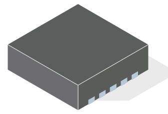


Actual Size
3 mm x 3 mm

650 kHz/1.2 MHz，18.5 V升压型直流(DC)-DC转换器，此转换器有一个3.2A开关

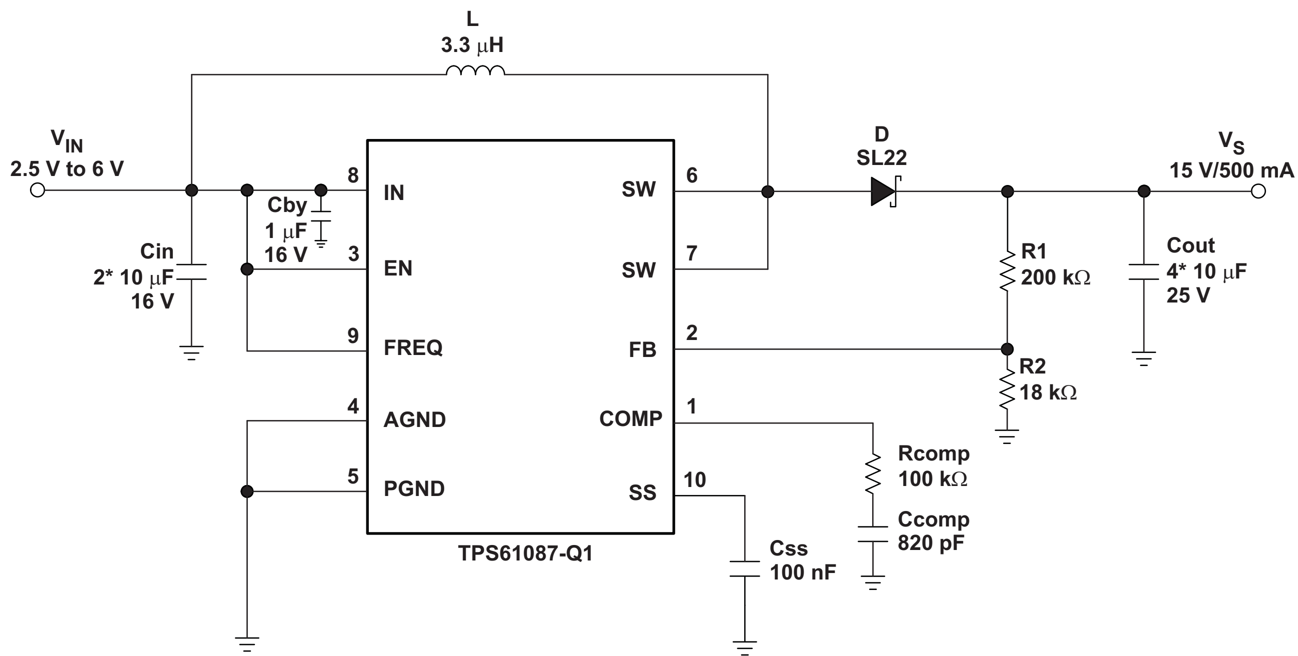
查询样品: **TPS61087-Q1**

特性

- 符合汽车应用要求
- **2.5V** 至 **6V** 输入电压范围
- 具有 **3.2A** 开关电流的 **18.5V** 升压转换器
- **650kHz/1.2MHz** 可选开关频率
- 可调节软启动
- 热关断
- 欠压锁定
- **10** 引脚方形扁平无引脚**(QFN)**封装

说明

TPS61087-Q1是一款高频，高效DC到DC转换器，此转换器含有一个能提供最高为18.5V输出电压的集成3.2A，0.13Ω电源开关。650kHz或者1.2MHz的可选频率使得此器件可使用小型外部电感器和电容器并提供快速瞬态响应。 此外部补偿可以优化特定条件下的应用。 一个连接至软启动引脚的电容器可大大减少启动时的涌入电流。



English Data Sheet: SLVSB50

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ORDERING INFORMATION[(1) (2)]

T_A	PACKAGE		ORDERABLE PART NUMBER	TOP-SIDE MARKING
–40 to 125°C	QFN-10 (DRC)	Reel of 3000	TPS61087QDRCRQ1	PMOQ

(1) The DRC package is available taped and reeled.
(2) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)[(1)]

	VALUE	UNIT
Input voltage range IN[(2)]	–0.3 to 7.0	V
Voltage range on pins EN, FB, SS, FREQ, COMP	–0.3 to 7.0	V
Voltage on pin SW	–0.3 to 20	V
ESD rating HBM	2	kV
ESD rating MM	200	V
ESD rating CDM	1000	V
Continuous power dissipation	See Dissipation Rating Table	
Operating junction temperature range	–40 to 150	°C
Storage temperature range	–65 to 150	°C

(1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability
(2) All voltage values are with respect to network ground terminal.

DISSIPATION RATINGS[(1) (2)]

PACKAGE	$T_A \leq 25°C$ POWER RATING	$T_A = 70°C$ POWER RATING	$T_A = 125°C$ POWER RATING
QFN	1.74 W	0.96 W	0.70 W

(1) $P_D = (T_J – T_A)/R_{\theta JA}$.
(2) The exposed thermal die is soldered to the PCB using thermal vias. For more information, see the Texas Instruments Application report SLMA002 regarding thermal characteristics of the PowerPAD package.

RECOMMENDED OPERATING CONDITIONS

		MIN	TYP	MAX	UNIT
V_{IN}	Input voltage range	2.5		6	V
V_S	Boost output voltage range	V_{IN} + 0.5		18.5	V
T_A	Operating free-air temperature	–40		125	°C

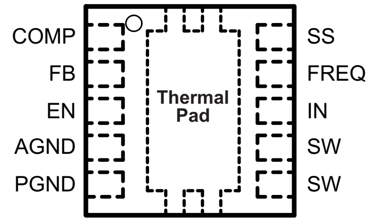
ELECTRICAL CHARACTERISTICS

V_{IN} = 5 V, EN = V_{IN}, V_S = 15 V, T_A = –40°C to 125°C, typical values are at T_A = 25°C (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
V_{IN}	Input voltage range		2.5		6	V
I_Q	Operating quiescent current into IN	Device not switching, V_{FB} = 1.3 V		75	100	μA
I_{SDVIN}	Shutdown current into IN	EN = GND			4	μA
V_{UVLO}	Under-voltage lockout threshold	V_{IN} falling			2.4	V
		V_{IN} rising			2.5	V
T_{SD}	Thermal shutdown	Temperature rising		150		°C
T_{SDHYS}	Thermal shutdown hysteresis			14		°C
LOGIC SIGNALS EN, FREQ						
V_{IH}	High level input voltage	V_{IN} = 2.5 V to 6.0 V	2			V
V_{IL}	Low level input voltage	V_{IN} = 2.5 V to 6.0 V			0.5	V
I_{INLEAK}	Input leakage current	EN = FREQ = GND			0.1	μA
BOOST CONVERTER						
V_S	Boost output voltage		V_{IN} + 0.5		18.5	V
V_{FB}	Feedback regulation voltage		1.230	1.238	1.250	V
gm	Transconductance error amplifier			107		μA/V
I_{FB}	Feedback input bias current	V_{FB} = 1.238 V			0.1	μA
$r_{DS(on)}$	N-channel MOSFET on-resistance	V_{IN} = V_{GS} = 5 V, I_{SW} = current limit		0.13	0.18	Ω
		V_{IN} = V_{GS} = 3V, I_{SW} = current limit		0.16	0.23	
I_{SWLEAK}	SW leakage current	EN = GND, V_{SW} = V_{IN} = 6.0V			2	μA
I_{LIM}	N-Channel MOSFET current limit		3.2	4.0	4.8	A
I_{SS}	Soft-start current	V_{SS} = 1.238 V	7	10	13	μA
f_S	Oscillator frequency	FREQ = V_{IN}	0.9	1.2	1.5	MHz
		FREQ = GND	480	650	820	kHz
	Line regulation	V_{IN} = 2.5 V to 6.0 V, I_{OUT} = 10 mA		0.0002		%/V
	Load regulation	V_{IN} = 5.0 V, I_{OUT} = 1 mA to 1 A		0.11		%/A

PIN ASSIGNMENT

DRC PACKAGE
(TOP VIEW)



10-PIN 3mm x 3mm x 1mm QFN

PIN FUNCTIONS

PIN		I/O	DESCRIPTION
NAME	NO.		
COMP	1	I/O	Compensation pin
FB	2	I	Feedback pin
EN	3	I	Shutdown control input. Connect this pin to logic high level to enable the device
AGND	4, Thermal Pad		Analog ground
PGND	5		Power ground
SW	6, 7		Switch pin
IN	8		Input supply pin
FREQ	9	I	Frequency select pin. The power switch operates at 650 kHz if FREQ is connected to GND and at 1.2 MHz if FREQ is connected to IN
SS	10		Soft-start control pin. Connect a capacitor to this pin if soft-start needed. Open = no soft-start

TYPICAL CHARACTERISTICS

TABLE OF GRAPHS

			FIGURE
$I_{OUT(max)}$	Maximum load current	vs. Input voltage at High frequency (1.2 MHz)	Figure 1
$I_{OUT(max)}$	Maximum load current	vs. Input voltage at Low frequency (650 kHz)	Figure 2
η	Efficiency	vs. Load current, V_S = 15 V, V_{IN} = 5 V	Figure 3
η	Efficiency	vs. Load current, V_S = 9 V, V_{IN} = 3.3 V	Figure 4
	PWM switching - discontinuous conduction		Figure 5
	PWM switching - continuous conduction		Figure 6
	Load transient response	at High frequency (1.2 MHz)	Figure 7
	Load transient response	at Low frequency (650 kHz)	Figure 8
	Soft-start		Figure 9
	Supply current	vs. Supply voltage	Figure 10
	Oscillator frequency	vs. Load current	Figure 11
	Oscillator frequency	vs. Supply voltage	Figure 12

The typical characteristics are measured with the inductors 7447789003 3.3 µH (high frequency) or 74454068 6.8 µH (low frequency) from Wurth and the rectifier diode SL22.

TYPICAL CHARACTERISTICS (continued)

MAXIMUM LOAD CURRENT
vs
INPUT VOLTAGE

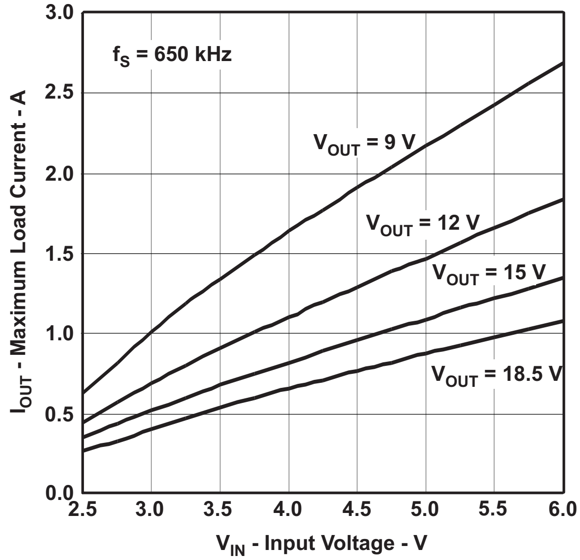


Figure 1.

