

TI Designs: TIDA-01534

車載用オフ・バッテリ、デュアル・フェーズ昇圧コンバータのリファレンス・デザイン



概要

このリファレンス・デザインは大電力、広い入力電圧範囲(公称9V～20V、過渡は最低6V、最高36V)で、同期整流昇圧コントローラをデュアル・フェーズ構成で使用し、4つの切り替え可能な12Vレールを出力する回路です。これらの各レールは最大2.5Aを供給でき、診断機能が搭載されています。また、このリファレンス・デザインにはデュアル同期整流降圧コントローラも実装されており、2つの大電流、低電圧レール(公称5V、3Aおよび3.8V、6.5A)を生成します。このデザインは、車載用オフ・バッテリのインフォティメント・アプリケーションに適しています。

リソース

[TIDA-01534](#)

[LM74700-Q1](#)

[LM25122-Q1](#)

[LM5140-Q1](#)

[TPS1H100-Q1](#)

デザイン・フォルダ

プロダクト・フォルダ

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特長

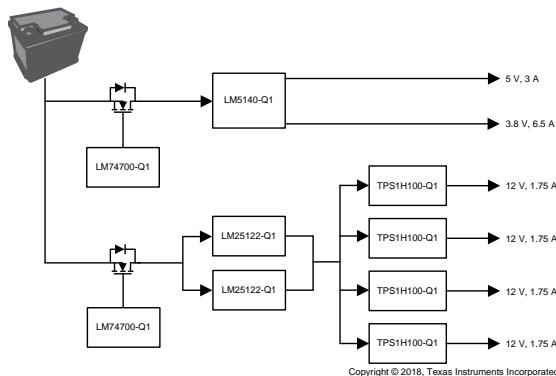
- 9V～20Vの広い入力電圧範囲、最低6V、最高36Vの過渡に対応
- デュアル・フェーズの大電流同期整流昇圧コントローラ構成
 - 診断機能を備えた4つの切り替え可能な12V出力
 - 各出力で1.75Aの公称電流
 - 標準的な動作条件で98%を超える効率
- デュアル同期整流降圧コントローラ
 - 公称5V、3A
 - 公称3.8V、6.5A
- ゼロ I_Q のスマート・ダイオード・コントローラによるバッテリ逆極性保護
- AMラジオ帯域の干渉を最小化

アプリケーション

- 車載用ヘッド・ユニット
- アフターマーケット・ヘッド・ユニット



E2Eエキスパートに質問





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1 System Description

The battery system of a vehicle normally supplies the power to end equipment in typical automotive infotainment applications. This reference design implements a circuit that converts a wide-input voltage to four 12-V outputs using a dual-phase synchronous boost circuit. This design also has a circuit that converts the input voltage to two lower voltages at 3.8 V and 5 V using a dual, synchronous buck circuit. The normal operating input voltage range is from 9 V to 20 V, and the design is able to handle transient voltages down to 6 V and up to 36 V. This design is a good fit for automotive head unit, aftermarket head unit, and voltage conditioning module (VCM) applications.

1.1 Key System Specifications

表 1. Key System Specifications

| PARAMETER | SPECIFICATIONS | DETAILS |
|------------------------------------|------------------------------|-----------------------|
| Input voltage range | 6-V to 36-V DC | 2.4.1 |
| Boost output voltage | 12.1 V | 2.4.2 |
| Boost output current (per channel) | 1.75 A | 2.4.2 |
| Boost supply switching frequency | 398 kHz | 2.4.2 |
| Buck output 1 voltage | 5 V ± 1% | 2.4.3 |
| Buck output 1 current | 3 A | 2.4.3 |
| Buck output 2 voltage | 3.8 V ± 1% | 2.4.3 |
| Buck output 2 current | 6.5 A | 2.4.3 |
| Buck supply switching frequency | 440 kHz (default) or 2.2 MHz | 2.4.3 |

2 System Overview

2.1 Block Diagram

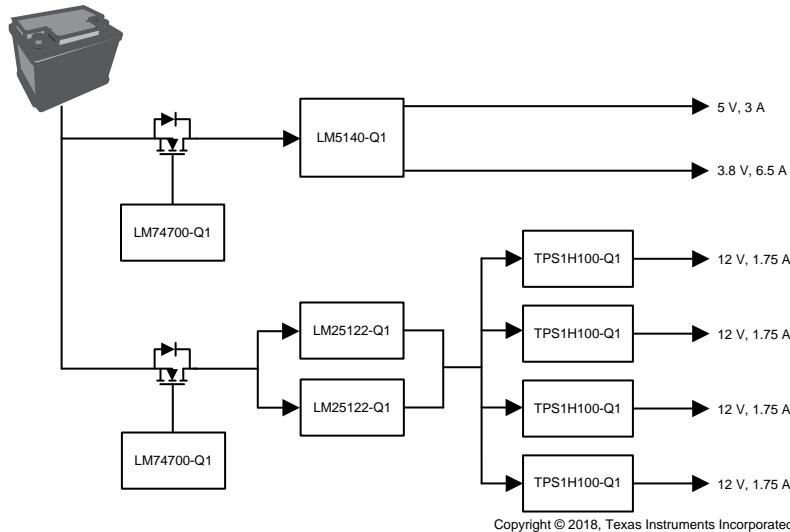


図 1. TIDA-01534 Block Diagram

2.2 Design Considerations

Some of the design considerations for off-battery, infotainment-end-equipment applications are:

- Wide-input voltage range
- Reverse battery condition
- Low-loss and high efficiency
- AM radio band electromagnetic interference (EMI)

The devices in this reference design have a wide supply input range that can accommodate the transient conditions in an off-battery application.

Protection from reverse battery conditions, which are typically caused by an incorrect installation or a jump-start connection, is mandatory. Low-loss and high efficient solutions are important, especially in high-current applications. This design utilizes two protection circuits in parallel to further reduce power loss.

Radio band EMI (especially in the AM band) must be minimized in infotainment end equipment. Using power supplies that have switching frequencies outside of the AM band, as well as the capability to operate in out-of-phase mode, helps achieve this objective.

2.3 Highlighted Products

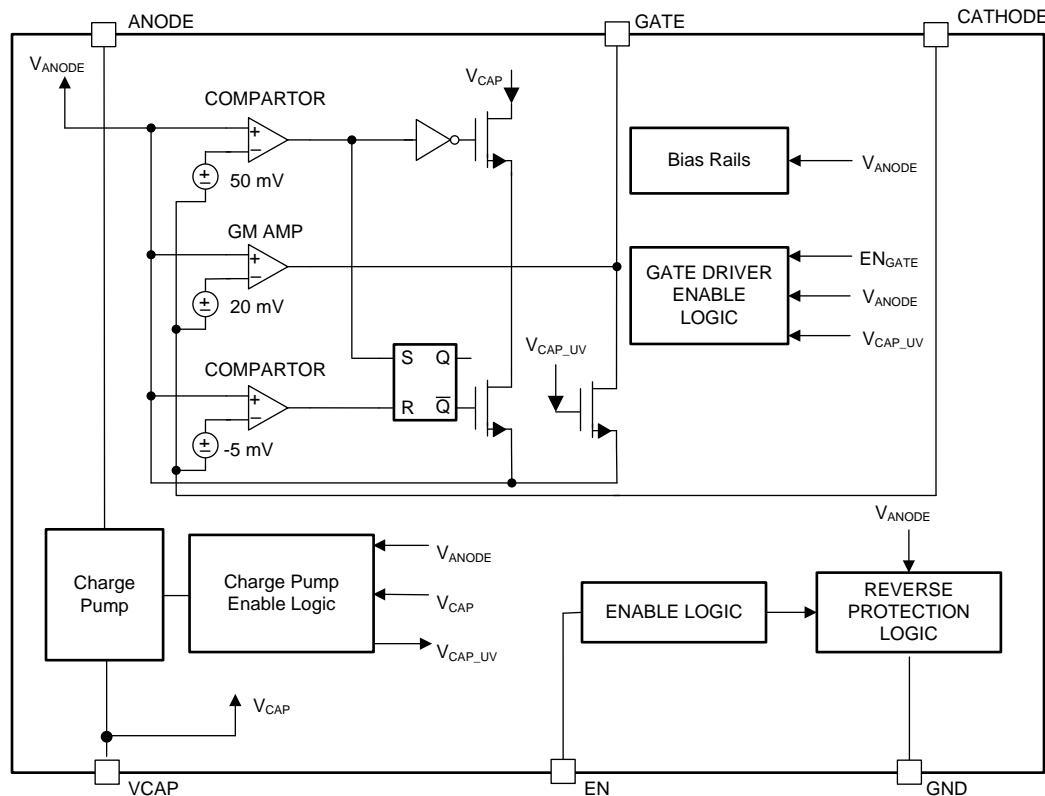
2.3.1 LM74700-Q1

The LM74700-Q1 is a smart diode controller that operates in conjunction with an external N-channel MOSFET to function as an ideal diode rectifier for low-loss reverse polarity protection. The wide supply input range of 3 V to 65 V allows control of many popular DC bus voltages. The device can withstand and protect the loads from negative supply voltages down to -65 V. With a low $R_{DS(ON)}$ external N-channel MOSFET, a very-low forward voltage drop can be achieved while minimizing the amount of power dissipated in the MOSFET.

