

## Temperature Sensing NTC Circuit With MSP430™ Smart Analog Combo

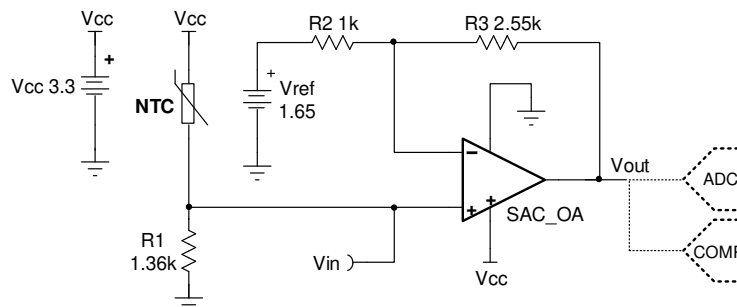
### Design Goals

Temperature		Output Voltage		Supply		
$T_{Min}$	$T_{Max}$	$V_{outMin}$	$V_{outMax}$	$V_{cc}$	$V_{ee}$	$V_{ref}$
25°C	50°C	0.2 V	3.1 V	3.3 V	0 V	1.65 V

### Design Description

Some MSP430™ microcontrollers (MCUs) contain configurable integrated signal chain elements such as op-amps, DACs, and programmable gain stages. These elements make up a peripheral called the Smart Analog Combo (SAC). For information on the different types of SACs and how to leverage their configurable analog signal chain capabilities, visit [MSP430 MCUs Smart Analog Combo Training](#). To get started with your design, download the [Temperature Sensing NTC Circuit Design Files](#).

This temperature sensing circuit uses a resistor in series with a negative-temperature-coefficient (NTC) thermistor to form a voltage divider, which produces an output voltage that is linear over temperature. The circuit uses the [MSP430FR2311](#) SAC\_L1 op-amp in a noninverting amplifier configuration with inverting reference to offset and gain the signal, which helps to use the full ADC resolution and increase measurement accuracy. (Note: The [MSP430FR2355](#) features four SAC\_L3 peripherals which each contain a built-in DAC and PGA, providing a single-chip solution for generating  $V_{ref}$  and measuring the thermistor circuit.) The output of the integrated SAC op-amp can be sampled directly by the on-board ADC or monitored by the on-board comparator for further processing inside the MCU.



### Design Notes

- The connection,  $V_{in}$ , is a negative temperature coefficient output voltage. To measure the output voltage of a PTC thermistor, switch the position of  $R_1$  and the thermistor.
- $V_{ref}$  can be generated using one of the integrated SAC\_L3 DACs in the MSP430FR2355 or a voltage divider. If a voltage divider is used the equivalent resistance of the voltage divider will influence the gain of the circuit.
- Using high value resistors can degrade the phase margin of the amplifier and introduce additional noise in the circuit. It is recommended to use resistor values of approximately 10 k $\Omega$  or less.
- If the solution is implemented using the MSP430FR2311, the SAC\_L1 op-amp is configured in general purpose mode to measure the thermistor circuit.
- If the solution is implemented using the MSP430FR2355, one SAC\_L3 peripheral is configured in DAC mode to generate the reference voltage and another is configured in general purpose mode to measure the thermistor circuit.

## Design Steps

$$V_{out} = V_{cc} \times \frac{R_1}{R_{NTC} + R_1} \times \frac{R_2 + R_3}{R_2} - \frac{R_3}{R_2} \times V_{ref}$$

1. Calculate the value of  $R_1$  to produce a linear output voltage. Use the minimum and maximum values of the NTC to obtain a range of values for  $R_1$ .

$$R_{NTC\_max} = R_{NTC @ 25^\circ C} = 2.252 \text{ k}\Omega, \quad R_{NTC\_min} = R_{NTC @ 50^\circ C} = 819.7 \Omega$$

$$R_1 = \sqrt{R_{NTC @ 25^\circ C} \times R_{NTC @ 50^\circ C}} = \sqrt{2.252 \text{ k}\Omega \times 819.7 \Omega} = 1.359 \text{ k}\Omega \approx 1.36 \text{ k}\Omega$$