MAXIMUM LOAD CURRENT
vs
INPUT VOLTAGE

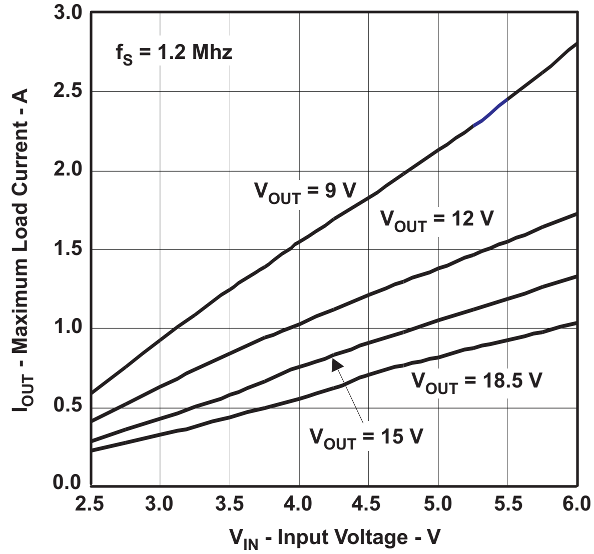


Figure 2.

EFFICIENCY
vs
LOAD CURRENT

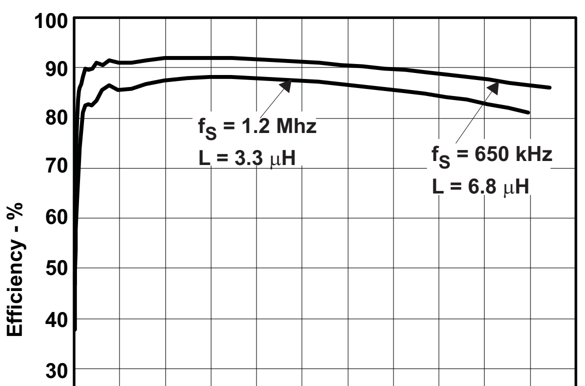


Figure 3.

EFFICIENCY
vs
LOAD CURRENT

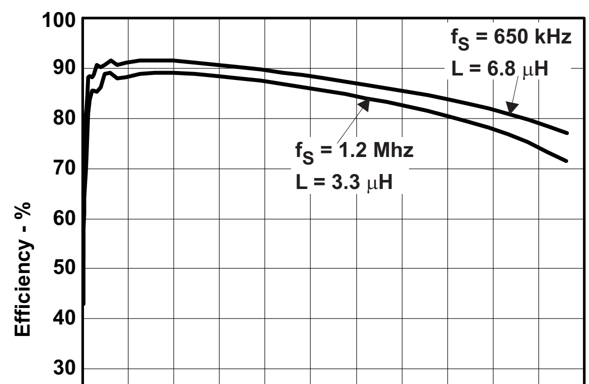


Figure 4.

TYPICAL CHARACTERISTICS (continued)

PWM SWITCHING
DISCONTINUOUS CONDUCTION MODE

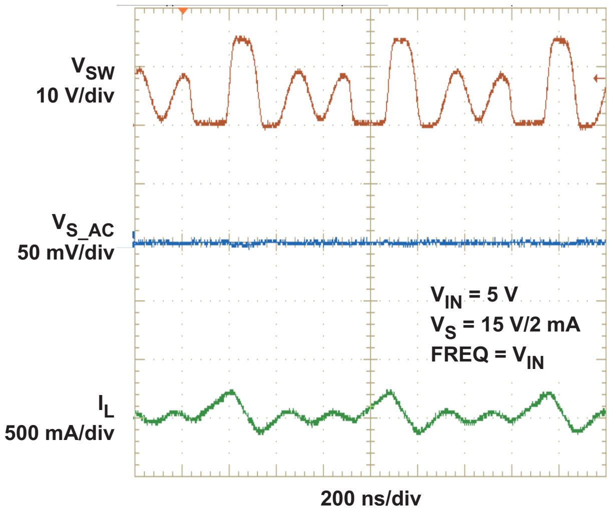


Figure 5.

PWM SWITCHING
CONTINUOUS CONDUCTION MODE

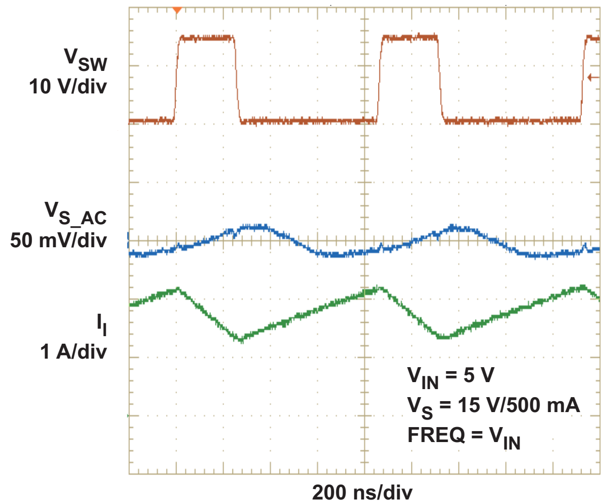


Figure 6.

LOAD TRANSIENT RESPONSE
HIGH FREQUENCY (1.2 MHz)

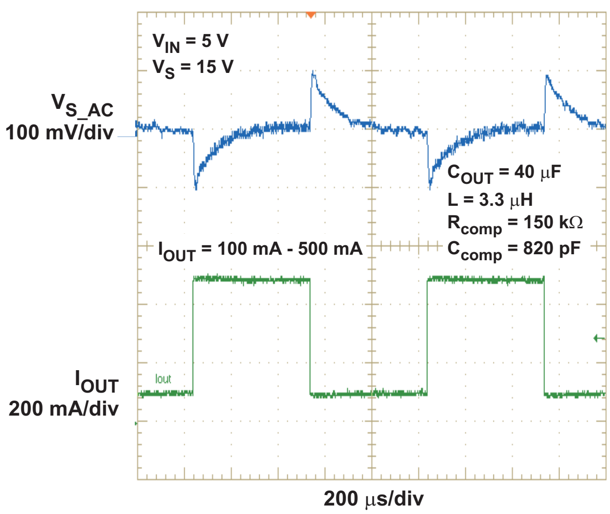


Figure 7.

LOAD TRANSIENT RESPONSE
LOW FREQUENCY (650 kHz)

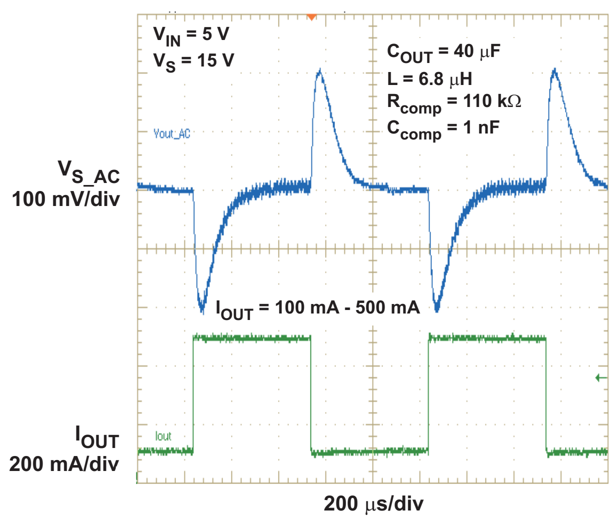


Figure 8.

TYPICAL CHARACTERISTICS (continued)

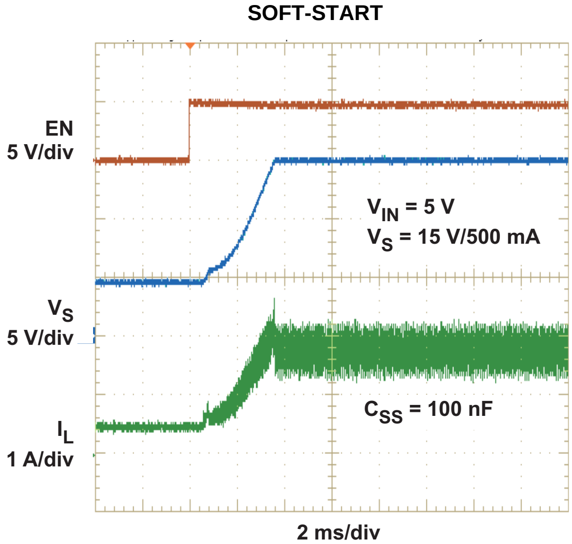


Figure 9.

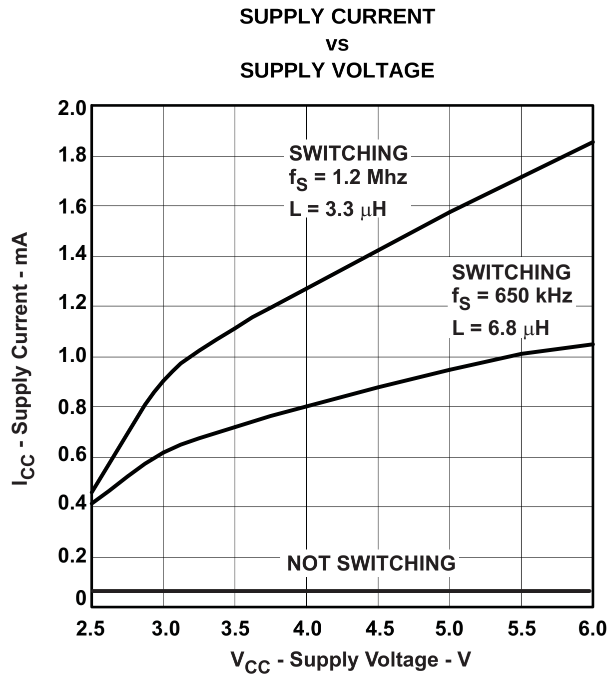


Figure 10.

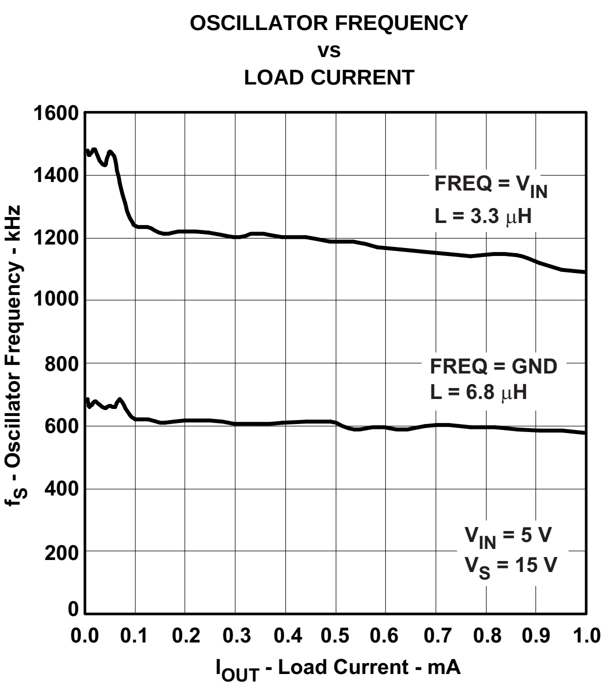


Figure 11.

