

# Instrumentation Amplifier (IA) topologies: one-amp

TI Precision Labs – Instrumentation Amplifiers

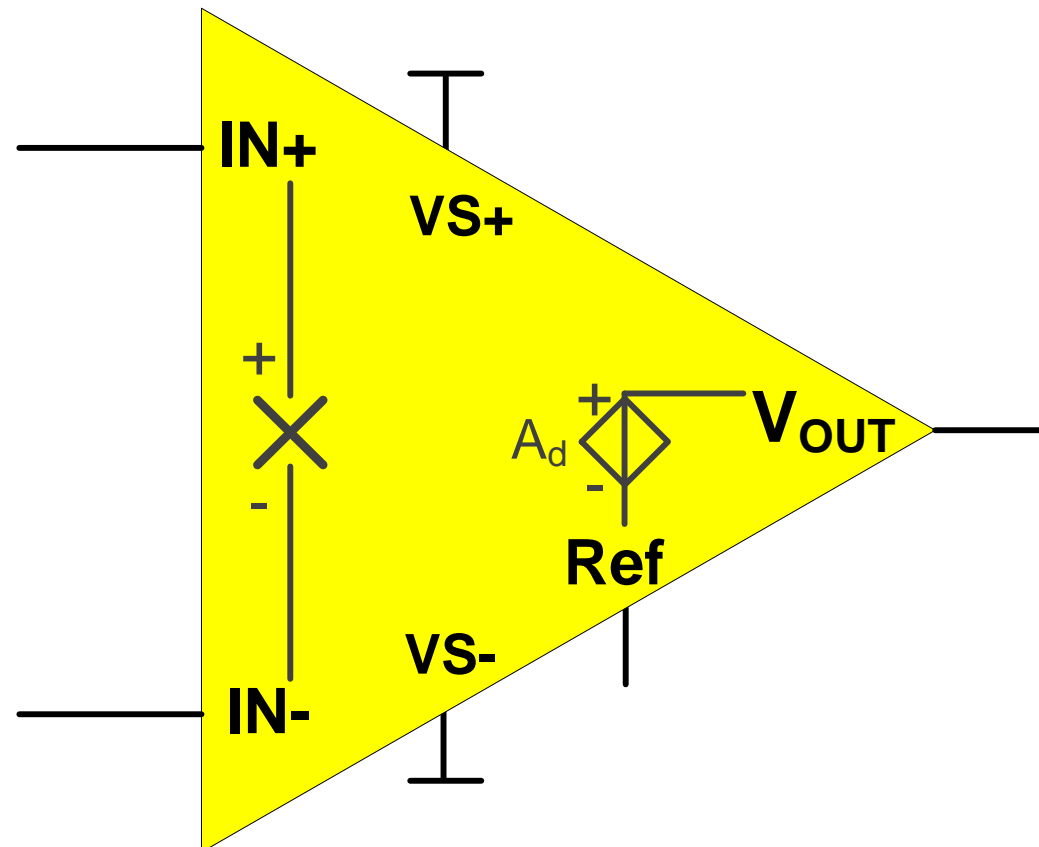
Presented by Tamara Alani

Prepared by Tamara Alani

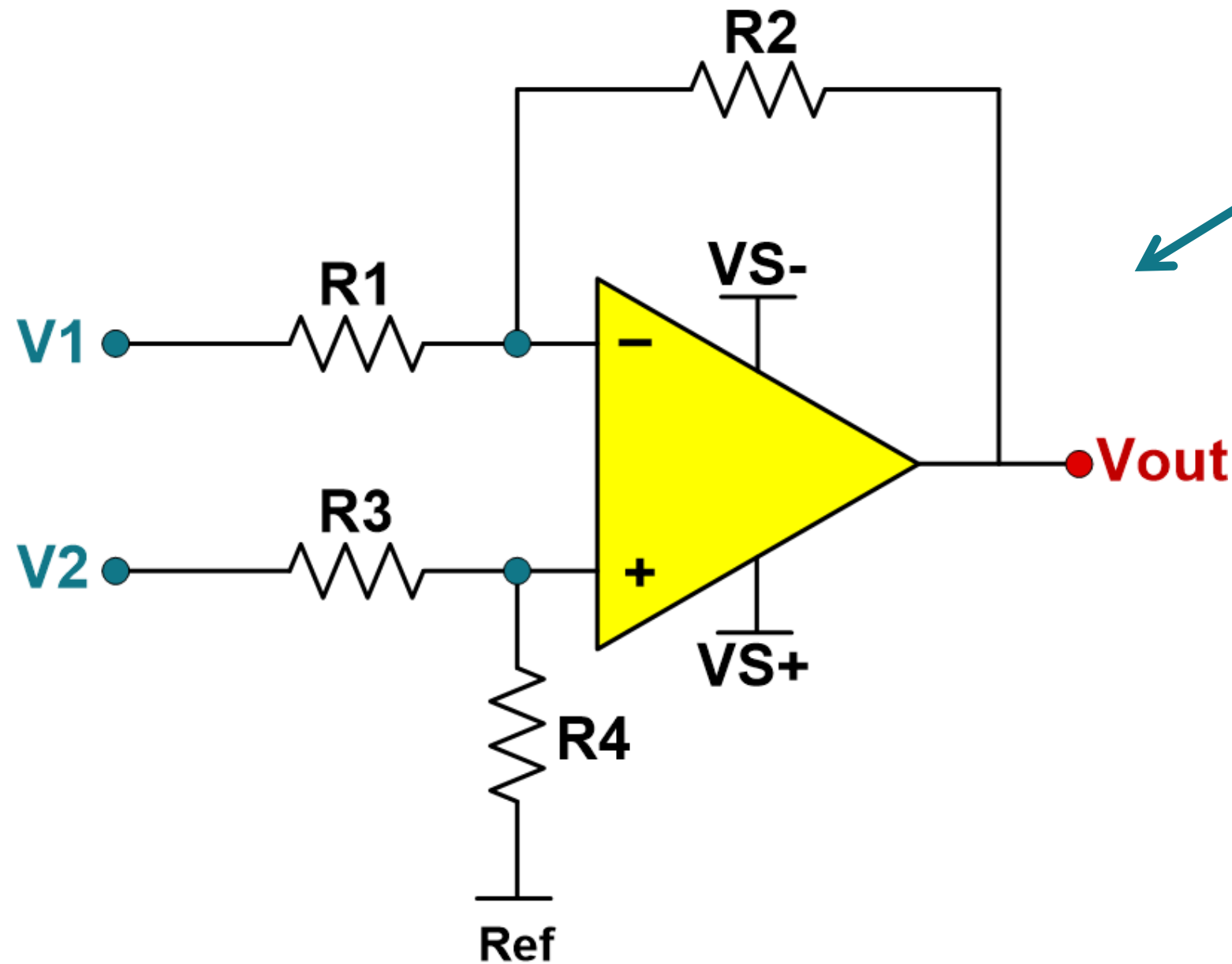
# Instrumentation amplifier – Idealized model

Two main characteristics of an instrumentation amplifier:

1. Amplifies the signals that differ between the two inputs
2. Rejects the signals that are the same (common) to both inputs



