

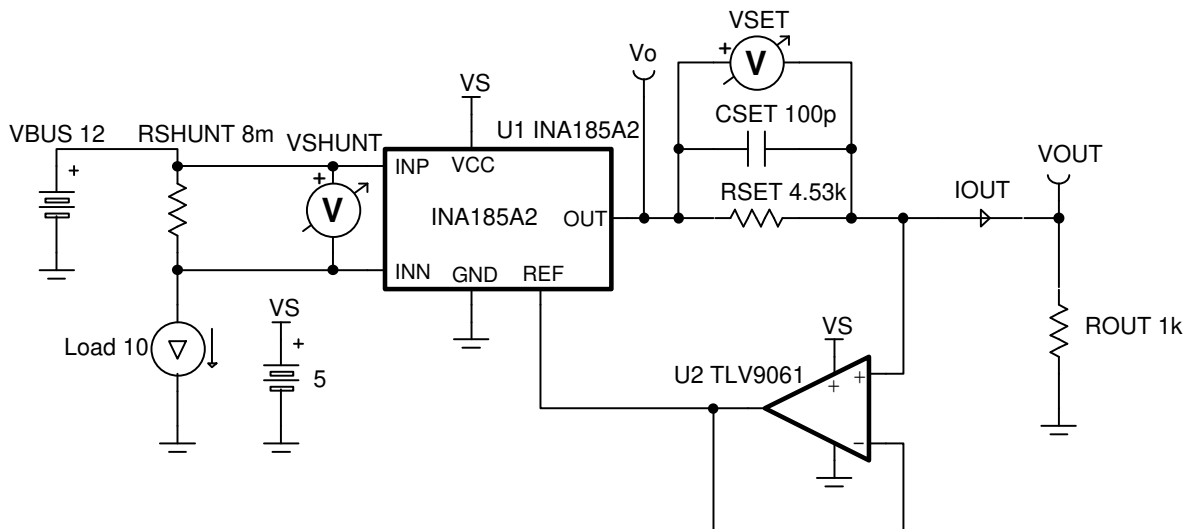
# Adjustable-gain, current-output, high-side current-sensing circuit



Input			Output			Error	Supply		
$I_{LOAD\ Min}$	$I_{LOAD\ Max}$	$V_{CM}$	$I_{OUT\ Min}$	$I_{OUT\ Max}$	Bandwidth	at $I_{LOAD\ Min}$	$I_{Q\ Max}$	$V_S$	$V_{ee}$
1A	10A	12V	88.3 $\mu$ A	883 $\mu$ A	200kHz	2.2% maximum, 0.3% typical	260 + 750 $\mu$ A	5V	GND (0V)

## Design Description

This circuit demonstrates how to convert a voltage-output, current-sense amplifier (CSA) into a current-output circuit using an operational amplifier (op amp) and a current-setting resistor ( $R_{SET}$ ). Taking advantage of the matched internal resistor gain network of the current-sense amplifier, this circuit utilizes the Howland Current Pump method to create a current source that is proportional to the sense current. The overall circuit gain is adjustable by changing the load resistor value ( $R_{OUT}$ ). Additionally, multiple circuits can be summed together to determine total current from multiple sources.



## Design Notes

1. The [Getting Started with Current Sense Amplifiers](#) video series introduces implementation, error sources, and advanced topics for using current sense amplifiers.
2. Choose precision 0.1% resistors to limit gain error at higher currents.
3. The output current ( $I_{OUT}$ ) is sourced from the VS supply, which adds to the  $I_Q$  of the current sense amplifier.
4. Use the  $V_{OUT}$  versus  $I_{OUT}$  curve ("claw-curve") of the CSA (U1) to set the  $I_{OUT}$  limit during  $I_{LOAD\_MAX}$ . If a higher amount of current is needed, then consider adding a buffer to the output of the current sense amplifier. A buffer on the output allows for smaller  $R_{OUT}$ .
5. For applications with higher bus voltages, simply substitute in a bidirectional current sense amplifier with a higher rated input voltage.
6. The  $V_{OUT}$  voltage is the input common-mode voltage ( $V_{CM}$ ) for the op amp.
7. Offset errors can be calibrated out with one-point calibration given that a known sense current is applied and the circuit is operating in the linear region. Gain error calibration requires a two-point calibration.
8. Include a small feed-forward capacitor ( $C_{SET}$ ) to increase BW and decrease  $V_{OUT}$  settling time to a step response in current. Increasing  $C_{SET}$  too much introduces gain peaking in the system gain curve, which results in output overshoot to a step response.
9. Multiple circuits can sum their current outputs into a single load resistor, but note that the headroom voltage for each individual circuit will decrease. The INA2181 and INA4181 devices are multi-channel CSAs that have similar performance to the INA185 device.
10. Follow best practices for printed-circuit board (PCB) layout according to the data sheet: decoupling capacitor close to the VS pin, routing the input traces for IN+ and IN- as a differential pair, and so forth.