2. Calculate the input voltage range.

$$V_{inMin} = V_{cc} \times \frac{R_1}{R_{NTC\_max} + R_1} = 3.3 \text{ V} \times \frac{1.36 \text{ k}\Omega}{2.252 \text{ k}\Omega + 1.36 \text{ k}\Omega} = 1.2418 \text{ V}$$

$$V_{inMax} = V_{cc} \times \frac{R_1}{R_{NTC\_min} + R_1} = 3.3 \text{ V} \times \frac{1.36 \text{ k}\Omega}{819.7 \Omega + 1.36 \text{ k}\Omega} = 2.0582 \text{ V}$$

3. Calculate the gain required to produce the maximum output swing.

$$G_{ideal} = \frac{V_{outMax} - V_{outMin}}{V_{inMax} - V_{inMin}} = \frac{3.1 \text{ V} - 0.2 \text{ V}}{2.0582 \text{ V} - 1.2418 \text{ V}} = 3.5519 \frac{\text{V}}{\text{V}}$$

4. Select  $R_2$  and calculate  $R_3$  to set the gain in Step 3.

$$\text{Gain} = \frac{R_2 + R_3}{R_2}$$

$$R_2 = 1 \text{ k}\Omega \text{ (Standard value)}$$

$$R_3 = R_2 \times (G_{ideal} - 1) = 1 \text{ k}\Omega \times (3.5519 \frac{\text{V}}{\text{V}} - 1) = 2.5519 \text{ k}\Omega$$

$$\text{Choose } R_3 = 2.55 \text{ k}\Omega$$

5. Calculate the actual gain based on standard values of  $R_2$  and  $R_3$ .

$$G_{actual} = \frac{R_2 + R_3}{R_2} = \frac{1 \text{ k}\Omega + 2.55 \text{ k}\Omega}{1 \text{ k}\Omega} = 3.55 \frac{\text{V}}{\text{V}}$$

6. Calculate the output voltage swing based on the actual gain.

$$V_{out\_swing} = (V_{inMax} - V_{inMin}) \times G_{actual} = (2.0582 \text{ V} - 1.2418 \text{ V}) \times 3.55 \frac{\text{V}}{\text{V}} = 2.9 \text{ V}$$

7. Calculate the maximum output voltage when the output voltage is symmetrical around mid-supply.

$$V_{outMax} = V_{mid-supply} + \frac{V_{out\_swing}}{2} = \frac{V_{cc} - V_{ee}}{2} + \frac{V_{out\_swing}}{2} = \frac{3.3 \text{ V} - 0 \text{ V}}{2} + \frac{2.9 \text{ V}}{2} = 3.1 \text{ V}$$

8. Calculate the reference voltage.

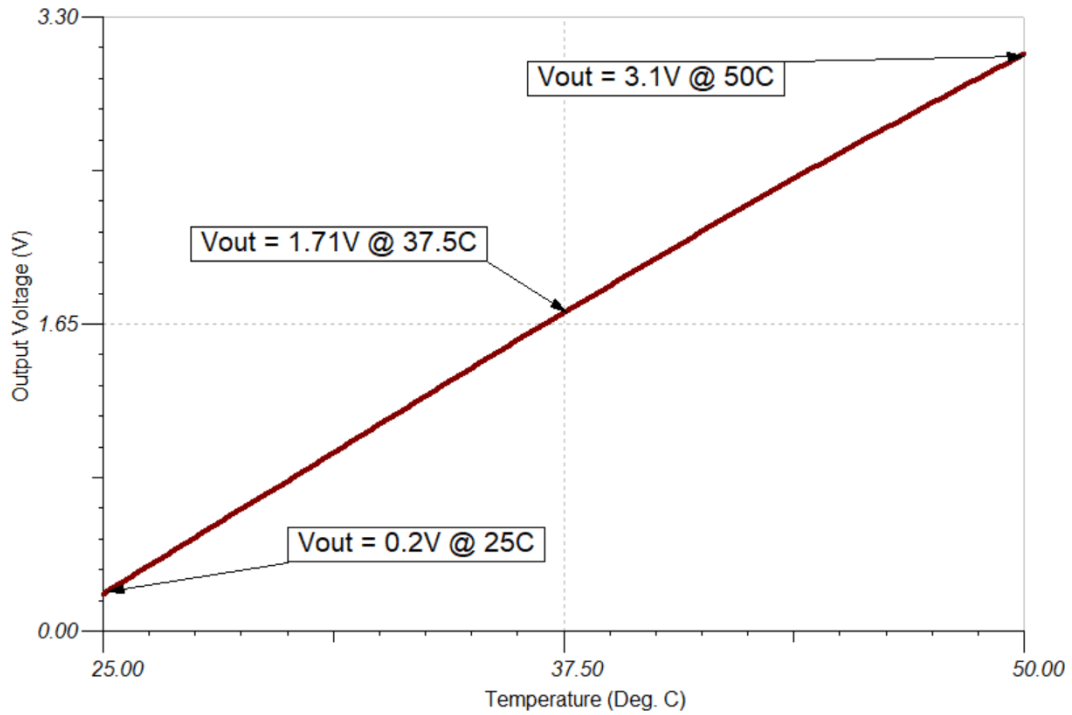
$$V_{outMax} = V_{inMax} \times G_{actual} - \frac{R_3}{R_2} \times V_{ref}$$