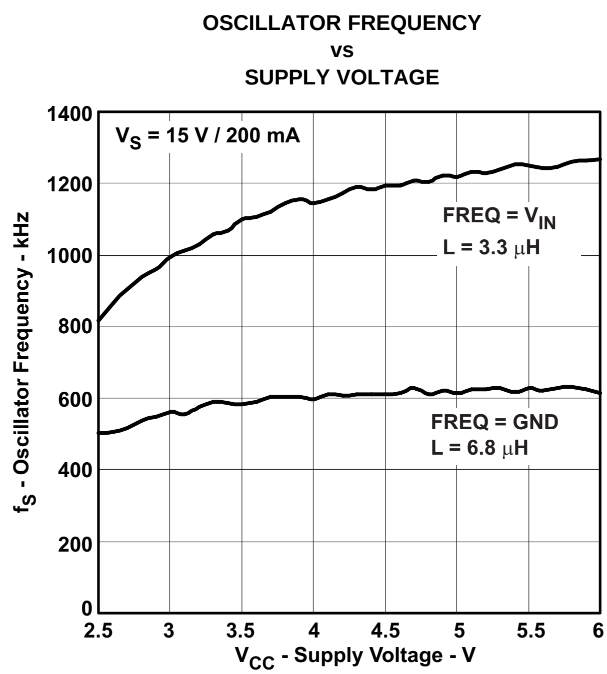


Figure 12.

DETAILED DESCRIPTION

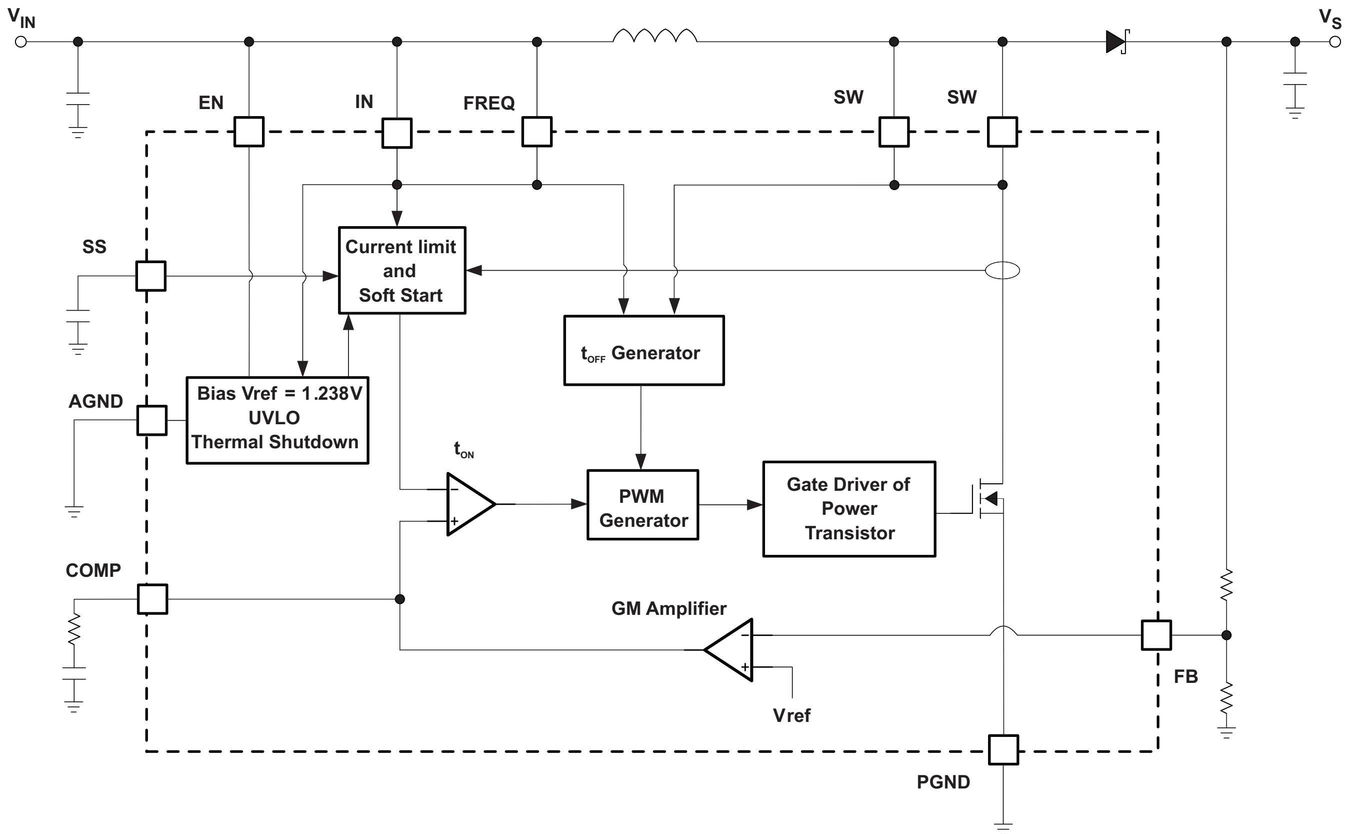


Figure 13. Block Diagram

The boost converter is designed for output voltages up to 18.5 V with a switch peak current limit of 3.2 A minimum. The device, which operates in a current mode scheme with quasi-constant frequency, is externally compensated for maximum flexibility and stability. The switching frequency is selectable between 650 kHz and 1.2 MHz and the minimum input voltage is 2.5 V. To limit the inrush current at start-up a soft-start pin is available.

TPS61087-Q1 boost converter's novel topology using adaptive off-time provides superior load and line transient responses and operates also over a wider range of applications than conventional converters.

The selectable switching frequency offers the possibility to optimize the design either for the use of small sized components (1.2 MHz) or for higher system efficiency (650 kHz). However, the frequency changes slightly because the voltage drop across the $r_{DS(on)}$ has some influence on the current and voltage measurement and thus on the on-time (the off-time remains constant).

The converter operates in continuous conduction mode (CCM) as soon as the input current increases above half the ripple current in the inductor, for lower load currents it switches into discontinuous conduction mode (DCM). If the load is further reduced, the part starts to skip pulses to maintain the output voltage.

Design Procedure

The first step in the design procedure is to verify that the maximum possible output current of the boost converter supports the specific application requirements. A simple approach is to estimate the converter efficiency, by taking the efficiency numbers from the provided efficiency curves or to use a worst case assumption for the expected efficiency, e.g. 90%.

1. Duty cycle, *D*:

$$D = 1 - \frac{V_{IN} \cdot \eta}{V_S} \tag{1}$$

2. Maximum output current, $I_{out(max)}$:

$$I_{out(\max)} = \left(I_{LIM(\min)} - \frac{\Delta I_L}{2} \right) \cdot (1 - D) \tag{2}$$

3. Peak switch current in application, I_{swpeak} :

$$I_{swpeak} = \frac{\Delta I_L}{2} + \frac{I_{out}}{1 - D} \tag{3}$$

with the inductor peak-to-peak ripple current, ΔI_L

$$\Delta I_L = \frac{V_{IN} \cdot D}{f_S \cdot L} \tag{4}$$

and

V_{IN}	Minimum input voltage
V_S	Output voltage
$I_{LIM(min)}$	Converter switch current limit (minimum switch current limit = 3.2 A)
f_S	Converter switching frequency (typically 1.2 MHz or 650 kHz)
L	Selected inductor value
η	Estimated converter efficiency (please use the number from the efficiency plots or 90% as an estimation)

The peak switch current is the steady state peak switch current that the integrated switch, inductor and external Schottky diode has to be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

Soft-start

The boost converter has an adjustable soft-start to prevent high inrush current during start-up. To minimize the inrush current during start-up an external capacitor, connected to the soft-start pin SS and charged with a constant current, is used to slowly ramp up the internal current limit of the boost converter. When the EN pin is pulled high, the soft-start capacitor C_{SS} is immediately charged to 0.3 V. The capacitor is then charged at a constant current of 10 µA typically until the output of the boost converter V_S has reached its Power Good threshold (roughly 98% of V_S nominal value). During this time, the SS voltage directly controls the peak inductor current, starting with 0 A at V_{SS} = 0.3 V up to the full current limit at V_{SS} = 800 mV. The maximum load current is available after the soft-start is completed. The larger the capacitor the slower the ramp of the current limit and the longer the soft-start time. A 100 nF capacitor is usually sufficient for most of the applications. When the EN pin is pulled low, the soft-start capacitor is discharged to ground.

Inductor Selection

The TPS61087-Q1 is designed to work with a wide range of inductors. The main parameter for the inductor selection is the saturation current of the inductor which should be higher than the peak switch current as calculated in the *Design Procedure* section with additional margin to cover for heavy load transients. An alternative, more conservative, is to choose an inductor with a saturation current at least as high as the maximum switch current limit of 4.8 A. The other important parameter is the inductor DC resistance. Usually the lower the DC resistance the higher the efficiency. It is important to note that the inductor DC resistance is not the only parameter determining the efficiency. Especially for a boost converter where the inductor is the energy storage element, the type and core material of the inductor influences the efficiency as well. At high switching frequencies of 1.2 MHz inductor core losses, proximity effects and skin effects become more important. Usually an inductor with a larger form factor gives higher efficiency. The efficiency difference between different inductors can vary between 2% to 10%. For the TPS61087-Q1, inductor values between 3 μH and 6 μH are a good choice with a switching frequency of 1.2 MHz, typically 3.3 μH. At 650 kHz we recommend inductors between 6 μH and 13 μH, typically 6.8 μH. Possible inductors are shown in Table 1.

Typically, it is recommended that the inductor current ripple is below 35% of the average inductor current. Therefore, the following equation can be used to calculate the inductor value, *L*:

$$L = \left(\frac{V_{IN}}{V_S}\right)^2 \cdot \left(\frac{V_S - V_{IN}}{I_{out} \cdot f_S}\right) \cdot \left(\frac{\eta}{0.35}\right) \quad (5)$$

with

V_{IN}	Minimum input voltage
V_S	Output voltage
I_{out}	Maximum output current in the application
f_S	Converter switching frequency (typically 1.2 MHz or 650 kHz)
η	Estimated converter efficiency (please use the number from the efficiency plots or 90% as an estimation)

Table 1. Inductor Selection

L (μH)	SUPPLIER	COMPONENT CODE	SIZE (L×W×H mm)	DCR TYP (mΩ)	I_{sat} (A)
1.2 MHz					
4.2	Sumida	CDRH5D28	5.7 × 5.7 × 3	23	2.2
4.7	Wurth Elektronik	7447785004	5.9 × 6.2 × 3.3	60	2.5
5	Coilcraft	MSS7341	7.3 × 7.3 × 4.1	24	2.9
5	Sumida	CDRH6D28	7 × 7 × 3	23	2.4
4.6	Sumida	CDR7D28	7.6 × 7.6 × 3	38	3.15
4.7	Wurth Elektronik	7447789004	7.3 × 7.3 × 3.2	33	3.9
3.3	Wurth Elektronik	7447789003	7.3 × 7.3 × 3.2	30	4.2
650 kHz					
10	Wurth Elektronik	744778910	7.3 × 7.3 × 3.2	51	2.2
10	Sumida	CDRH8D28	8.3 × 8.3 × 3	36	2.7
6.8	Sumida	CDRH6D26HPNP	7 × 7 × 2.8	52	2.9
6.2	Sumida	CDRH8D58	8.3 × 8.3 × 6	25	3.3
10	Coilcraft	DS3316P	12.95 × 9.40 × 5.08	80	3.5
10	Sumida	CDRH8D43	8.3 × 8.3 × 4.5	29	4
6.8	Wurth Elektronik	74454068	12.7 × 10 × 4.9	55	4.1

Rectifier Diode Selection

To achieve high efficiency a Schottky type should be used for the rectifier diode. The reverse voltage rating should be higher than the maximum output voltage of the converter. The averaged rectified forward current I_{avg}, the Schottky diode needs to be rated for, is equal to the output current I_{out}:

$$I_{avg} = I_{out} \tag{6}$$

Usually a Schottky diode with 2 A maximum average rectified forward current rating is sufficient for most applications. The Schottky rectifier can be selected with lower forward current capability depending on the output current I_{out} but has to be able to dissipate the power. The dissipated power, P_D, is the average rectified forward current times the diode forward voltage, $V_{forward}$.

$$P_D = I_{avg} \cdot V_{forward} \tag{7}$$

Typically the diode should be able to dissipate around 500mW depending on the load current and forward voltage.