## Design Steps

1. To satisfy system requirements, the minimum shunt ( $V_{SHUNT\_MIN}$ ) voltage value must be sufficiently greater than the known offsets of the amplifiers. Here is the equation for the worst-case maximum output current:

$$I_{OUT\_MAX\_Worst-Case} = \frac{V_{SET\_MAX}}{R_{SET} \cdot (1 - \text{Tolerance}_{Rset})}$$

$$I_{OUT\_MAX\_Worst-Case} = \frac{\text{Gain}_{INA185} \cdot (1 + \text{GainError}) \cdot [V_{SHUNT\_MIN} + V_{OS\_INA185}] + V_{OS\_TLV9061}}{R_{SET} \cdot (1 - \text{Tolerance}_{Rset})}$$

2. Since offset errors dominate at the low currents, negate resistor tolerance and gain error for establishing  $V_{SHUNT\_MIN}$ . Set the error of  $V_{SET}$  to 2.2% to determine the following condition:

$$V_{SHUNT\_MIN} > \left( \frac{1}{2.2\%} \right) \cdot \left\{ V_{OS\_INA185} + \frac{V_{OS\_TLV9061}}{\text{Gain}_{INA185}} \right\}$$

3.  $V_{OUT\_MIN}$  also needs to be large enough so the common-mode voltage ( $V_{CM}$ ) and output voltage ( $V_{OUT\_TLV9061}$ ) of the TLV9061 device are in the optimal operating region. The TLV9061 device is a rail-to-rail-input-output (RRIO) op amp so it can operate with very small  $V_{CM}$  and output voltages, but  $A_{OL}$  will vary. Testing conditions for data sheet CMRR and  $A_{OL}$  show that choosing  $V_{OUT\_MIN} > 50$  mV will provide sufficient  $A_{OL}$  when circuit sensing minimum load current.

$$V_{OUT\_TLV9061} = V_{CM\_TLV9061} = V_{OUT}$$

$$V_{OUT\_MIN} > 50\text{mV for good TLV9061 } A_{OL}$$

4. The scaling of  $R_{OUT}$  and  $R_{SET}$  can be determined by setting three parameters:  $V_{O\_MAX}$ ,  $I_{OUT\_MAX}$ , and  $R_{OUT}$ . It is critical that  $I_{OUT\_MAX}$  does not exceed the driving capability of the CSA or else  $V_{O\_MAX}$  will droop and the circuit will lose headroom voltage. Use the swing-to-rail specification and the  $V_{OUT}$  versus  $I_{OUT}$  data sheet curve to determine optimal values.
  - a. Choose  $V_{O\_MAX} = 4.9\text{V}$
  - b. Choose  $I_{OUT\_MAX} = 900\mu\text{A}$

c. Choose  $R_{OUT} = 1k\Omega$

5. Using the system of equations for  $V_{OUT}$ , solve for  $R_{SET}$ . Choose the closest larger 1% resistor value. Note that rounding up the  $R_{SET}$  value will decrease the  $I_{OUT\_MAX}$  from initially chosen  $900\mu A$ .

$$V_{SET\_MAX} = I_{OUT\_MAX} \cdot R_{SET}$$

$$V_{OUT\_MAX} = I_{OUT\_MAX} \cdot R_{OUT}$$

$$V_{OUT\_MAX} = V_{O\_MAX} - V_{SET\_MAX}$$

$$R_{SET} = \frac{V_{O\_MAX} - I_{OUT\_MAX} \cdot R_{OUT}}{I_{OUT\_MAX}} = 4444.3\Omega$$

$$R_{SET} = 4530\Omega, 1\%$$

6. Now choose an INA185 gain variant and solve for  $R_{SHUNT}$ . Choose a 1% resistor value. Note that  $R_{SET}$  is independent of gain and  $R_{SHUNT}$  can be calculated for each gain variant.

$$V_{OUT\_MAX} = I_{OUT\_MAX} \cdot R_{OUT} = 900mV$$

$$V_{SET\_MAX} = V_{O\_MAX} - V_{OUT\_MAX} = 4V$$

$$V_{IN\_MAX} = \frac{V_{SET\_MAX}}{\text{Gain}_{INA185A2}} = \frac{4V}{50 \frac{V}{V}} = 80mV$$

$$R_{SHUNT} = \frac{V_{IN\_MAX}}{I_{LOAD\_MAX}} = \frac{80mV}{10A}$$

$$R_{SHUNT} = 8m\Omega$$

7. Now check if  $V_{OUT\_MIN}$  and  $V_{SHUNT\_MIN}$  are large enough to achieve 2% error at 1A with updated values. Use the maximum offset specifications of the devices when calculating error.