For low-load currents, the forward voltage is regulated to 20 mV to enable graceful shutdown of the MOSFET. TI recommends external N-channel MOSFETs with a 5 V or lower threshold voltage. With the enable pin low, the controller is off and draws approximately 3 μ A of current.

The LM74700-Q1 controller provides a charge pump gate drive for an external N-channel MOSFET. The high voltage rating of the LM74700-Q1 helps to simplify the system designs for automotive ISO 7637 protection. Fast response to reverse current blocking makes the device suitable for systems with output voltage holdup requirements during ISO 7637 pulse testing, as well as power fail and brownout conditions. The LM74700-Q1 is also suitable for ORing applications or AC rectification.

図 2 shows the LM74700-Q1 functional block diagram.



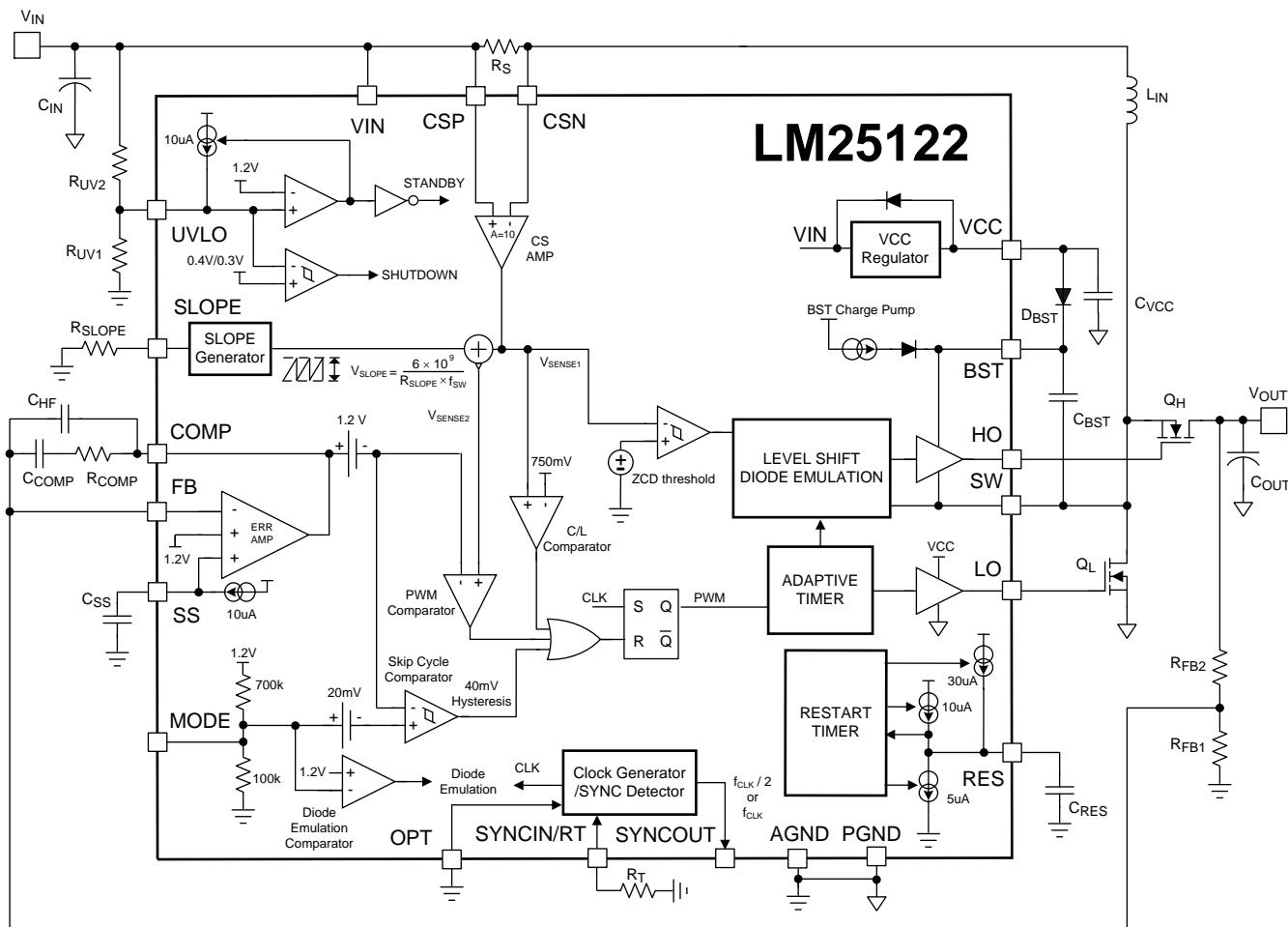
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図 2. LM74700-Q1 Functional Block Diagram

2.3.2 LM25122-Q1

The LM25122-Q1 is a multiphase-capable synchronous boost controller intended for high-efficiency synchronous boost regulator applications. The control method is based on peak current mode control. Current mode control provides inherent line feedforward, cycle-by-cycle current limiting, and ease-of-loop compensation.

The switching frequency is programmable up to 600 kHz. Higher efficiency is achieved by two robust N-channel MOSFET gate drivers with adaptive deadtime control. A user-selectable diode emulation mode also enables discontinuous mode operation for improved efficiency at light load conditions.



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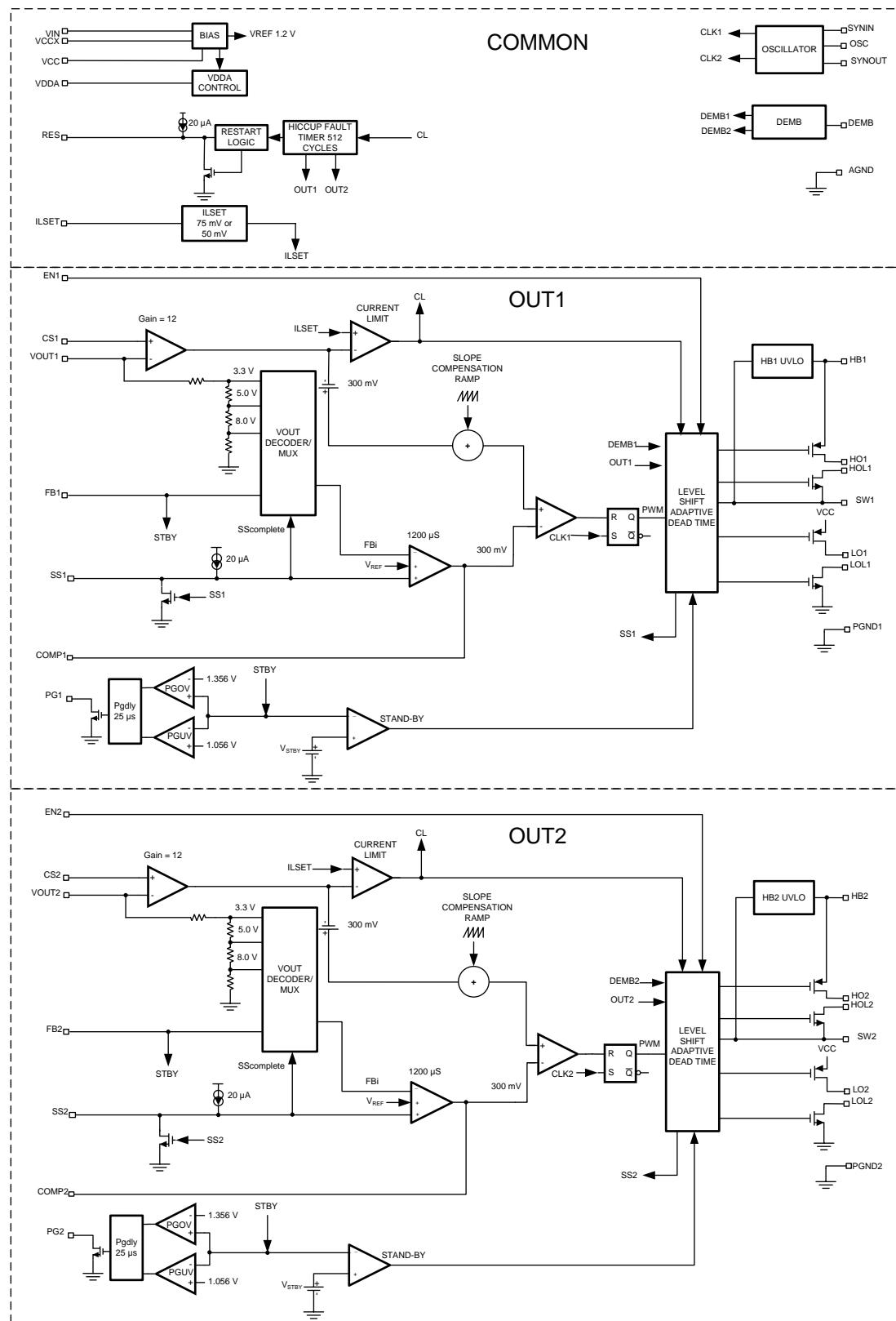
図 3. LM25122-Q1 Functional Block Diagram

2.3.3 LM5140-Q1

The LM5140-Q1 is a dual synchronous buck controller intended for high voltage wide VIN step-down converter applications. The control method is based on current mode control. Current mode control provides inherent line feedforward, cycle-by-cycle current limiting, and easier loop compensation.