Table 2. Rectifier Diode Selection

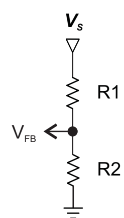
CURRENT RATING I_{avg}	V_r	$V_{forward}/I_{avg}$	SUPPLIER	COMPONENT CODE
2 A	20 V	0.44 V / 2 A	Vishay Semiconductor	SL22
2 A	20 V	0.5 V / 2 A	Fairchild Semiconductor	SS22

Setting the Output Voltage

The output voltage is set by an external resistor divider. Typically, a minimum current of 50 μA flowing through the feedback divider gives good accuracy and noise covering. A standard low side resistor of 18 kΩ is typically selected. The resistors are then calculated as:

$$R2 = \frac{V_{FB}}{70\mu A} \approx 18k\Omega \qquad R1 = R2 \cdot \left(\frac{V_S}{V_{FB}} - 1\right)$$

$$V_{FB} = 1.238V$$



(8)

Compensation (COMP)

The regulator loop can be compensated by adjusting the external components connected to the COMP pin. The COMP pin is the output of the internal transconductance error amplifier.

Standard values of R_{COMP} = *16 kΩ* and C_{COMP} = *2.7 nF* will work for the majority of the applications.

See Table 3 for dedicated compensation networks giving an improved load transient response. The following equations can be used to calculate R_{COMP} and C_{COMP}:

$$R_{COMP} = \frac{110 \cdot V_{IN} \cdot V_S \cdot C_{out}}{L \cdot I_{out}} \qquad C_{COMP} = \frac{V_s \cdot C_{out}}{7.5 \cdot I_{out} \cdot R_{COMP}} \tag{9}$$

with

V_{IN}	Minimum input voltage
V_S	Output voltage
C_{out}	Output capacitance
L	Inductor value, e.g. 3.3 μH or 6.8 μH
I_{out}	Maximum output current in the application

Make sure that R_{COMP} < *120 kΩ* and C_{COMP}> *820 pF*, independent of the results of the above formulas.

Table 3. Recommended Compensation Network Values at High/Low Frequency

FREQUENCY	L	V_S	V_{IN} ± 20%	R_{COMP}	C_{COMP}
High (1.2 MHz)	3.3 µH	15 V	5 V	100 kΩ	820 pF
			3.3 V	91 kΩ	1.2 nF
		12 V	5 V	68 kΩ	820 pF
			3.3 V	68 kΩ	1.2 nF
		9 V	5 V	39 kΩ	820 pF
			3.3 V	39 kΩ	1.2 nF
Low (650 kHz)	6.8 µH	15 V	5 V	51 kΩ	1.5 nF
			3.3 V	47 kΩ	2.7 nF
		12 V	5 V	33 kΩ	1.5 nF
			3.3 V	33 kΩ	2.7 nF
		9 V	5 V	18 kΩ	1.5 nF
			3.3 V	18 kΩ	2.7 nF

Table 3 gives conservative R_{COMP} and C_{COMP} values for certain inductors, input and output voltages providing a very stable system. For a faster response time, a higher R_{COMP} value can be used to enlarge the bandwidth, as well as a slightly lower value of C_{COMP} to keep enough phase margin. These adjustments should be performed in parallel with the load transient response monitoring of TPS61087-Q1.

Input Capacitor Selection

For good input voltage filtering low ESR ceramic capacitors are recommended. TPS61087-Q1 has an analog input IN. Therefore, a 1 µF bypass is highly recommended as close as possible to the IC from IN to GND.

Two 10 µF (or one 22 µF) ceramic input capacitors are sufficient for most of the applications. For better input voltage filtering this value can be increased. See Table 4 and typical applications for input capacitor recommendation.

Output Capacitor Selection

For best output voltage filtering a low ESR output capacitor like ceramic capcaitor is recommended. Four 10 µF ceramic output capacitors (or two 22 µF) work for most of the applications. Higher capacitor values can be used to improve the load transient response. See Table 4 for the selection of the output capacitor.

Table 4. Rectifier Input and Output Capacitor Selection

	CAPACITOR/SIZE	VOLTAGE RATING	SUPPLIER	COMPONENT CODE
C_{IN}	22 µF/1206	16 V	Taiyo Yuden	EMK316 BJ 226ML
IN bypass	1 µF/0603	16 V	Taiyo Yuden	EMK107 BJ 105KA
C_{OUT}	10 µF/1206	25 V	Taiyo Yuden	TMK316 BJ 106KL

To calculate the output voltage ripple, the following equation can be used:

$$\Delta V_C = \frac{V_S - V_{IN}}{V_S \cdot f_S} \cdot \frac{I_{out}}{C_{out}} \qquad \Delta V_{C\_ESR} = I_{L(peak)} \cdot R_{C\_ESR} \tag{10}$$

with

ΔV_C	Output voltage ripple dependent on output capacitance,output current and switching frequency
V_S	Output voltage
V_{IN}	Minimum input voltage of boost converter
f_S	Converter switching frequency (typically 1.2 MHz or 650 kHz)
I_{out}	Output capacitance
ΔV_{C_ESR}	Output voltage ripple due to output capacitors ESR (equivalent series resistance)
I_{SWPEAK}	Inductor peak switch current in the application
R_{C_ESR}	Output capacitors equivalent series resistance (ESR)

ΔV_{C_ESR} can be neglected in many cases since ceramic capacitors provide low ESR.

Frequency Select Pin (FREQ)

The frequency select pin FREQ allows to set the switching frequency of the device to 650 kHz (FREQ = low) or 1.2 MHz (FREQ = high). Higher switching frequency improves load transient response but reduces slightly the efficiency. The other benefits of higher switching frequency are a lower output ripple voltage. The use of a 1.2 MHz switching frequency is recommended unless light load efficiency is a major concern.

Undervoltage Lockout (UVLO)

To avoid mis-operation of the device at low input voltages an undervoltage lockout is included that disables the device, if the input voltage falls below 2.4 V.

Thermal Shutdown

A thermal shutdown is implemented to prevent damages due to excessive heat and power dissipation. Typically the thermal shutdown happens at a junction temperature of 150°C. When the thermal shutdown is triggered the device stops switching until the junction temperature falls below typically 136°C. Then the device starts switching again.

Overvoltage Prevention

If overvoltage is detected on the FB pin (typically 3 % above the nominal value of 1.238 V) the part stops switching immediately until the voltage on this pin drops to its nominal value. This prevents overvoltage on the output and secures the circuits connected to the output from excessive overvoltage.

APPLICATION INFORMATION

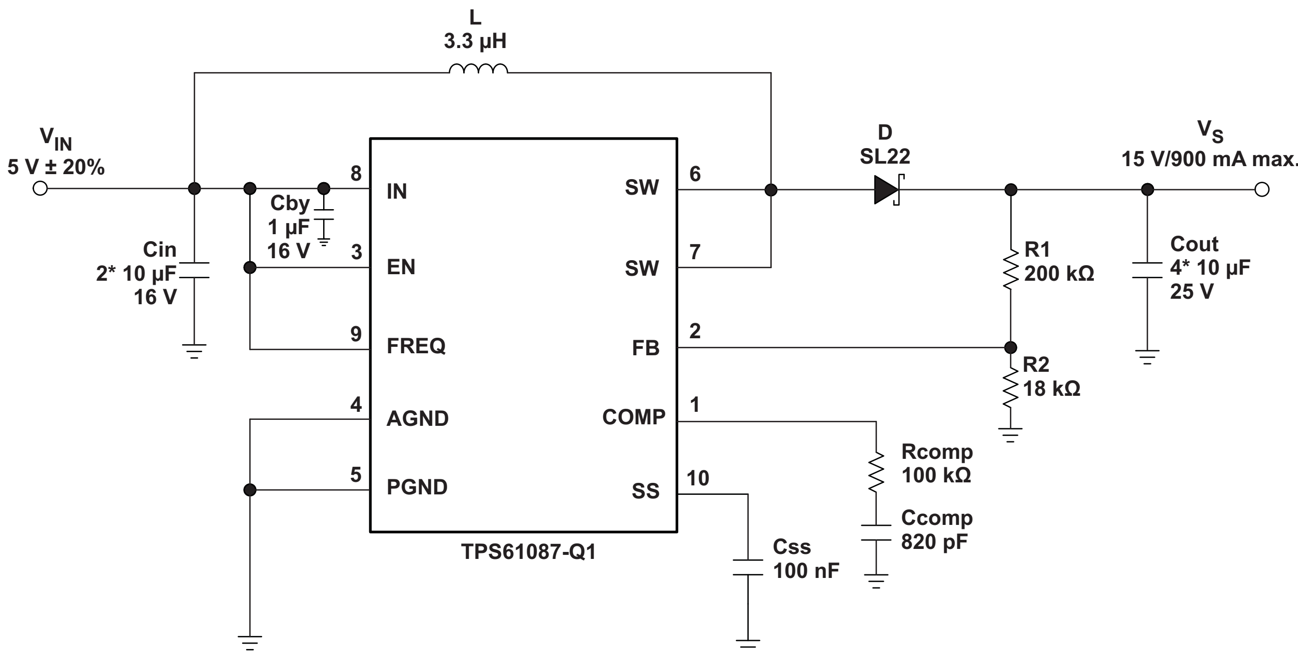


Figure 14. Typical Application, 5 V to 15 V (f_S = 1.2 MHz)

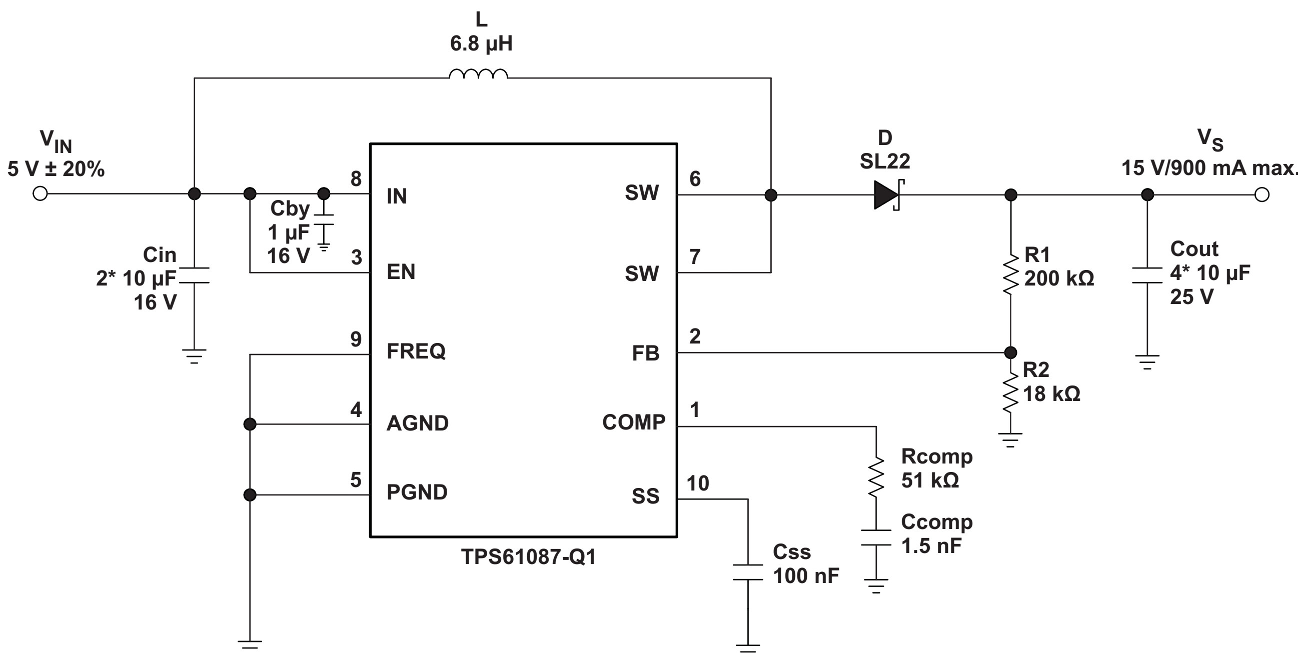


Figure 15. Typical Application, 5 V to 15 V (f_S = 650 kHz)