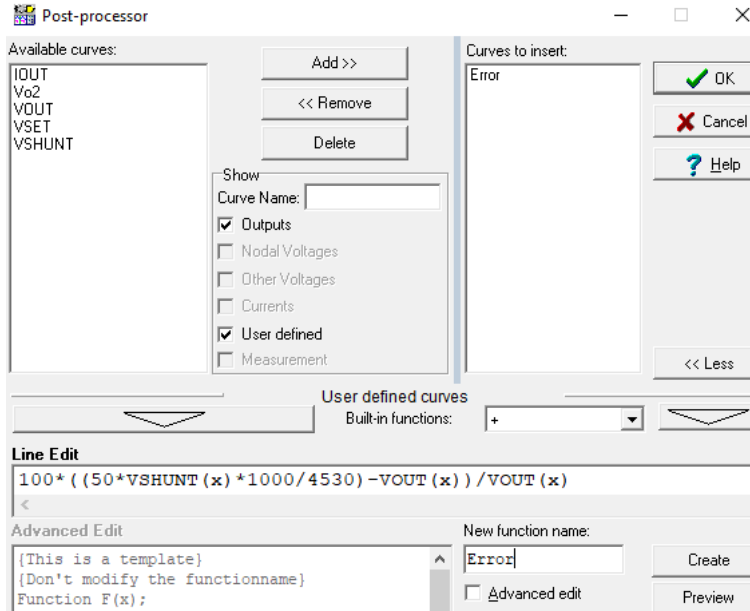
$$V_{SHUNT\_MIN} > \left( \frac{1}{2.2\%} \right) \cdot \left\{ V_{OS\_INA185A2} + \frac{V_{OS\_TLV9061}}{\text{GAIN}_{INA185A2}} \right\} = 45.45 \cdot \left\{ 130\mu V + \frac{2mV}{50 \frac{V}{V}} \right\} = 7.73mV$$

$$V_{SHUNT\_MIN} = 1A \cdot 8m\Omega = 8mV > 7.73mV$$

$$V_{OUT\_MIN} = V_{SHUNT\_MIN} \cdot \text{Gain}_{INA185A2} \cdot \frac{R_{OUT}}{R_{SET}}$$

$$V_{OUT\_MIN} = 8mV \cdot 50 \frac{V}{V} \cdot \frac{1k\Omega}{4.53k\Omega} = 88mV > 50mV$$

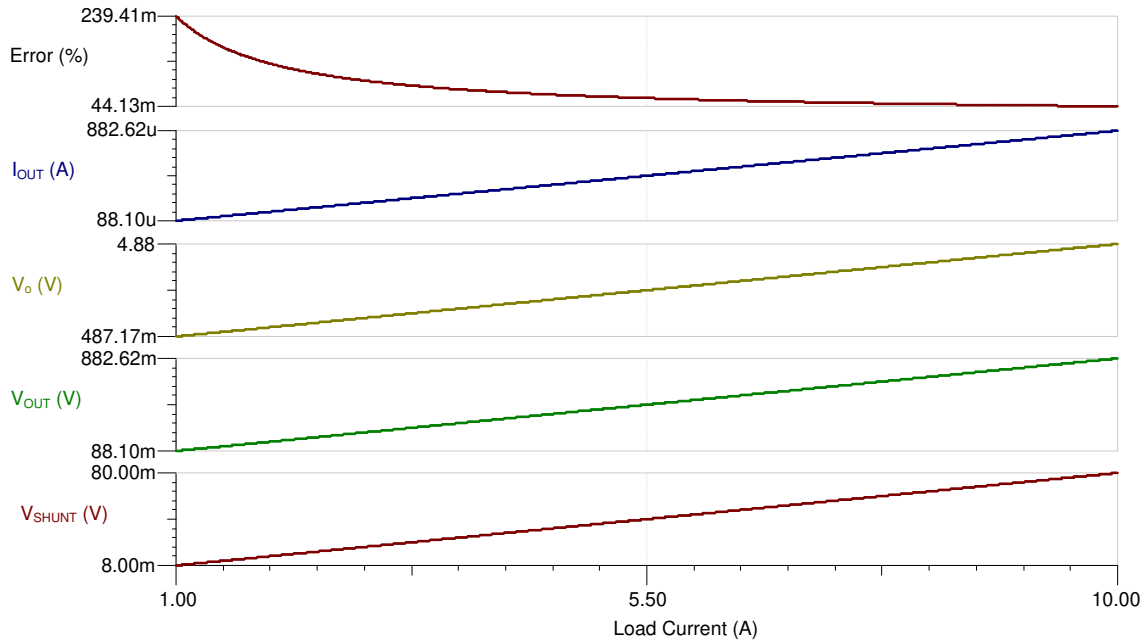
8. Run a simulation in TINA-TI software using available models. Note that these models use typical specifications. Calculate *Error* in the TINA-TI *Post-processor* window.