# IA topology – One-amp configuration



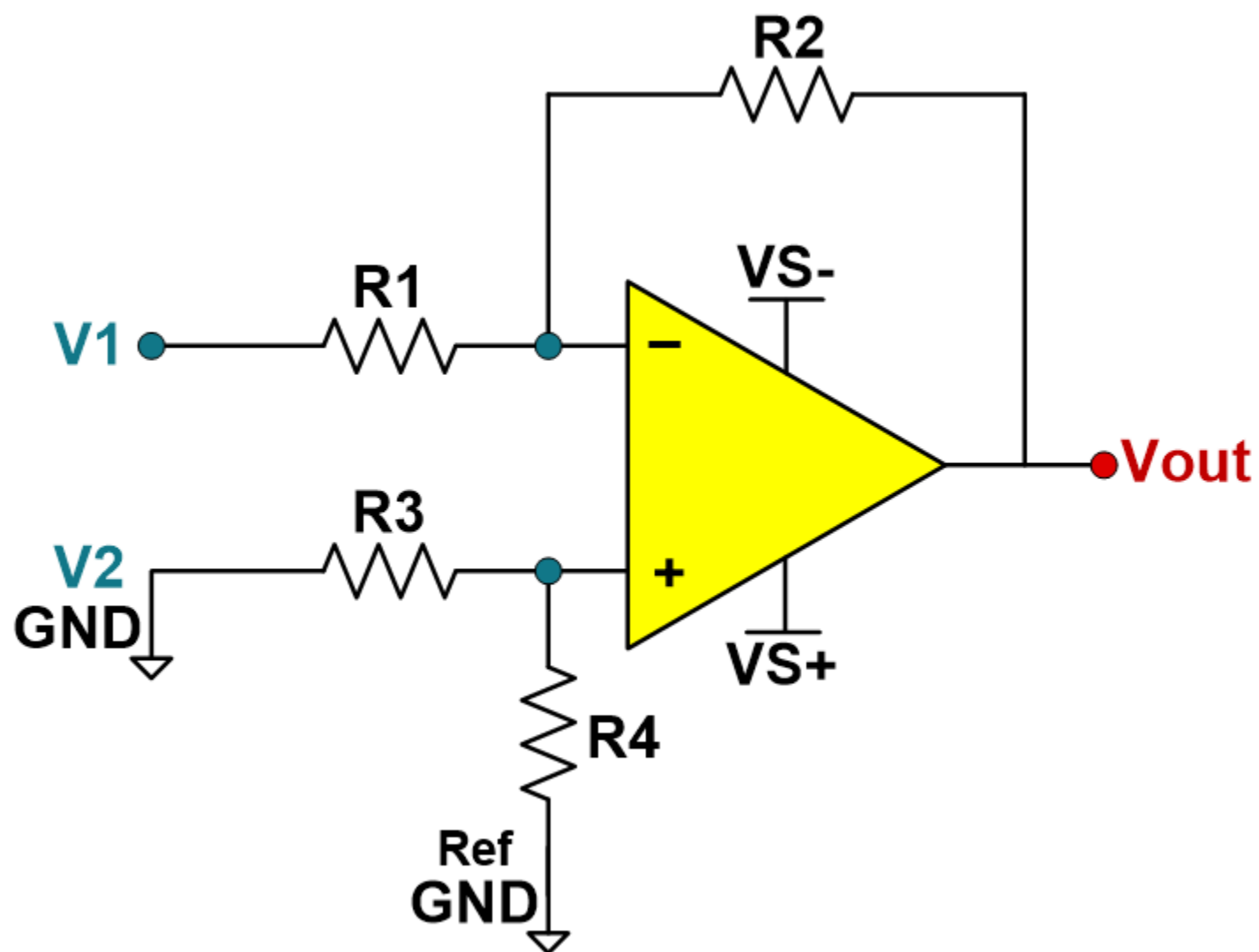
*“difference amplifier”*

A difference amplifier fulfills the primary behaviors of an idealized IA

Equation	V1	V2	Ref
V1*	Keep	Short	Short
V2*	Short	Keep	Short
Ref*	Short	Short	Keep