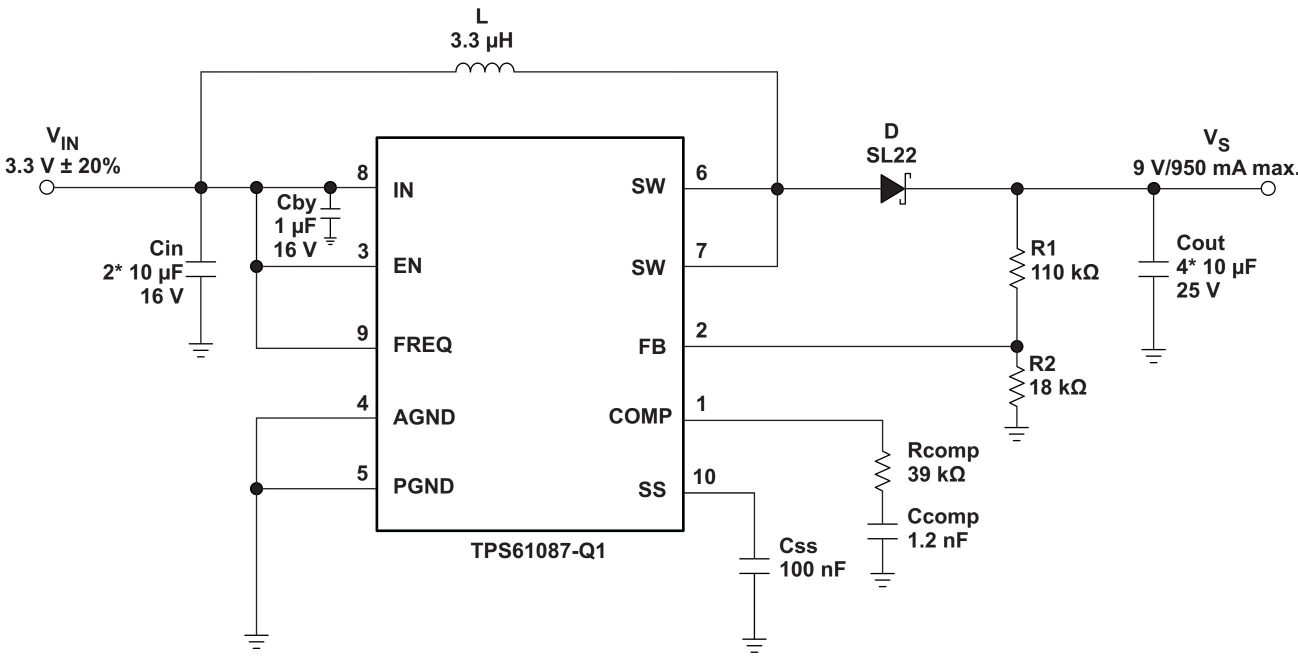


Figure 16. Typical Application, 3.3 V to 9 V (f_S = 1.2 MHz)

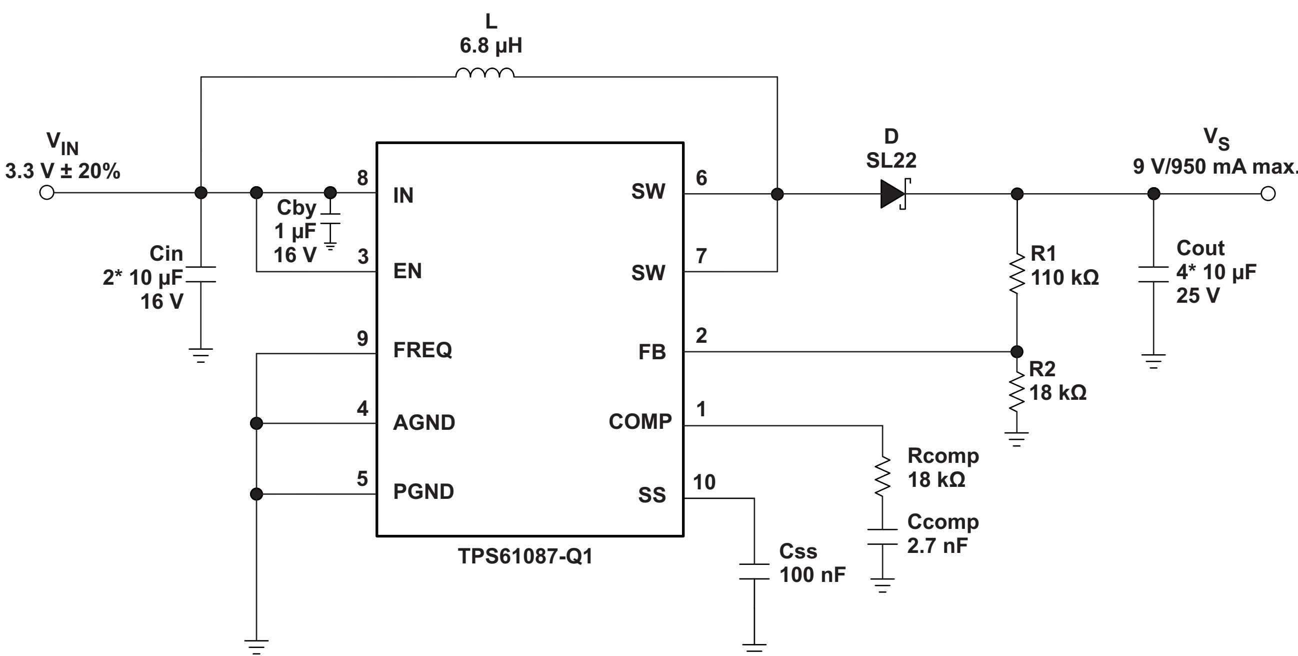


Figure 17. Typical Application, 3.3 V to 9 V (f_S = 650 kHz)

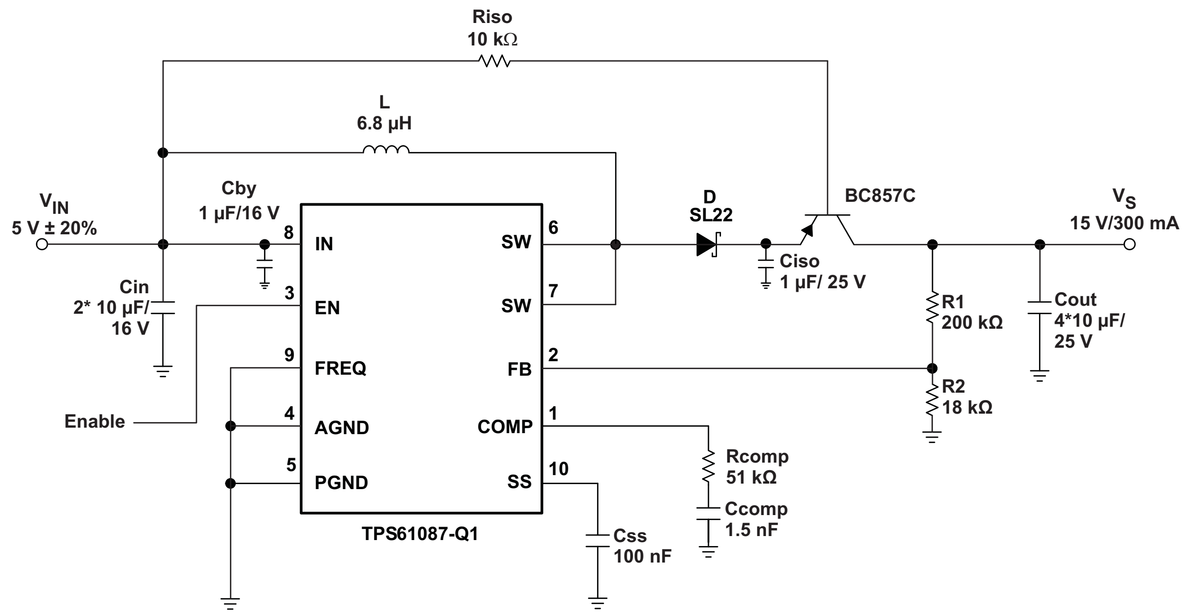


Figure 18. Typical Application with External Load Disconnect Switch

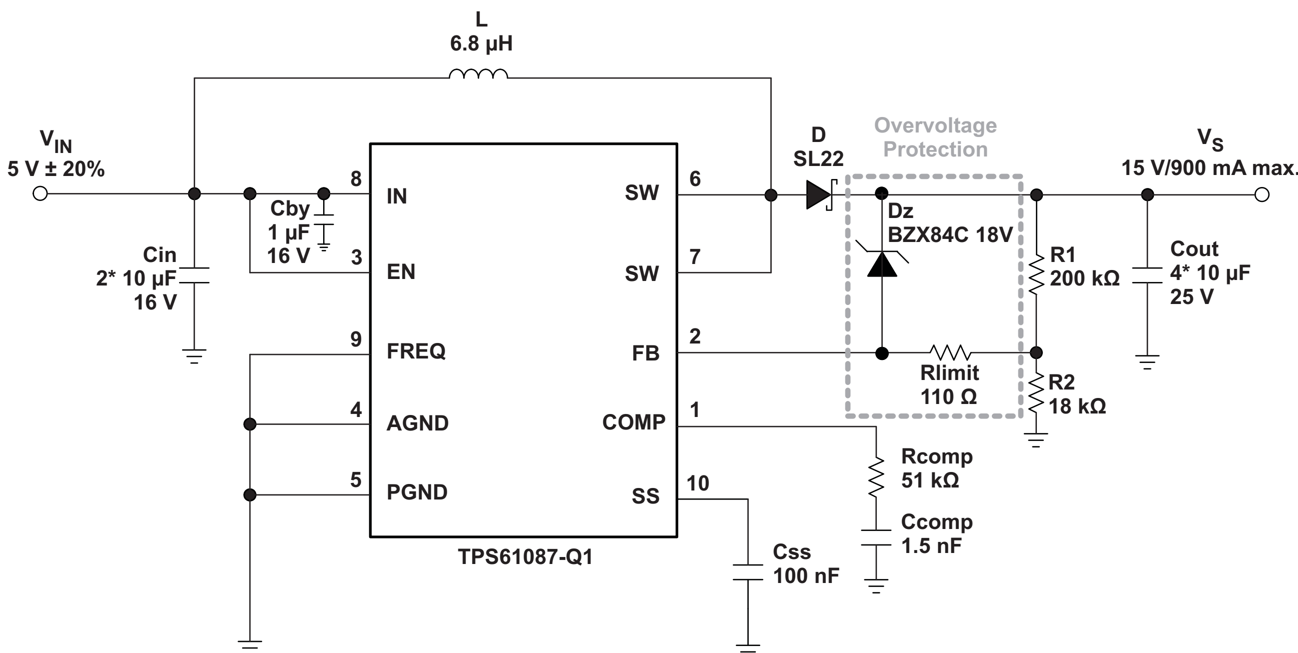


Figure 19. Typical Application, 5 V to 15 V (f_S = 1.2 MHz) with Overvoltage Protection

