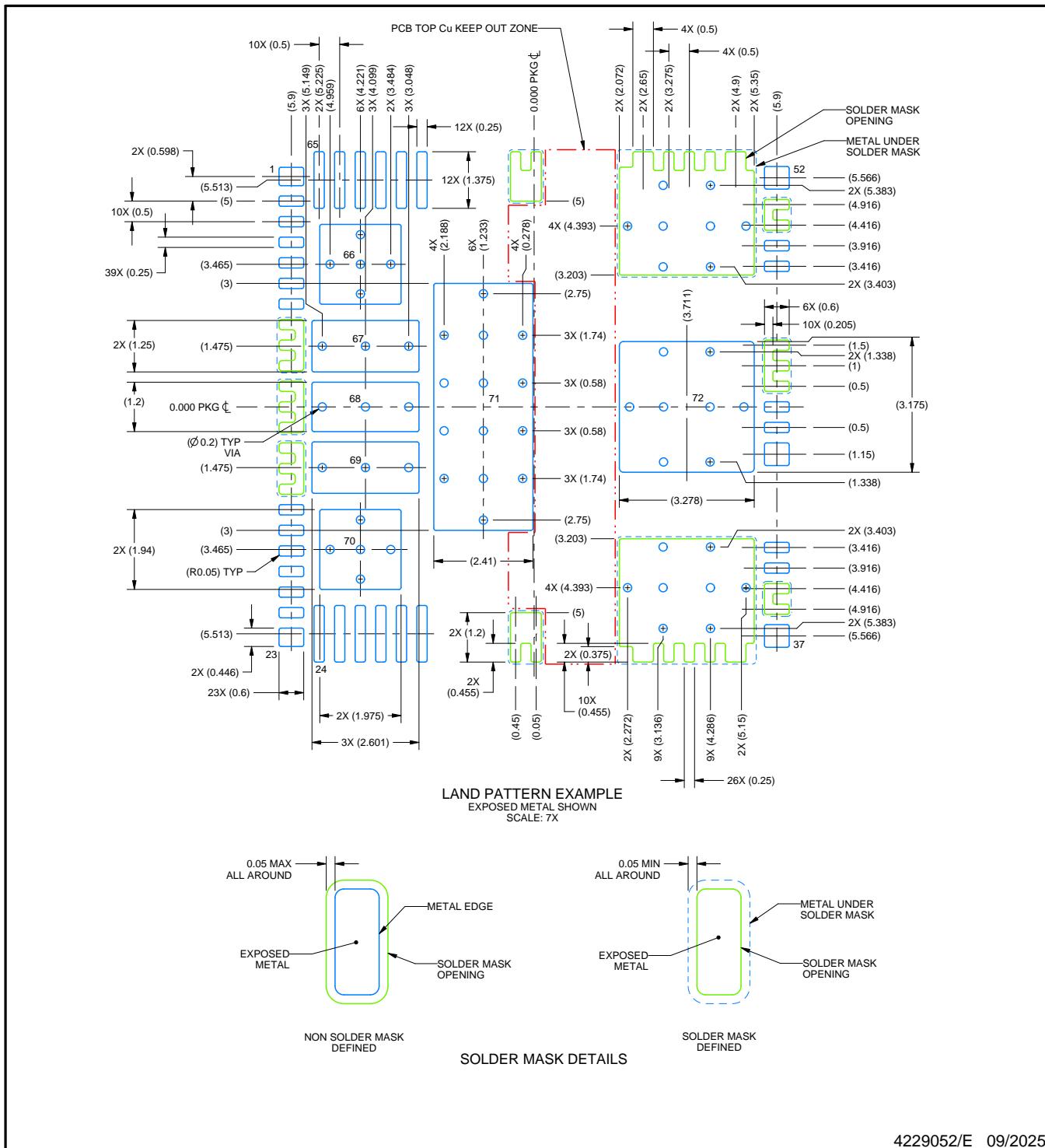
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad(s) must be soldered to the printed circuit board for thermal and mechanical performance.