The LM5140-Q1 features adjustable slew rate control to simplify compliance with the CISPR and automotive EMI requirements. The LM5140-Q1 operates at selectable switching frequencies of 2.2 MHz or 440 kHz, with the two controller channels switching 180° out of phase. In light or no-load conditions, the LM5140-Q1 operates in skip cycle mode for improved low power efficiency. The LM5140-Q1 includes a high voltage bias regulator with automatic switch-over to an external bias supply, to improve efficiency and reduce input current.

Additional features include frequency synchronization, cycle-by-cycle current limit, hiccup mode fault protection for sustained overloads, independent power good outputs, and independent enable inputs.


図 4. LM5140-Q1 Functional Block Diagram

2.3.4 TPS1H100-Q1

The TPS1H100-Q1 is a high-side power switch that is fully protected and single channel, with integrated NMOS power FET and charge pump. Full diagnostics and high-accuracy current sense features enable intelligent control of the load. Programmable current limit function greatly improves the reliability of the entire system. The device diagnostic reporting has two versions to support both digital status and analog current sense output, both of which can be set as high impedance when diagnostics are disabled, for multiplexing the MCU analog or digital interface among devices.

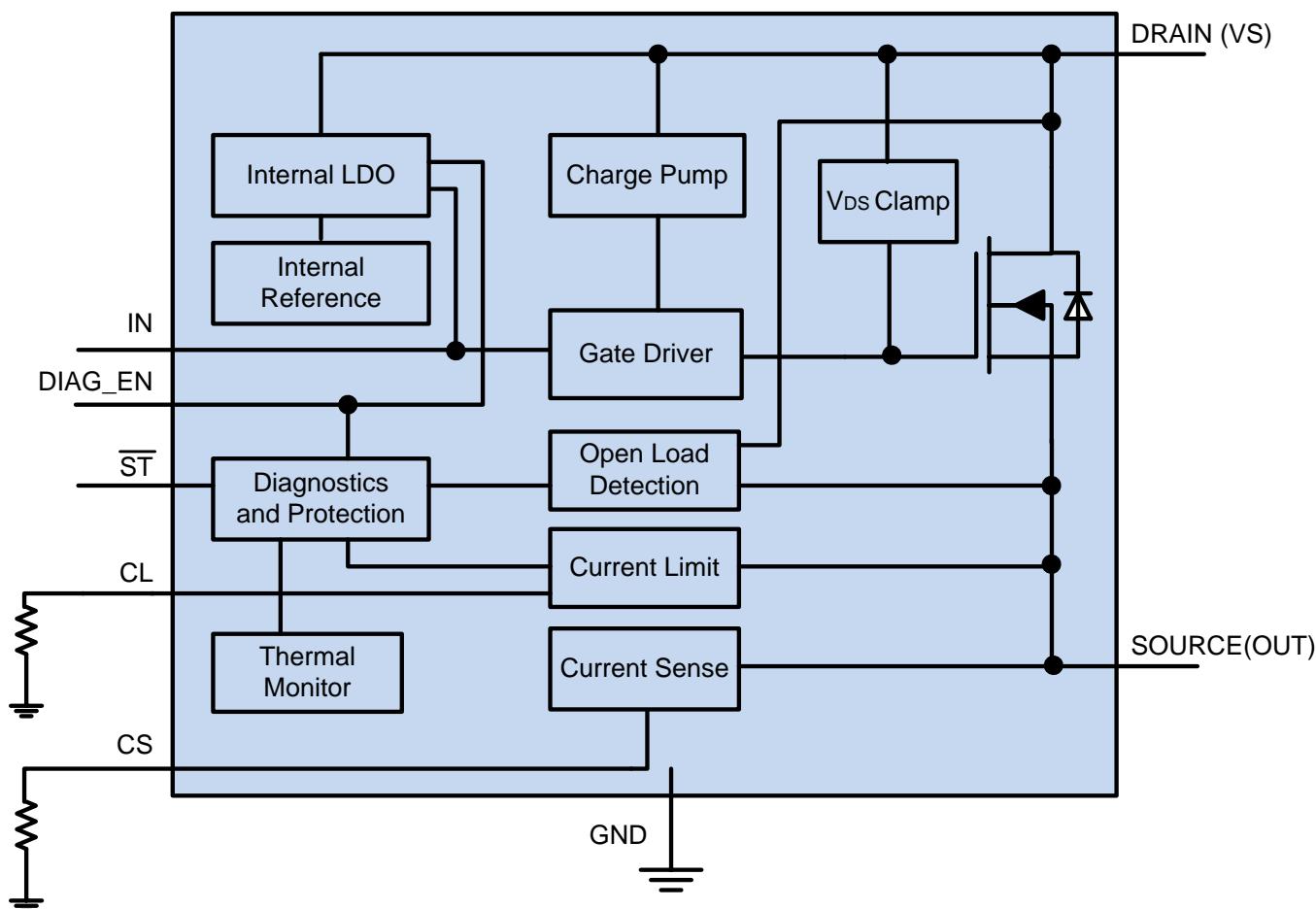


図 5. TPS1H100-Q1 Functional Block Diagram

2.4 System Design Theory

2.4.1 Input Protection

The LM74700-Q1 smart diode controller is used to protect the circuit from reverse battery condition. The very low $R_{DS(ON)}$ of the n-channel MOSFET helps reduce power loss, especially during high-current operation. By using two separate input paths, the resistance is reduced to improve overall power loss of the system.

2.4.2 Boost Voltage Supply Controllers (LM25122-Q1)

Two LM25122-Q1s are used to provide high current output for the boost voltage to supply up to 2.5 A for each of the four downstream systems. To help reduce EMI, the two devices are designed to operate in dual phase interleaved operation, with outputs 180° out of phase from each other. U100 is set as the master device with SYNCOUT connecting to SYNCIN of the slave device (U101). 図 6 shows the connections between a master device and a slave device.

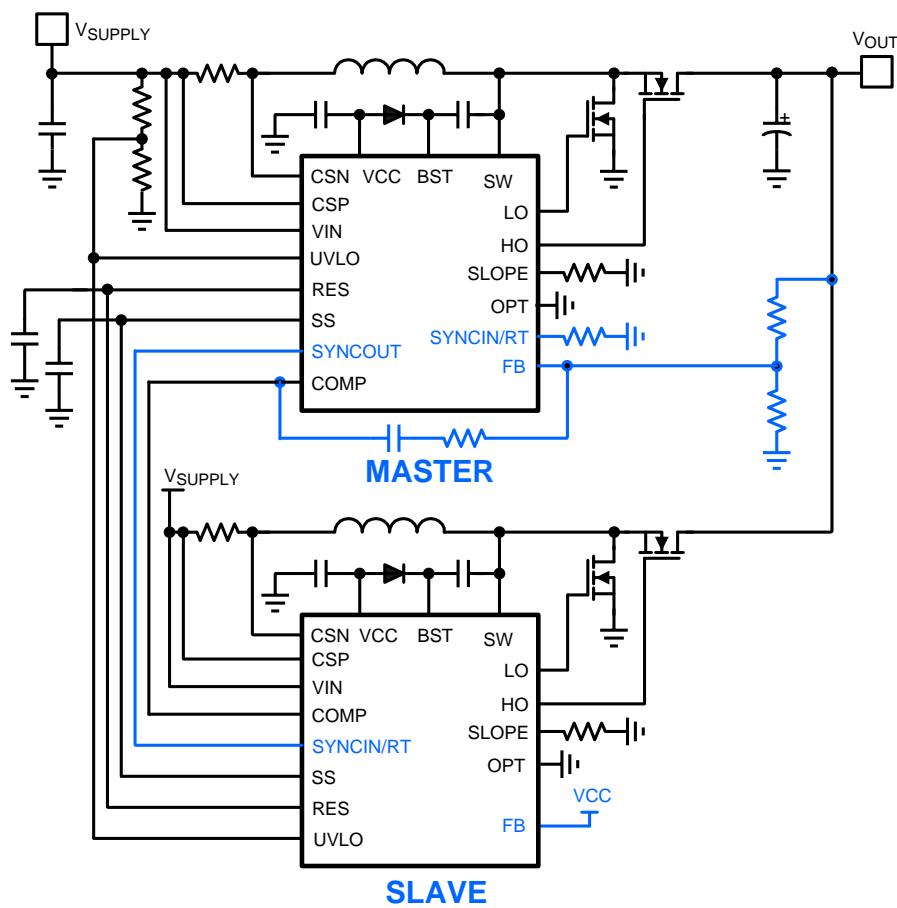


図 6. LM25122-Q1 Dual-Phase Interleaved Boost Configuration

To avoid the AM radio band, the SYNCIN/RT pin of U100 is used to set the switching frequency to 398 kHz with resistor R115:

$$f_{SW} = \frac{9 \times 10^9}{R115} = \frac{9 \times 10^9}{22.6 \text{ k}} = 398 \text{ kHz} \quad (1)$$