$$3.1 \text{ V} = 2.0582 \text{ V} \times 3.55 \frac{\text{V}}{\text{V}} - \frac{2.55 \text{ k}\Omega}{1 \text{ k}\Omega} \times V_{ref}$$

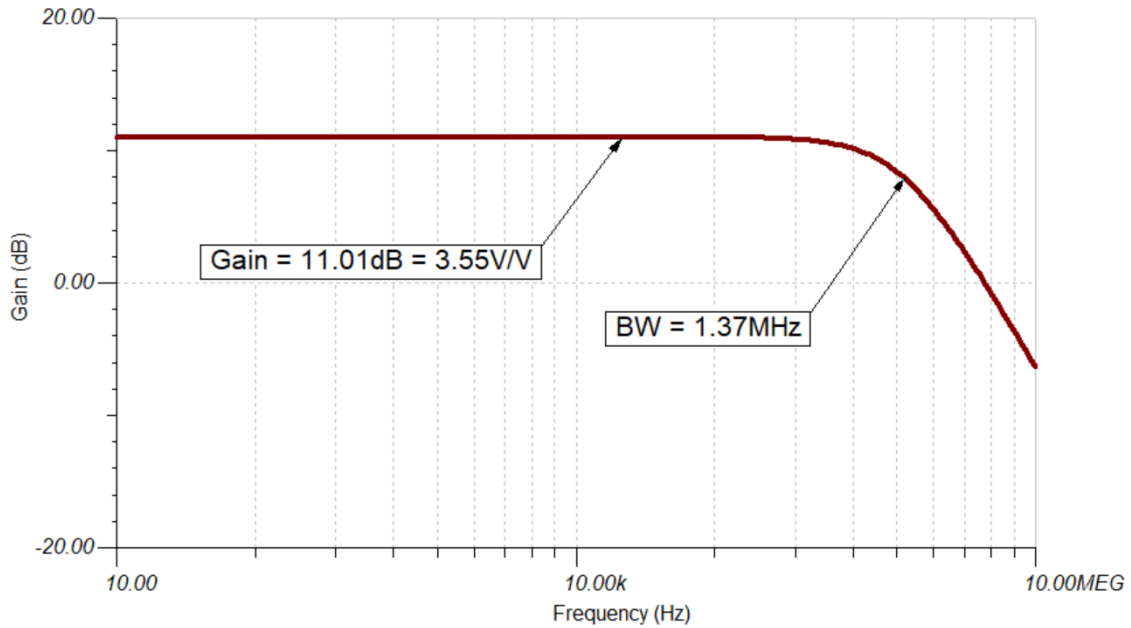
$$V_{ref} = \frac{2.0582 \text{ V} \times 3.55 \frac{\text{V}}{\text{V}} - 3.1 \text{ V}}{\frac{2.55 \text{ k}\Omega}{1 \text{ k}\Omega}} = 1.65 \text{ V}$$

**Design Simulations**

**DC Transfer Results**



**AC Simulation Results**



**Target Applications**

- [Field temperature transmitters](#)
- [Thermostats](#)
- [Thermometers](#)
- Thermistor probes
- System temperature monitor