**$V_{out} = V1^* + V2^* + Ref^*$**

# Superposition – Derive $V_{out}$ due to $V_1$



Assume  $R_1 = R_2 = R_3 = R_4$

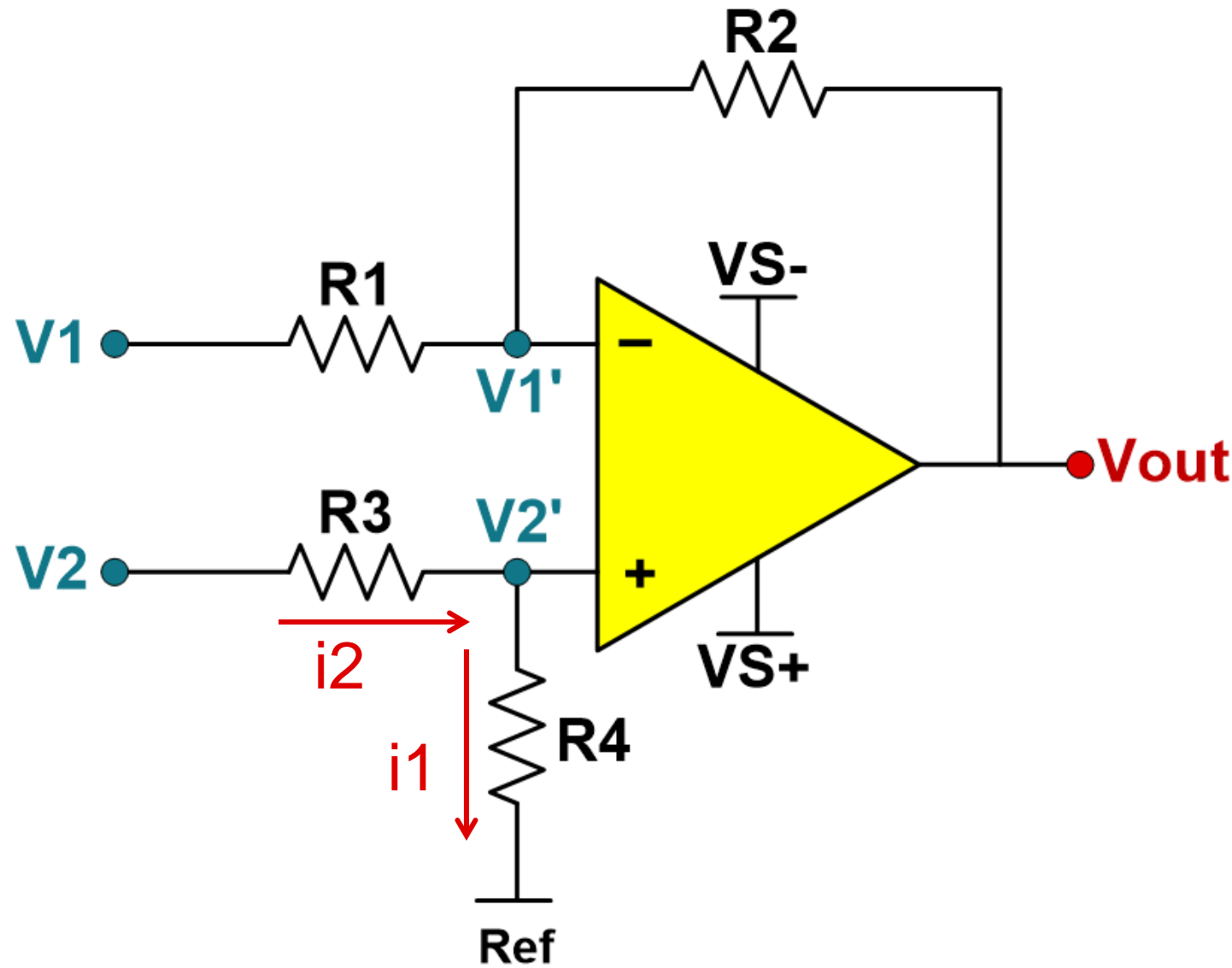
Ground the non-inverting input

$$V_{out} = V_1 \times \left( \frac{-R_2}{R_1} \right)$$

Since we assumed  $R_1 = R_2 = R_3 = R_4$ ,