TFT LCD APPLICATION

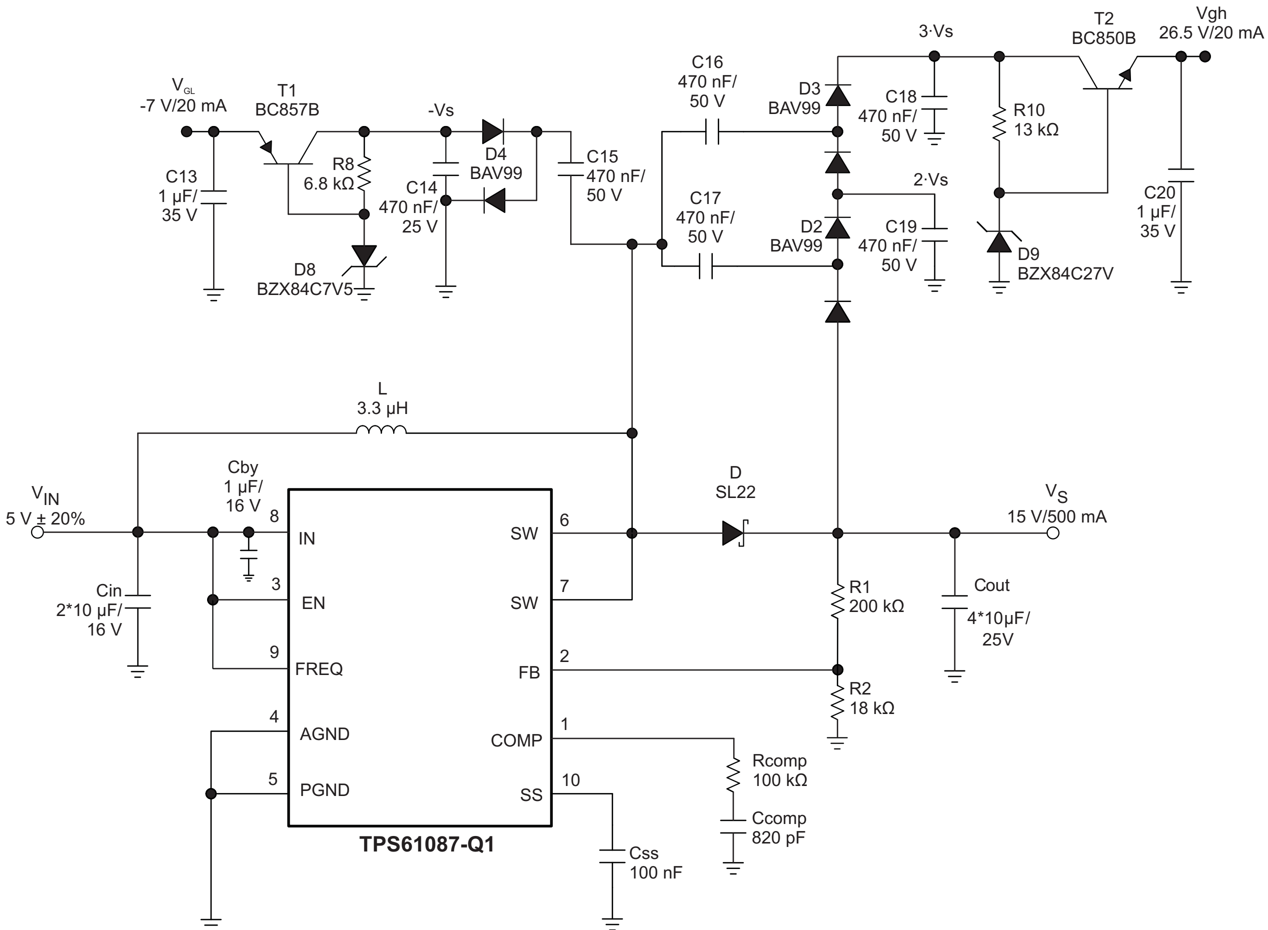


Figure 20. Typical Application 5 V to 15 V (f_S = 1.2 MHz) for TFT LCD with External Charge Pumps (VGH, VGL)

WHITE LED APPLICATIONS

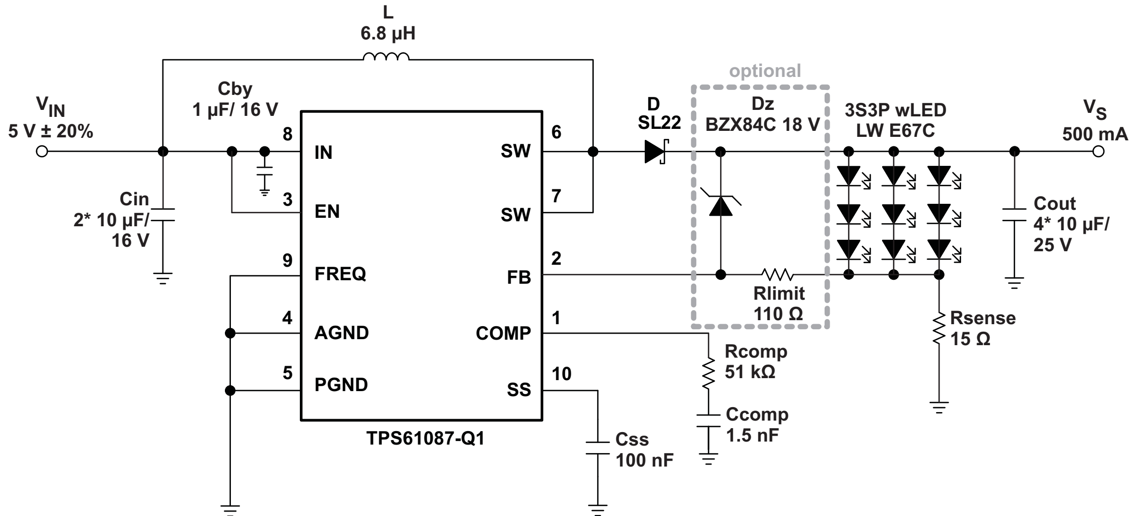


Figure 21. Simple Application (5 V input voltage) (f_S = 650 kHz) for wLED Supply (3S3P) (with optional clamping Zener diode)

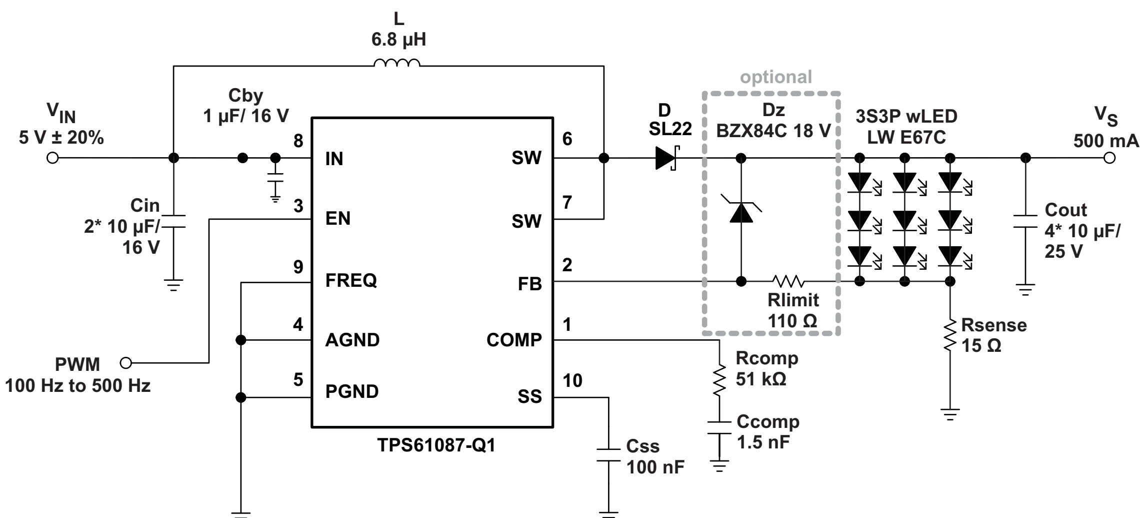


Figure 22. Simple Application (5 V input voltage) (f_S = 650 kHz) for wLED Supply (3S3P) with Adjustable Brightness Control using a PWM Signal on the Enable Pin (with optional clamping Zener diode)

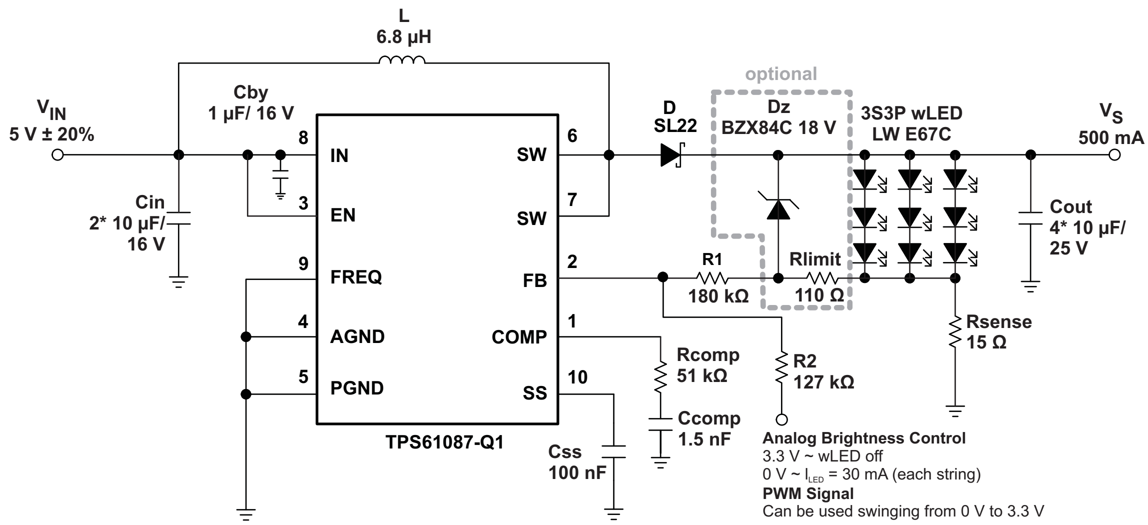


Figure 23. Simple Application (5 V input voltage) (f_S = 650 kHz) for wLED Supply (3S3P) with Adjustable Brightness Control using an Analog Signal on the Feedback Pin (with optional clamping Zener diode)

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package | Pins	Package qty | Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS61087QDRCRQ1	Active	Production	VSON (DRC) | 10	3000 | LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	PMOQ
TPS61087QDRCRQ1.B	Active	Production	VSON (DRC) | 10	3000 | LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	PMOQ
TPS61087QWDRCRQ1	Active	Production	VSON (DRC) | 10	3000 | LARGE T&R	Yes	SN	Level-3-260C-168 HR	-40 to 125	11ZC
TPS61087QWDRCRQ1.B	Active	Production	VSON (DRC) | 10	3000 | LARGE T&R	Yes	SN	Level-3-260C-168 HR	-40 to 125	11ZC

(1) **Status:** For more details on status, see our product life cycle.