The output voltage is set to 12.1 V with feedback resistors R102, R112, and R117 to the master device (U100):

$$V_{\text{OUT}} \text{ (12V_Boosted)} = \frac{51\Omega + 90.9\text{ k}\Omega}{10\text{ k}\Omega} + 1 \times 1.2\text{ V} = 12.1\text{ V} \quad (2)$$

Resistor R102 is used to facilitate measurement of loop transfer function of the power supply. For more information, see [AN-1889 How to Measure the Loop Transfer Function of Power Supplies](#).

When the input voltage is equal to or greater than the set output voltage (12.1 V), the LM25122-Q1s are in 100% duty cycle operation for the high-side synchronous switch (bypass operation); thus the output voltage is equal to the input voltage.

2.4.3 Buck Voltage Supply Controller (LM5140-Q1)

The LM5140-Q1 generates 5-V and 3.8-V output rails from the battery source. Pin 3 (FB2) is connected to feedback resistors R28, R33, and R37 for 5-V output. Pin 28 (FB1) is connected to feedback resistors R26, R29, and R34 for 3.8-V output. The two outputs switch 180° out of phase to each other to help reduce EMI.

$$V_{\text{OUT}} \text{ (5V0)} = \frac{51\Omega + 31.6\text{ k}\Omega}{10\text{ k}\Omega} + 1 \times 1.2\text{ V} = 5\text{ V} \quad (3)$$

$$V_{\text{OUT}} \text{ (3V8)} = \frac{165\Omega + 21.5\text{ k}\Omega}{10\text{ k}\Omega} + 1 \times 1.2\text{ V} = 3.8\text{ V} \quad (4)$$

To avoid the AM radio band, switching frequency is set to 440 kHz by grounding pin 37 (OSC) through a 0-Ω resistor (R39).

3 Hardware, Testing Requirements, and Test Results

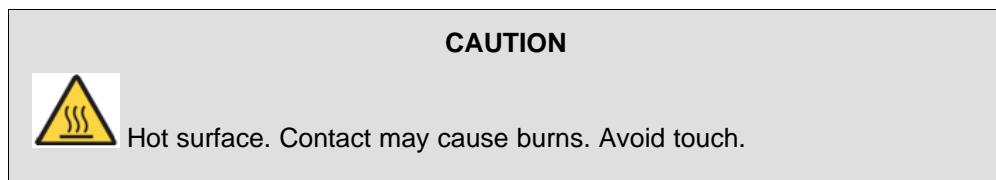
3.1 Required Hardware

The hardware for this design is as follows:

- Agilent 1000-W power supply or other comparable power supply
- Thermal imager for temperature measurements
- Oscilloscope for signal measurements
- Variable loads
- Frequency Response Analyzer (Venable 3120)

3.2 Testing and Results

3.2.1 Test Setup

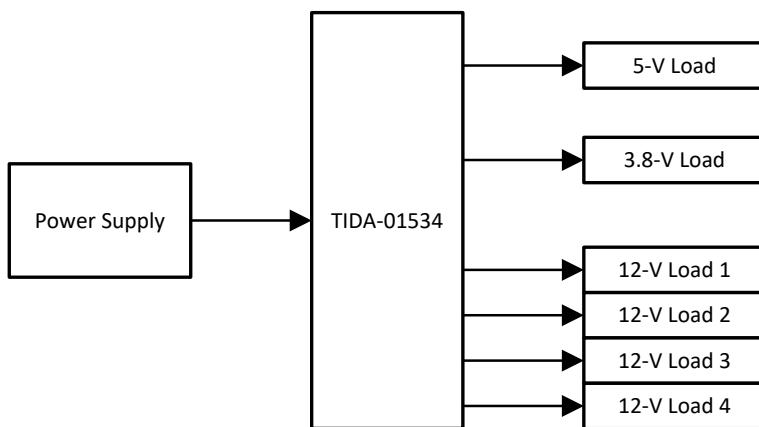


Connect proper variable loads to outputs for desired loading base on specific test

Connect power supply to PCB inputs (J1: V_{IN}, J2: GND)

For boost outputs, install shunt between pins 1 and 2 of corresponding header to enable, or between pins 2 and 3 to disable:

- J200 header for J201 output
- J202 header for J203 output
- J204 header for J205 output
- J206 header for J207 output



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図 7. Test Setup Block Diagram

3.2.2 Test Results

3.2.2.1 Start-up Waveforms

The following three figures show captures of input and outputs during start-up with various input voltages.

- Channel 1, 2 V/div (yellow): V_{IN} source input
- Channel 2, 2 V/div (magenta): 12-V boost output
- Channel 3, 1 V/div (cyan): 3.8-V buck output
- Channel 4, 1 V/div (green): 5-V buck output

図 8 shows start-up waveforms with source input voltage (V_{IN}) at 9 V.

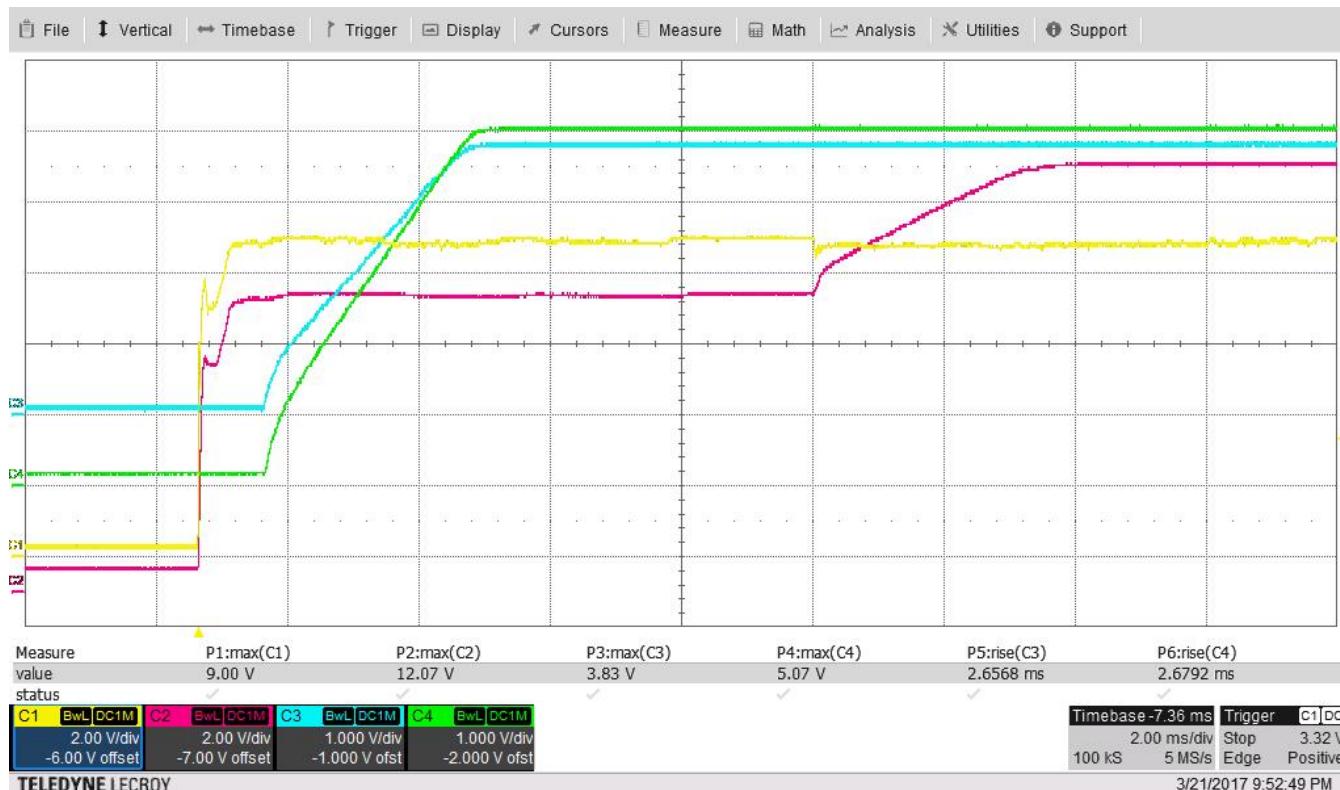


図 8. Start-up With Input at 9 V

図 9 和 図 10 show start-up waveforms without soft-start at the boost with source input voltage (V_{IN}) at 6 V and at 9 V, respectively.