# EXAMPLE BOARD LAYOUT

REN0065A

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



NOTES: (continued)

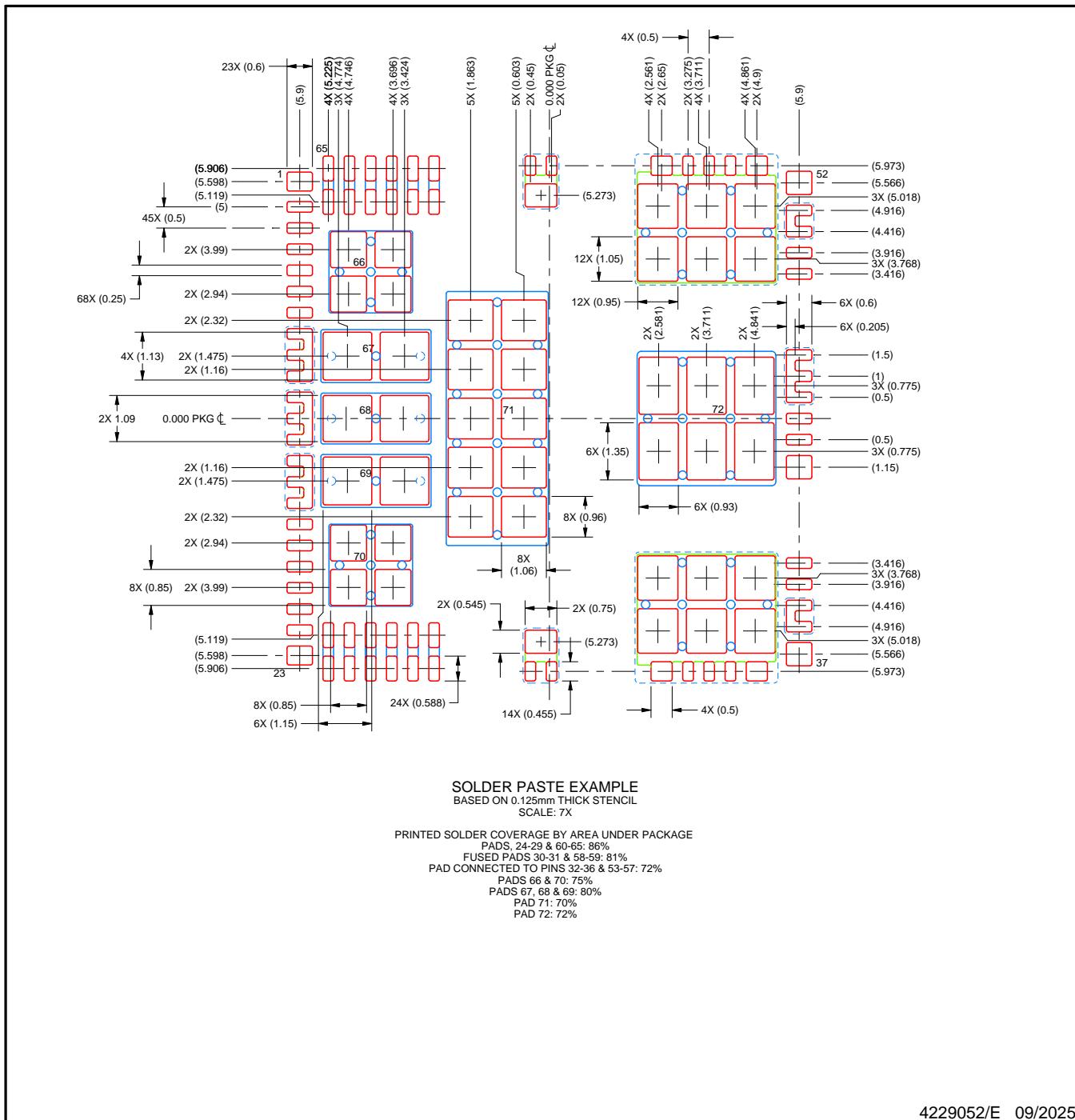
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/slua271](http://www.ti.com/lit/slua271)).
5. Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.

# EXAMPLE STENCIL DESIGN

REN0065A

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



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NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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