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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OTHER QUALIFIED VERSIONS OF TPS61087-Q1 :

- Catalog : TPS61087

NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product

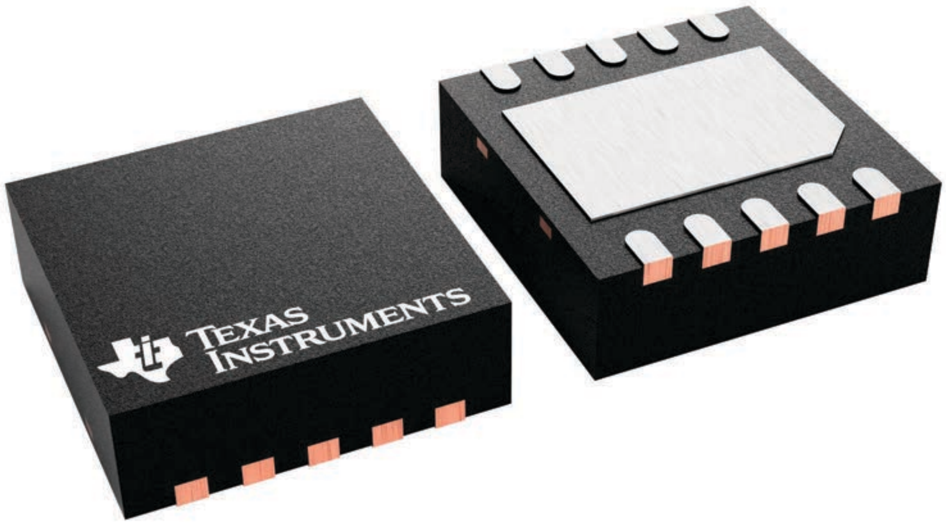
DRC 10

VSON - 1 mm max height

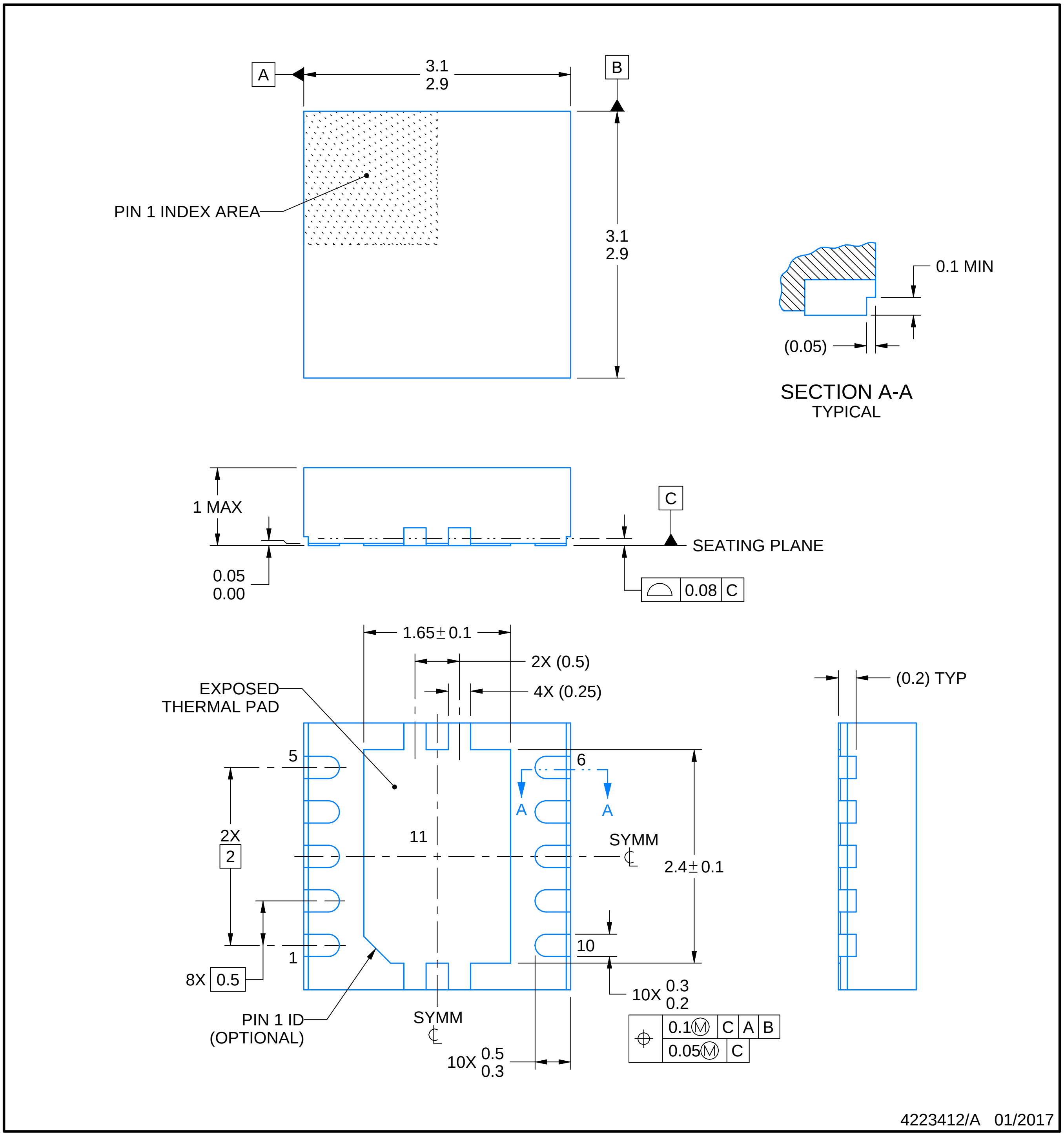
3 x 3, 0.5 mm pitch

PLASTIC SMALL OUTLINE - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.

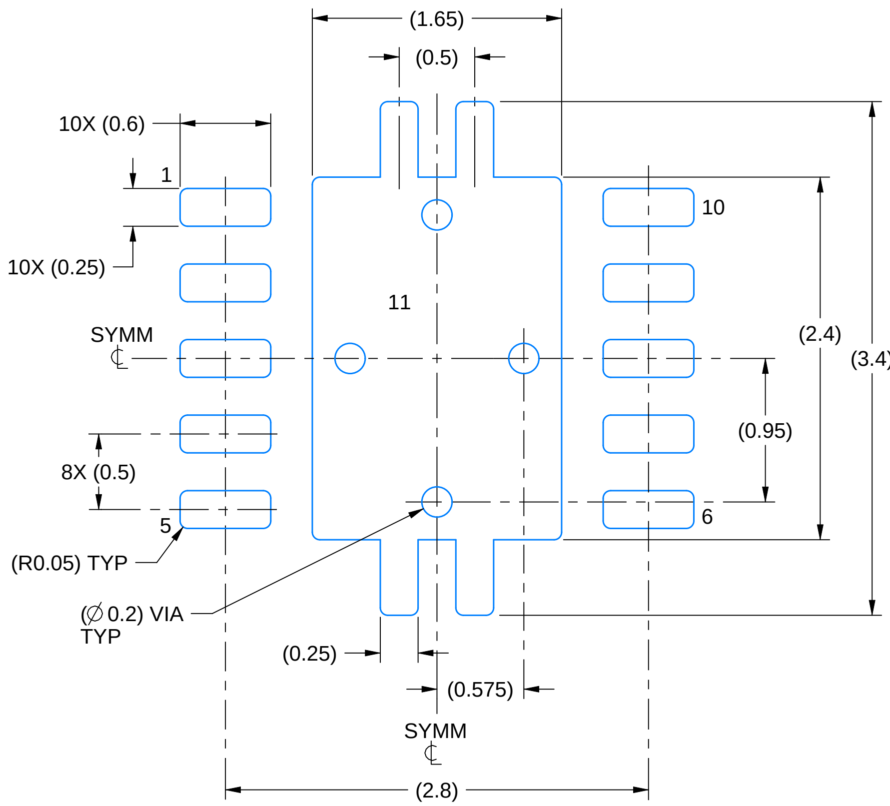


4226193/A

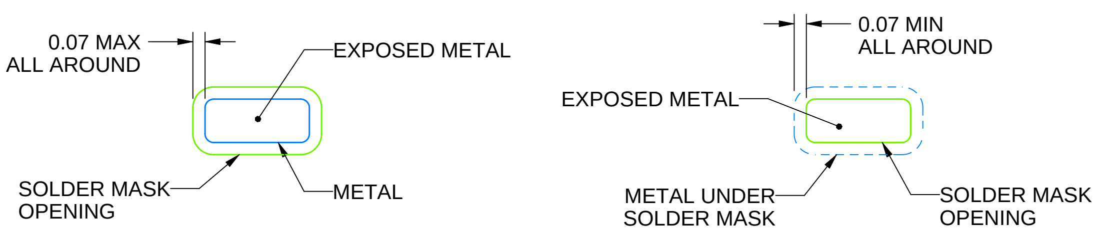


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for optimal thermal and mechanical performance.



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE:20X



NON SOLDER MASK
DEFINED
(PREFERRED)