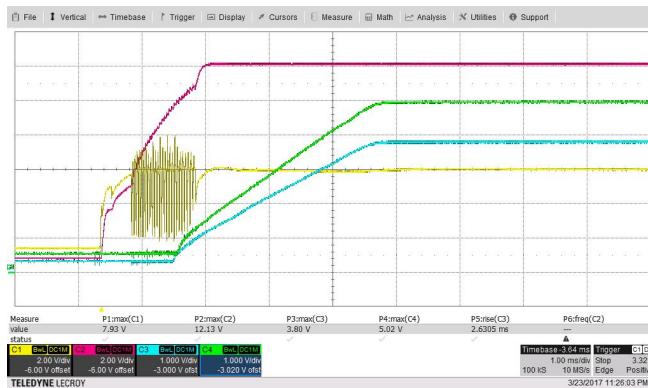


図 9. Start-up Without Boost Soft-Start With Input at 6 V

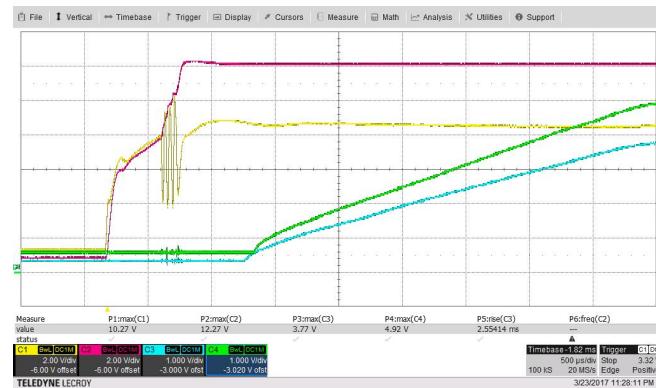


図 10. Start-up Without Boost Soft-Start With Input at 9 V

図 11 和 図 12 show the in-rush current during start-up without soft-start at the boost with source input voltage (V_{IN}) at 9 V and at 15 V, respectively.

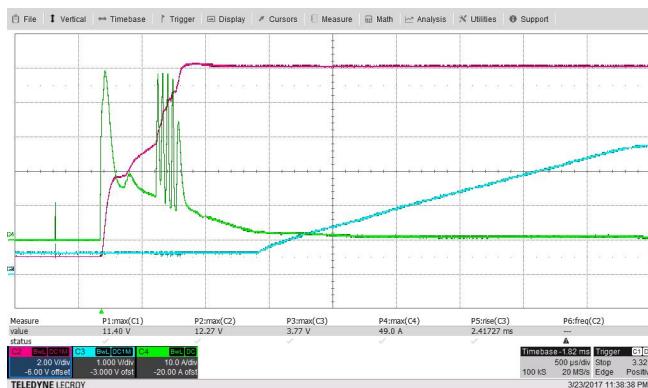


図 11. In-rush Current During Start-Up Without Boost Soft-Start With Input at 9 V

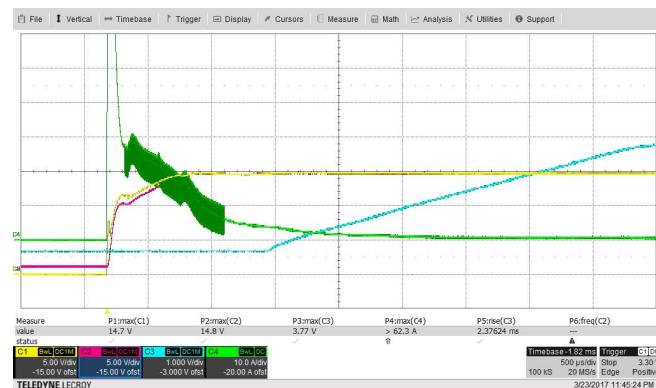


図 12. In-rush Current During Start-up Without Boost Soft-Start With Input at 15 V

3.2.2.2 Output Switch Nodes Waveforms

The following figures show the waveforms at the switch nodes at different levels of input voltage.

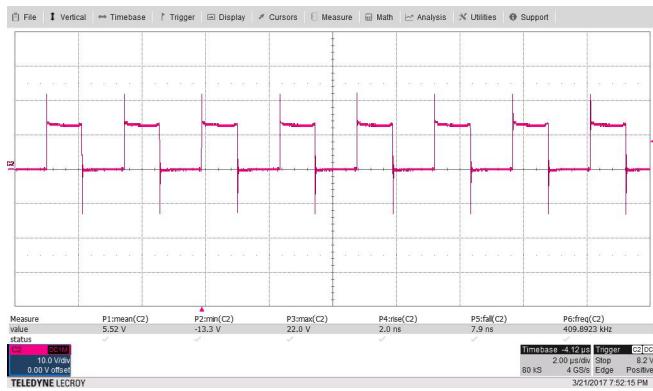


図 13. Boost 12-V Output Switch Node 1 (TP101) With Input at 6 V

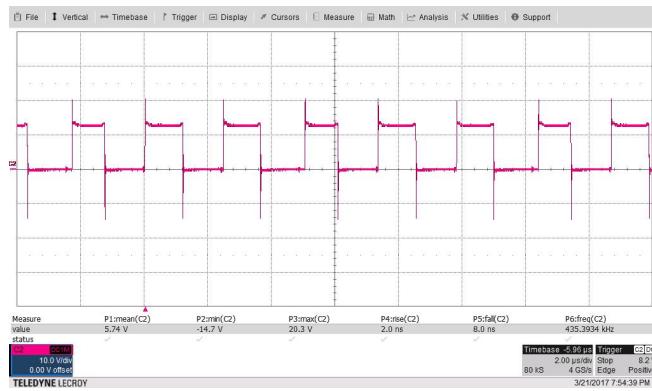


図 14. Boost 12-V Output Switch Node 2 (TP105) With Input at 6 V



図 15. Boost 12-V Output Switch Node 1 (TP101) With Input at 9 V

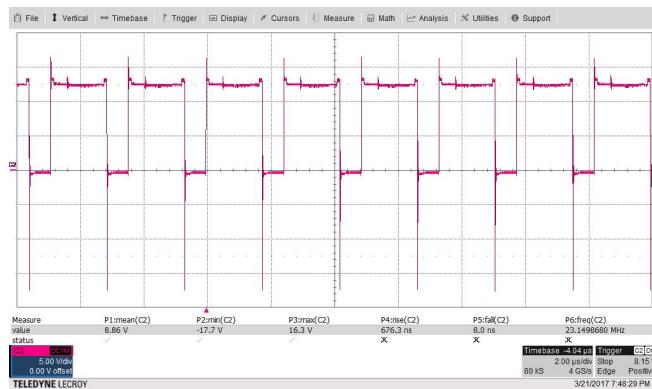


図 16. Boost 12-V Output Switch Node 2 (TP105) With Input at 9 V



図 17. Buck 5-V Output Switch Node (TP5) With Input at 36 V and Output Current at 8 A



図 18. Buck 3.8-V Output Switch Node (TP4) With Input at 36 V and Output Current at 10 A

3.2.2.3 Output Ripple and Dynamic Load-step Waveforms

The following figures show the boost output ripple and response to dynamic current 50% load-step from 5-A half load to 10-A full load at different levels of input voltage.