$$V_{out} = -V_1 \text{ (Equation } V_1^*)$$

# Voltage between 2 sources – V2' derivation



$$i1 = \frac{V2' - Ref}{R4}$$

$$i2 = \frac{V2 - V2'}{R3}$$

$$i1 = i2 = \frac{V2' - Ref}{R4} = \frac{V2 - V2'}{R3}$$

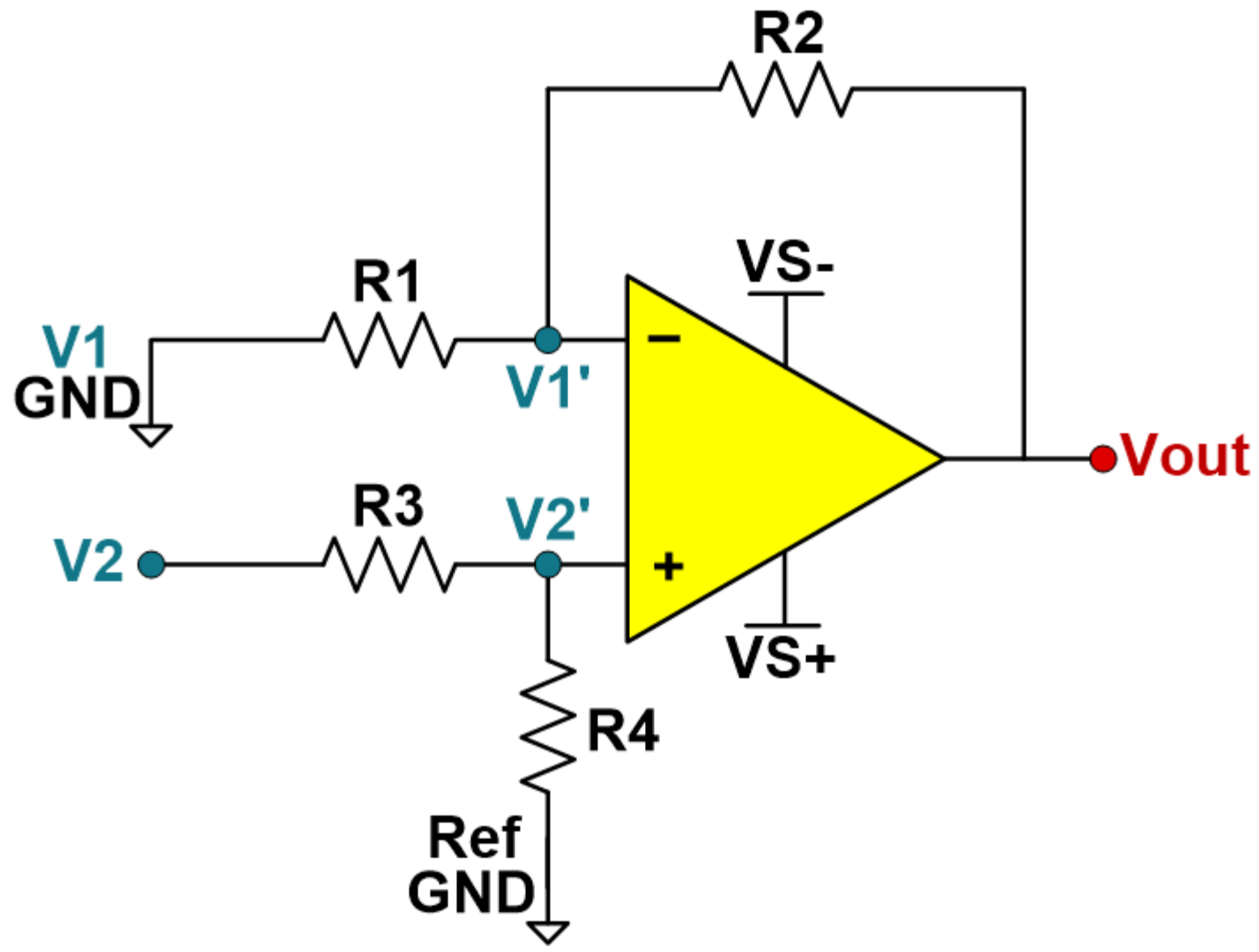
$$V2' = \frac{(R4 \times V2) + (R3 \times Ref)}{R3 + R4}$$