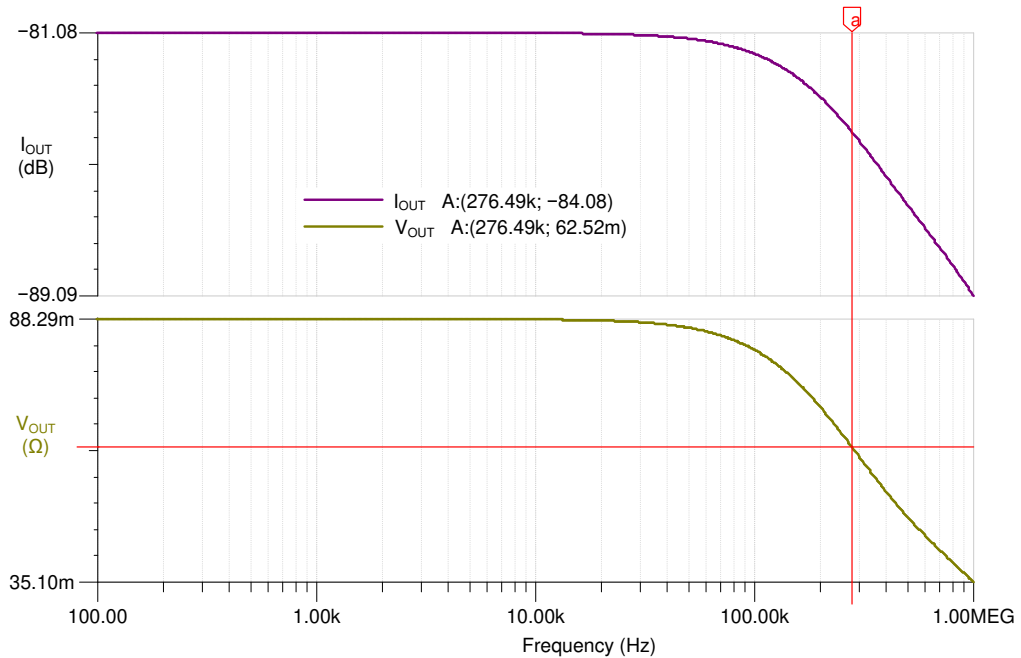
## Design Simulations

### DC Simulation Results

The following graph shows a linear output response for load currents from 1A to 10A.



### AC Simulation Result – $I_{LOAD}$ to $I_{OUT}$ ( $V_{OUT}$ ) circuit gain



## Design References

See [Analog Engineer's Circuit Cookbooks](#) for TI's comprehensive circuit library.

See the circuit SPICE simulation file [SBOMA16](#).

## Getting Started with Current Sense Amplifiers video series

<https://training.ti.com/getting-started-current-sense-amplifiers>

## Current Sense Amplifiers on TI.com

<http://www.ti.com/amplifier-circuit/current-sense/products.html>

## Comprehensive Study of the Howland Current Pump

<http://www.ti.com/analog/docs/litabsmultiplefilelist.tsp?literatureNumber=snoa474a&docCategoryId=1&familyId=78>

For direct support from TI Engineers use the E2E community

<http://e2e.ti.com>

## Design Featured Current Sense Amplifier

INA185A2	
$V_S$	2.7V to 5.5V (operational)
$V_{CM}$	0V to 26V
Swing to $V_S$ ( $V_{SP}$ )	$V_S - 0.02V$
$V_{OS}$	$\pm 25\mu V$ to $\pm 130\mu V$ at 12V $V_{CM}$
$I_Q$	200 $\mu A$ to 260 $\mu A$
$I_B$	75 $\mu A$ at 12V
BW	210kHz at 50V/V (A2 gain variant)
# of channels	1
Body size (including pins)	1.60 mm $\times$ 1.60 mm
<a href="http://www.ti.com/product/ina185">http://www.ti.com/product/ina185</a>	

## Design Featured Operational Amplifier

TLV9061 (TLV9061S is shutdown version)	
$V_S$	1.8V to 5.5V
$V_{CM}$	$(V-) - 0.1V < V_{CM} < (V+) + 0.1V$
CMRR	103dB
$A_{OL}$	130dB
$V_{OS}$	$\pm 1.6mV$ maximum
$I_Q$	750 $\mu A$ maximum
$I_B$ (input bias current)	$\pm 0.5pA$
GBP (gain bandwidth product)	10MHz
# of channels	1 (2 and 4 channel packages available)
Body size (including pins)	0.80 mm $\times$ 0.80 mm
<a href="http://www.ti.com/product/tlv9061">http://www.ti.com/product/tlv9061</a>	

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