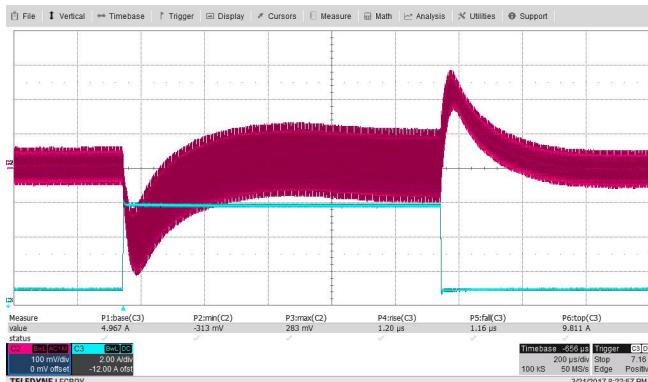


図 19. Boost 12-V Output With Load-Step From 5 A to 10 A With Input at 9 V

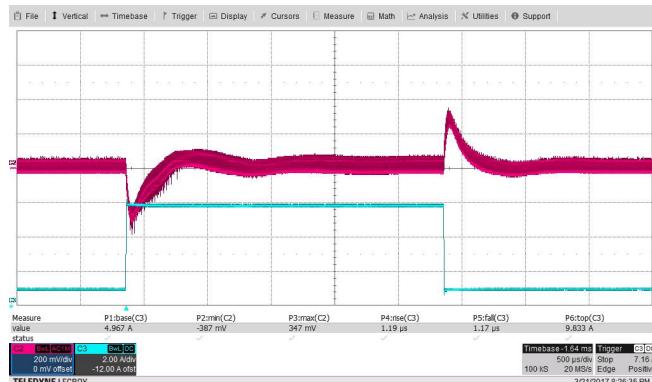


図 20. Boost 12-V Output With Load-Step From 5 A to 10 A With Input at 7 V

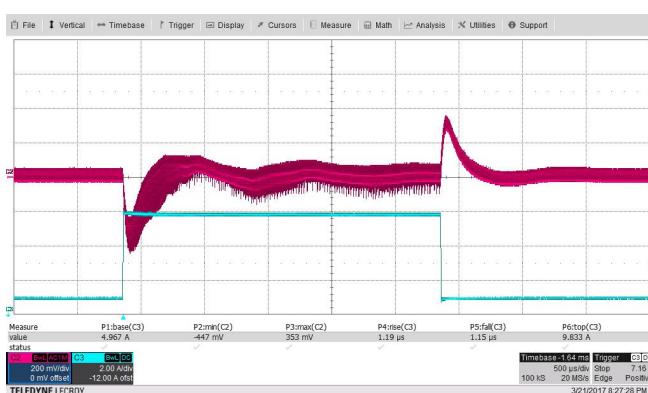


図 21. Boost 12-V Output With Load-Step From 5 A to 10 A With Input at 6.5 V

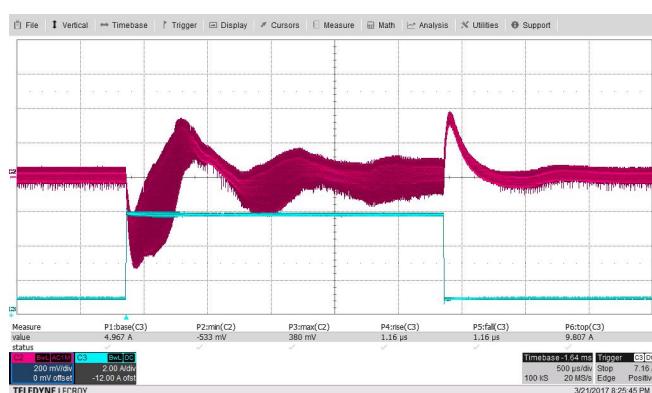


図 22. Boost 12-V Output With Load-Step From 5 A to 10 A With Input at 6 V

The following figures show the buck output ripple and response to dynamic current load-step from 3 A to 8 A (for 5-V output), and from 5 A to 10 A (for 3.8-V output), at different levels of input voltage:



図 23. Buck 5-V Output With Load-Step From 3 A to 8 A With Input at 36 V



図 24. Buck 5-V Output With Load-Step From 3 A to 8 A With Input at 20 V

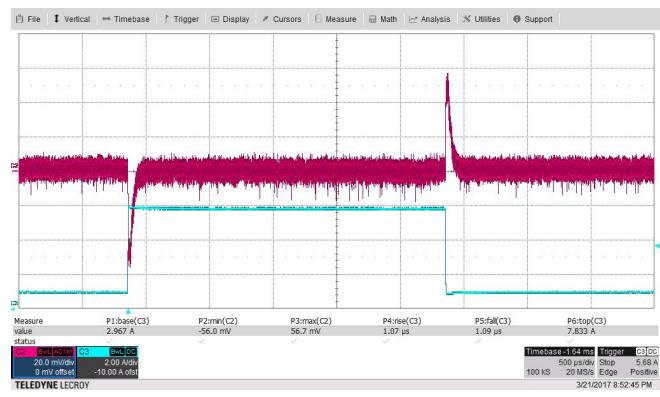


図 25. Buck 5-V Output With Load-Step From 3 A to 8 A With Input at 9 V

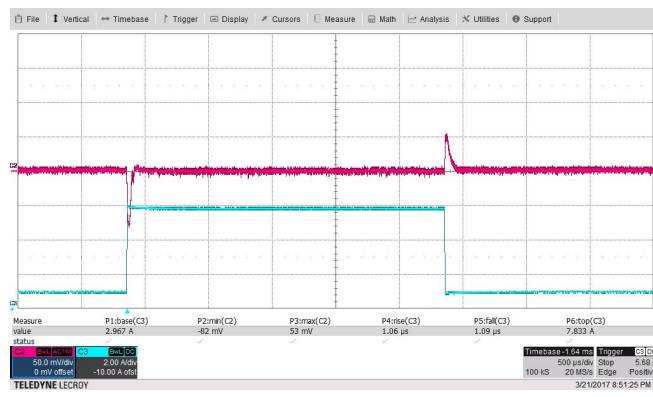


図 26. Buck 5-V Output With Load-Step From 3 A to 8 A With Input at 6.5 V

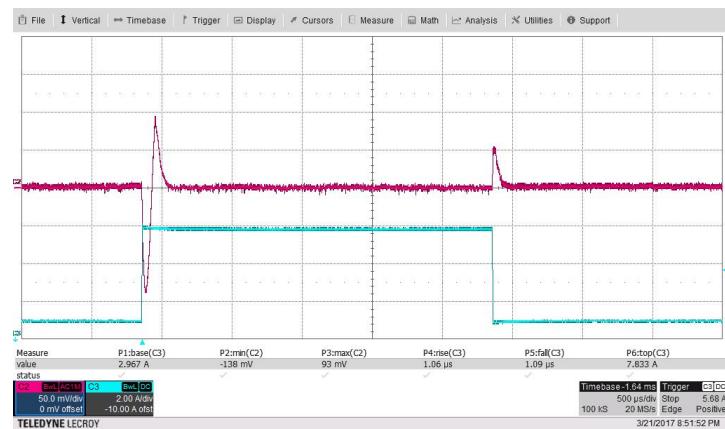


図 27. Buck 5-V Output With Load-Step From 3 A to 8 A With Input at 6 V

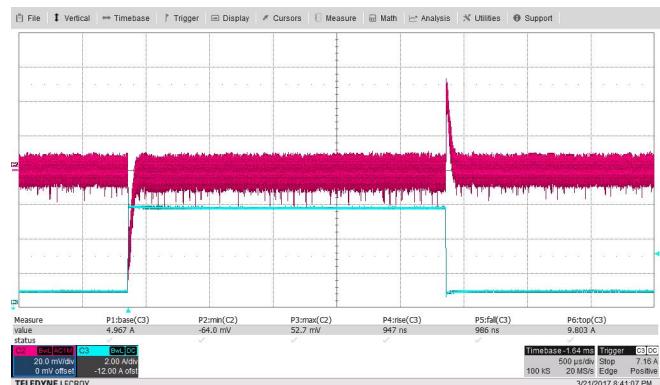


図 28. Buck 3.8-V Output With Load-Step From 5 A to 10 A With Input at 36 V

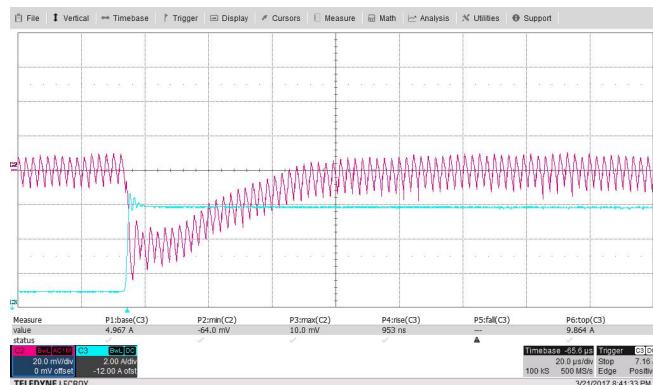


図 29. Buck 3.8-V Output With Load-Step From 5 A to 10 A With Input at 36 V (Zoomed)