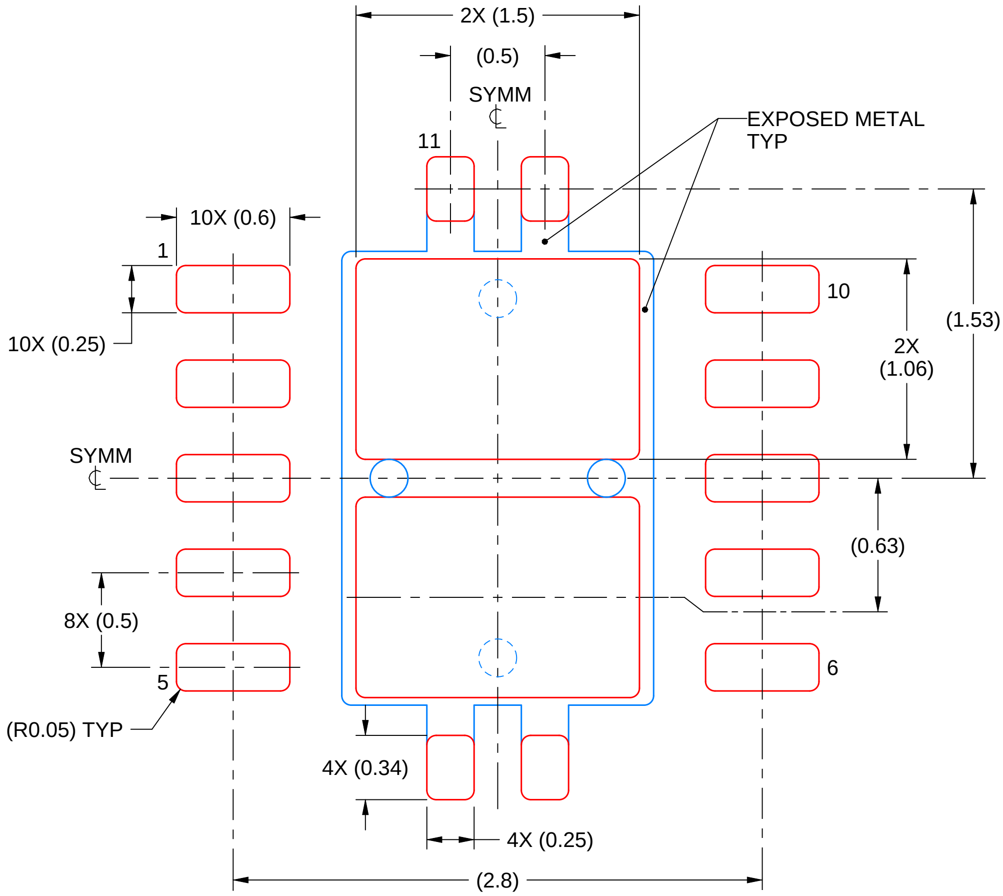
SOLDER MASK
DEFINED

SOLDER MASK DETAILS

4223412/A 01/2017

NOTES: (continued)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



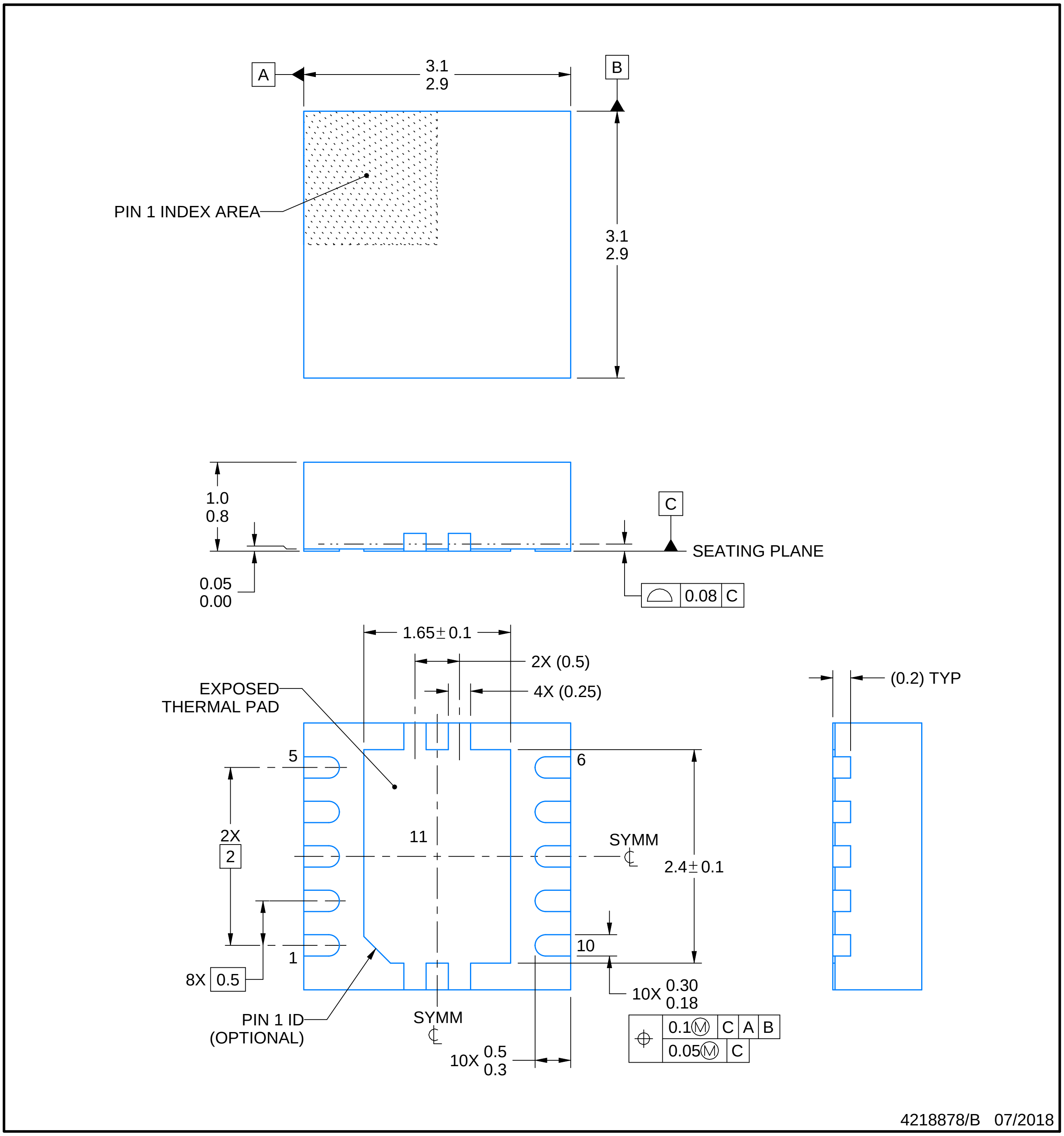
SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 11:
80% PRINTED SOLDER COVERAGE BY AREA
SCALE:25X

4223412/A 01/2017

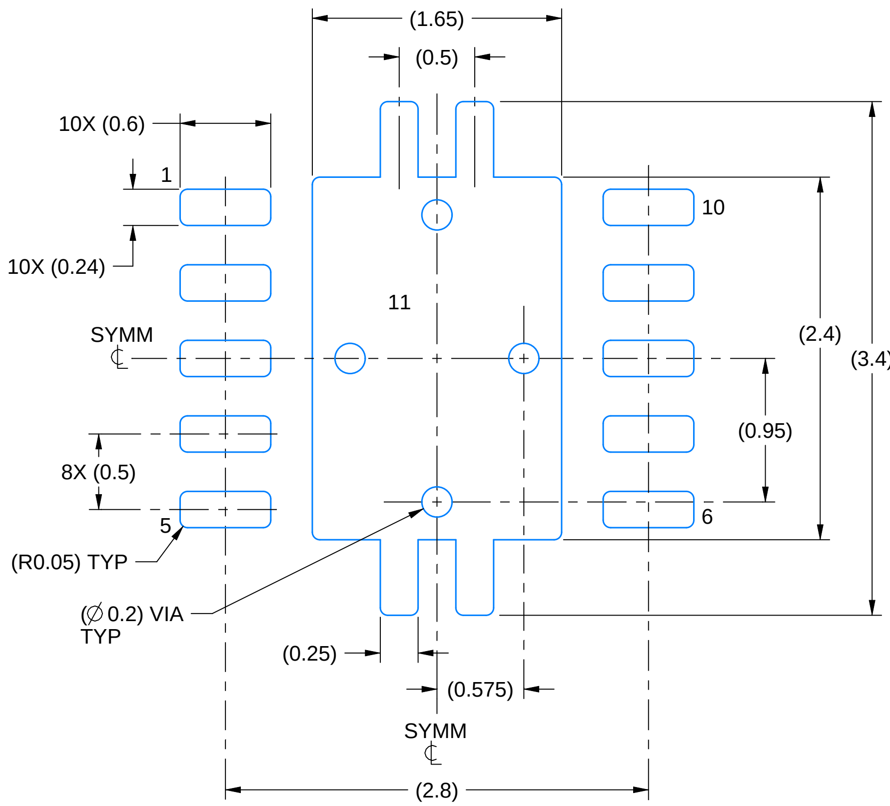
NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

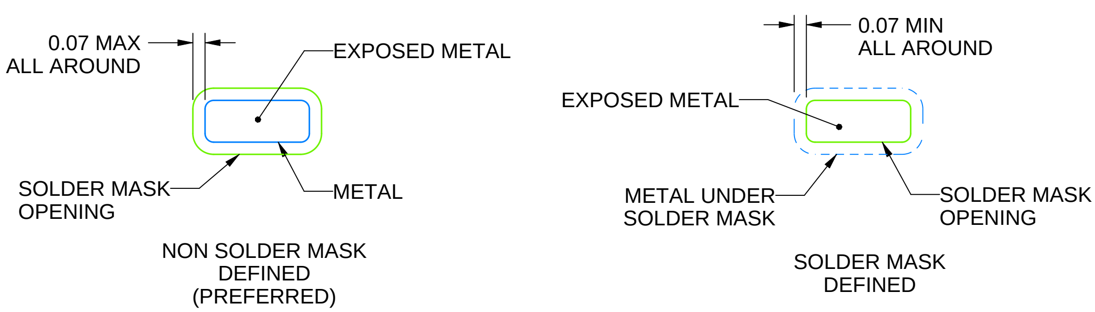


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for optimal thermal and mechanical performance.



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE:20X

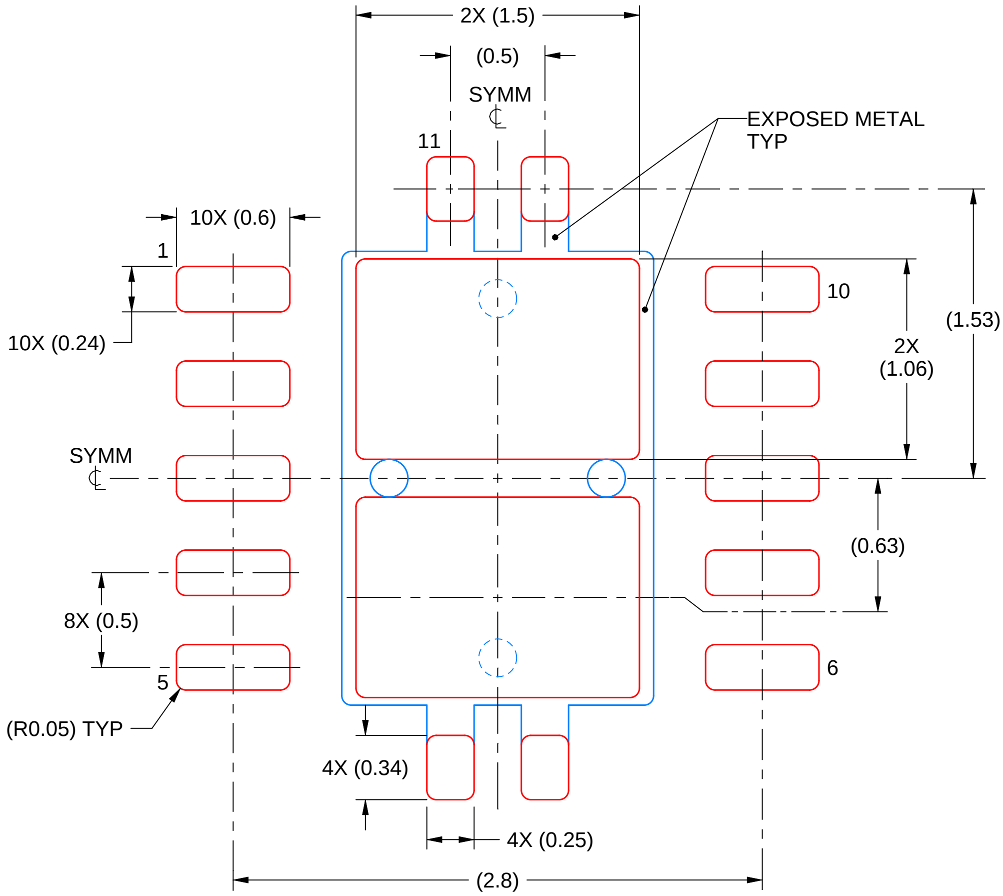


SOLDER MASK DETAILS

4218878/B 07/2018

NOTES: (continued)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 11:
80% PRINTED SOLDER COVERAGE BY AREA
SCALE:25X

4218878/B 07/2018

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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