## References



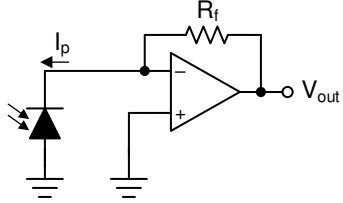
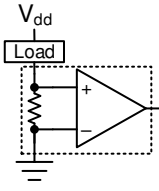
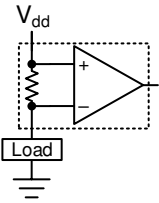
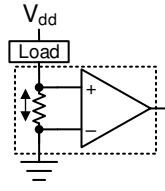

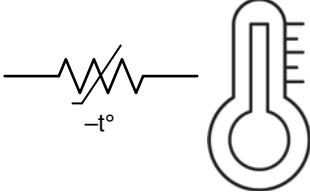
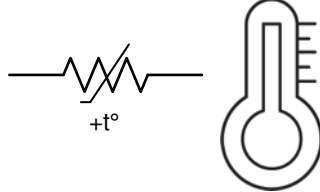
1. [MSP430 MCUs Smart Analog Combo Training](#)
2. [Analog Engineer's Circuit Cookbooks](#)
3. [MSP430FR2311 TINA-TI Spice Model](#)
4. [MSP430 Temp Sense NTC Circuit Code Examples and SPICE Simulation File](#)

## Design Featured Op Amp

MSP430FRxx Smart Analog Combo		
	MSP430FR2311 SAC_L1	MSP430FR2355 SAC_L3
$V_{CC}$	2.0 V to 3.6 V	
$V_{CM}$	-0.1 V to $V_{CC} + 0.1$ V	
$V_{out}$	Rail-to-rail	
$V_{os}$	$\pm 5$ mV	
$A_{OL}$	100 dB	
$I_q$	350 $\mu$ A (high-speed mode)	
	120 $\mu$ A (low-power mode)	
$I_b$	50 pA	
UGBW	4 MHz (high-speed mode)	2.8 MHz (high-speed mode)
	1.4 MHz (low-power mode)	1 MHz (low-power mode)
SR	3 V/ $\mu$ s (high-speed mode)	
	1 V/ $\mu$ s (low-power mode)	
Number of channels	1	4
<a href="http://www.ti.com/product/MSP430FR2311">http://www.ti.com/product/MSP430FR2311</a>		
<a href="http://www.ti.com/product/MSP430FR2355">http://www.ti.com/product/MSP430FR2355</a>		

## Design Alternate Op Amp

MSP430FR2311 Transimpedance Amplifier	
$V_{CC}$	2.0 V to 3.6 V
$V_{CM}$	-0.1 V to $V_{CC}/2$ V
$V_{out}$	Rail-to-rail
$V_{os}$	$\pm 5$ mV
$A_{OL}$	100 dB
$I_q$	350 $\mu$ A (high-speed mode)
	120 $\mu$ A (low-power mode)
$I_b$	5 pA (TSSOP-16 with OA-dedicated pin input)
	50 pA (TSSOP-20 and VQFN-16)
UGBW	5 MHz (high-speed mode)
	1.8 MHz (low-power mode)
SR	4 V/ $\mu$ s (high-speed mode)
	1 V/ $\mu$ s (low-power mode)
Number of channels	1
<a href="http://www.ti.com/product/MSP430FR2311">http://www.ti.com/product/MSP430FR2311</a>	

<p>Low-noise and long-range PIR sensor conditioner circuit</p> 	<p>Bridge amplifier circuit</p> 	<p>Transimpedance amplifier circuit</p> 
<p>Single-supply, low-side, unidirectional current-sensing circuit</p> 	<p>High-side current sensing with discrete difference amplifier circuit</p> 	<p>Low-side, bidirectional current-sensing circuit</p> 
<p>Half-wave rectifier circuit</p> 	<p>Temperature sensing with NTC thermistor circuit</p> 	<p>Temperature sensing with PTC thermistor circuit</p> 

---

## Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

### Changes from October 19, 2019 to March 9, 2020

**Page**

- 
- Added *Related MSP430 Circuits* section..... 5
-

## IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to [TI's Terms of Sale](#) or other applicable terms available either on [ti.com](http://ti.com) or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265  
Copyright © 2022, Texas Instruments Incorporated