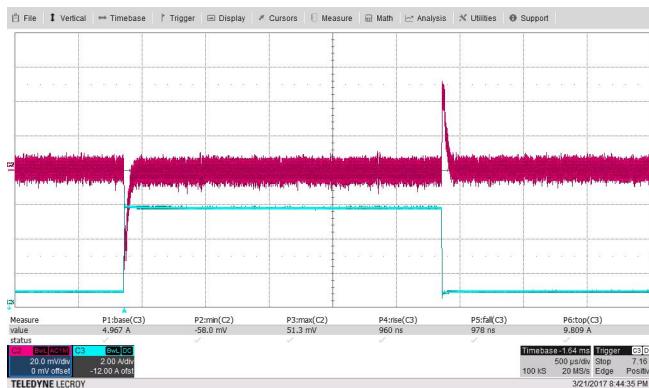


図 30. Buck 3.8-V Output With Load-Step From 5 A to 10 A With Input at 9 V

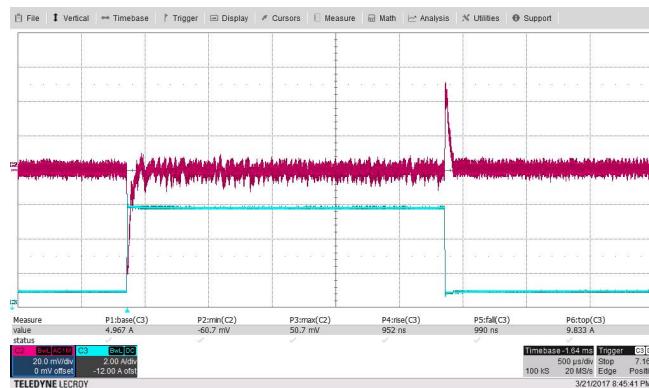


図 31. Buck 3.8-V Output With Load-Step From 5 A to 10 A With Input at 6 V

3.2.2.4 Efficiency Measurements

The efficiency of the 12-V outputs are measured at various input voltages, with the disabled buck controller circuit drawing less than 100 μ A. At typical operating conditions, the efficiency is more than 95%.

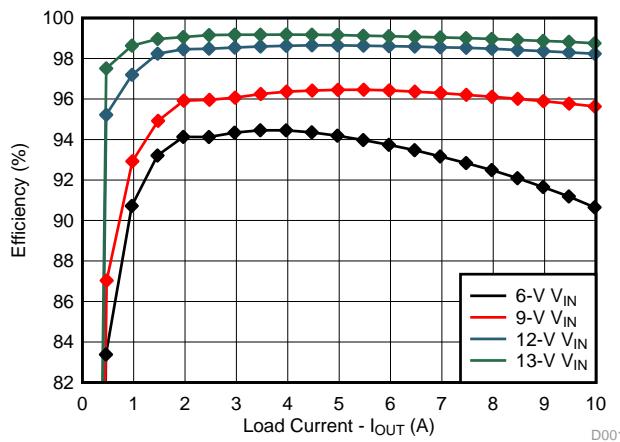


図 32. Boost 12-V Output Efficiency

表 2. Boost 12-V Output Measurements With Input at 6 V

| V_{IN} (V) | I_{IN} (A) | V_{OUT} (V) | I_{OUT} (A) | EFFICIENCY (%) | P_{LOSS} (W) |
|--------------|--------------|---------------|---------------|----------------|----------------|
| 5.999 | 0.179 | 12.065 | 0.000 | 0.000 | 1.071 |
| 5.999 | 1.113 | 12.065 | 0.461 | 83.378 | 1.110 |
| 5.999 | 2.134 | 12.065 | 0.963 | 90.717 | 1.188 |
| 5.999 | 3.157 | 12.066 | 1.463 | 93.208 | 1.286 |
| 5.999 | 4.198 | 12.064 | 1.965 | 94.126 | 1.480 |
| 5.999 | 5.265 | 12.061 | 2.465 | 94.122 | 1.856 |
| 5.999 | 6.315 | 12.060 | 2.964 | 94.339 | 2.145 |
| 5.999 | 7.375 | 12.059 | 3.465 | 94.457 | 2.452 |
| 5.999 | 8.442 | 12.059 | 3.967 | 94.452 | 2.810 |
| 5.999 | 9.519 | 12.059 | 4.468 | 94.353 | 3.225 |
| 5.999 | 10.601 | 12.059 | 4.967 | 94.186 | 3.698 |
| 5.999 | 11.695 | 12.059 | 5.468 | 93.974 | 4.228 |
| 5.999 | 12.796 | 12.059 | 5.968 | 93.739 | 4.807 |
| 5.999 | 13.908 | 12.059 | 6.468 | 93.473 | 5.446 |
| 5.999 | 15.032 | 12.059 | 6.967 | 93.164 | 6.165 |
| 5.999 | 16.177 | 12.059 | 7.471 | 92.833 | 6.955 |
| 5.999 | 17.322 | 12.060 | 7.970 | 92.489 | 7.806 |
| 5.999 | 18.490 | 12.060 | 8.471 | 92.092 | 8.772 |
| 5.999 | 19.680 | 12.061 | 8.972 | 91.653 | 9.855 |
| 5.999 | 20.882 | 12.061 | 9.472 | 91.188 | 11.039 |
| 5.999 | 22.118 | 12.062 | 9.973 | 90.650 | 12.407 |

表 5. Boost 12-V Output Measurements With Input at 13 V

| V _{IN} (V) | I _{IN} (A) | V _{OUT} (V) | I _{OUT} (A) | EFFICIENCY (%) | P _{LOSS} (W) |
|---------------------|---------------------|----------------------|----------------------|----------------|-----------------------|
| 13.004 | 0.011 | 12.972 | 0.000 | 0.000 | 0.138 |
| 13.004 | 0.475 | 12.968 | 0.465 | 97.509 | 0.154 |
| 13.004 | 0.976 | 12.963 | 0.966 | 98.634 | 0.173 |
| 13.004 | 1.476 | 12.958 | 1.466 | 98.964 | 0.199 |
| 13.004 | 1.977 | 12.952 | 1.966 | 99.059 | 0.242 |
| 13.004 | 2.477 | 12.947 | 2.467 | 99.156 | 0.272 |
| 13.004 | 2.977 | 12.942 | 2.967 | 99.177 | 0.319 |
| 13.004 | 3.478 | 12.936 | 3.467 | 99.176 | 0.373 |
| 13.004 | 3.981 | 12.931 | 3.971 | 99.182 | 0.423 |
| 13.004 | 4.481 | 12.926 | 4.471 | 99.177 | 0.480 |
| 13.004 | 4.979 | 12.920 | 4.969 | 99.161 | 0.544 |
| 13.004 | 5.481 | 12.915 | 5.470 | 99.127 | 0.622 |
| 13.004 | 5.980 | 12.909 | 5.970 | 99.106 | 0.696 |
| 13.004 | 6.481 | 12.904 | 6.470 | 99.070 | 0.784 |
| 13.004 | 6.979 | 12.899 | 6.969 | 99.044 | 0.867 |
| 13.004 | 7.480 | 12.893 | 7.470 | 99.008 | 0.965 |
| 13.004 | 7.981 | 12.887 | 7.970 | 98.969 | 1.070 |
| 13.004 | 8.481 | 12.879 | 8.471 | 98.917 | 1.194 |
| 13.004 | 8.982 | 12.872 | 8.972 | 98.871 | 1.319 |
| 13.004 | 9.483 | 12.864 | 9.474 | 98.824 | 1.450 |
| 13.004 | 9.985 | 12.856 | 9.974 | 98.753 | 1.620 |

The efficiency of the 5-V output is measured with no load at the 3.8-V output. The estimated 22 mA of input current drawn by the 3.8-V circuit with the input at 13 V (or 23 mA with the input at 20 V), and 11 mA by the boost circuit, are subtracted in the calculations. At typical operating conditions, the efficiency is more than 90%.

Similarly, the efficiency of the 3.8-V output is measured with no load at the 5-V output. The estimated 26 mA of input current drawn by the 5-V circuit with the input at 13 V (or 27 mA with the input at 20 V), and 11 mA by the boost circuit, are subtracted in the calculations. At typical operating conditions, the efficiency is more than 90%.

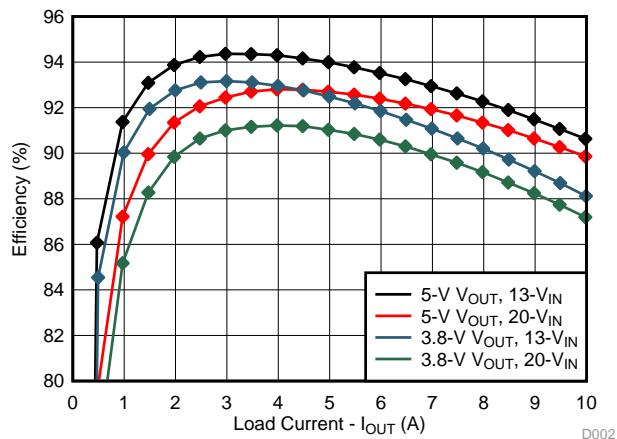


図 33. Buck 5-V and 3.8-V Output Efficiency

3.2.2.5 Bode Plots

The following figures show the bode plots of the design.

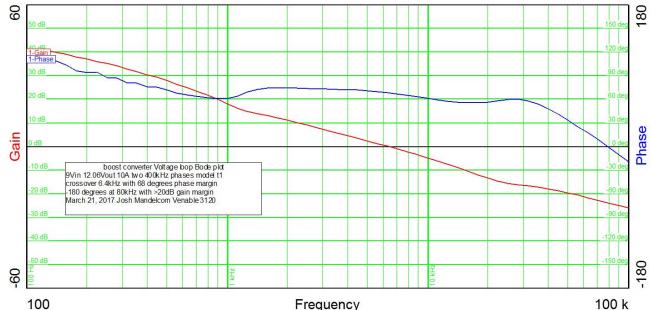


図 34. Boost 12-V Output Bode Plot With Input at 9 V and Output Current at 10 A

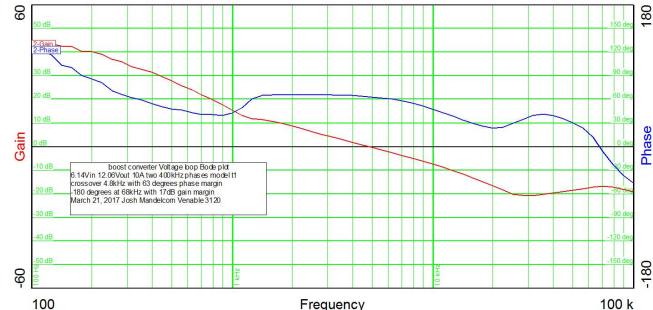


図 35. Boost 12-V Output Bode Plot With Input at 6 V and Output Current at 10 A

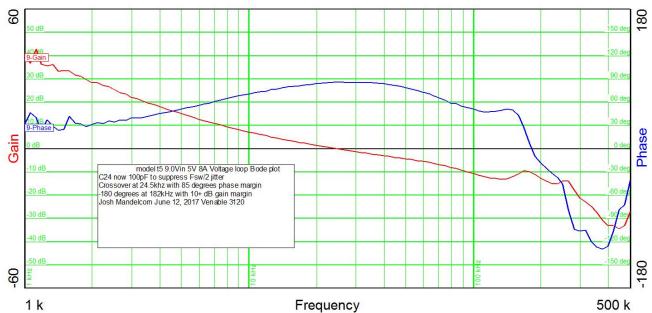


図 36. Buck 5-V Output Bode Plot With Input at 9 V and Output Current at 8 A

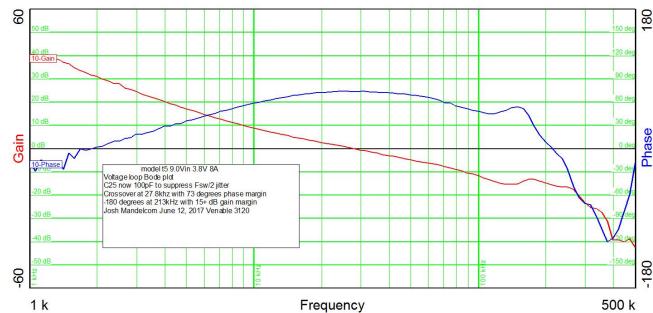


図 37. Buck 3.8-V Output Bode Plot With Input at 9 V and Output Current at 8 A

3.2.2.6 Thermal Measurements

The temperature of the dual LM25122-Q1 boost controllers is measured at steady state input voltage of 9 V, at the ambient temperature of 25°C. One measurement is done with a combined load of 7 A in free air, and the other is done with a combined load of 10 A with airflow of 2 m/s. The temperature of the hottest LM25122-Q1 is 72°C and 61.3°C, respectively, as shown in 図 38 and 図 39.

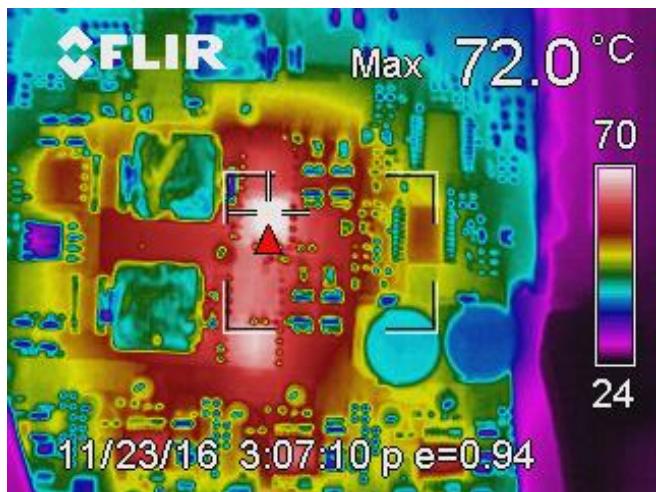


図 38. Thermal Measurement of LM25122-Q1 With Output at 7 A

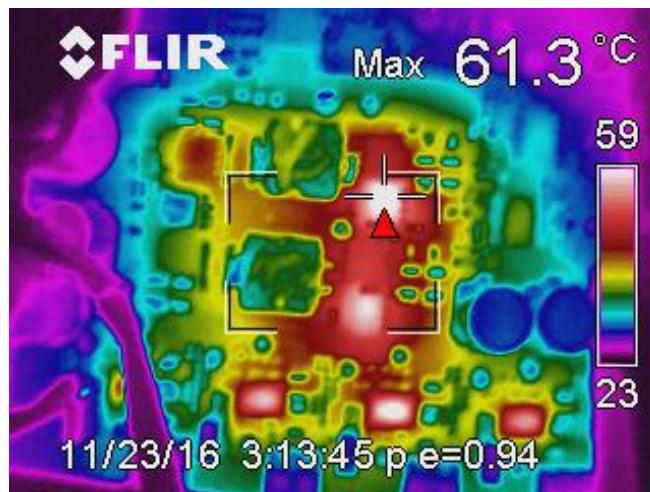


図 39. Thermal Measurement of LM25122-Q1 With Output at 10 A

The temperature of the LM5140-Q1 buck controller is measured at steady state input voltage of 20 V, at the ambient temperature of 25°C. The 5-V output is connected to a 5-A load, and the 3.8-V output is connected to a 6.5-A load. Both measurements are taken in free air. The temperature of the LM5140-Q1 is 56.4°C and 66.5°C, respectively, as shown in 図 40 and 図 41.



図 40. Thermal Measurement of LM5140-Q1 With 5-V Output at 5 A

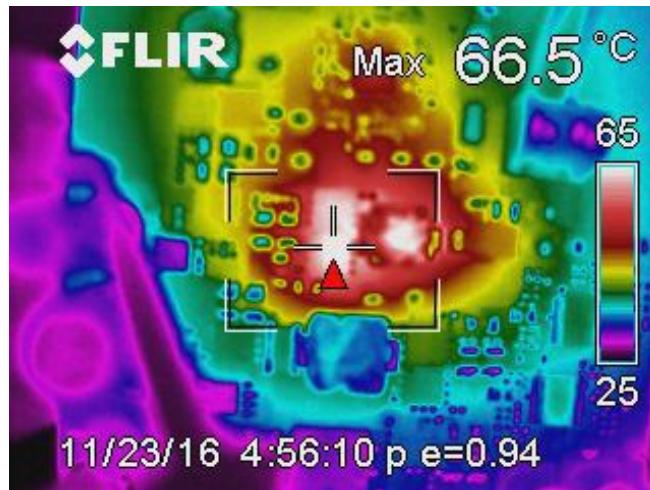


図 41. Thermal Measurement of LM5140-Q1 With 3.8-V Output at 6.5 A

4 Design Files

4.1 Schematics

To download the schematics, see the design files at [TIDA-01534](#).

4.2 Bill of Materials

To download the bill of materials (BOM), see the design files at [TIDA-01534](#).

4.3 PCB Layout Recommendations

4.3.1 Layout Prints

To download the layer plots, see the design files at [TIDA-01534](#).

4.4 Altium Project

To download the Altium project files, see the design files at [TIDA-01534](#).

4.5 Gerber Files

To download the Gerber files, see the design files at [TIDA-01534](#).

4.6 Assembly Drawings

To download the assembly drawings, see the design files at [TIDA-01534](#).

5 Related Documentation

1. Texas Instruments, [AN-1889 How to Measure the Loop Transfer Function of Power Supplies](#)

5.1 商標

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