Since  $R1 = R2 = R3 = R4$ ,

$$V2' = \frac{V2 + Ref}{2}$$



# Superposition – Derive $V_{out}$ due to $V_2$



$$V_{out} = V_2' \times \left( 1 + \frac{R_2}{R_1} \right)$$

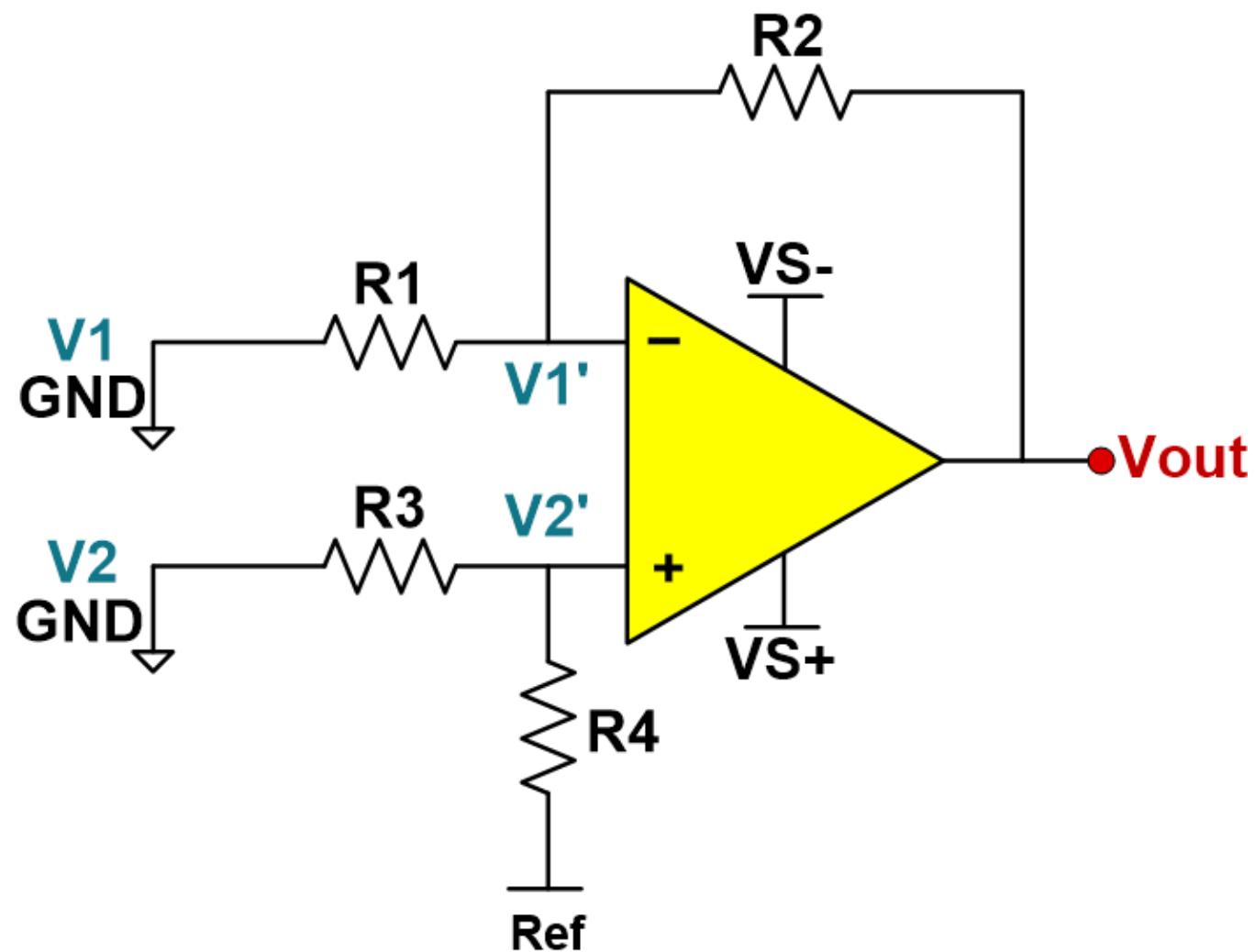
$$V_2' = \frac{Ref + V_2}{2}$$

$$V_{out} = \frac{Ref + V_2}{2} \times \left( 1 + \frac{R_2}{R_1} \right)$$

Since  $R_1 = R_2 = R_3 = R_4$ , and  $Ref = 0V$

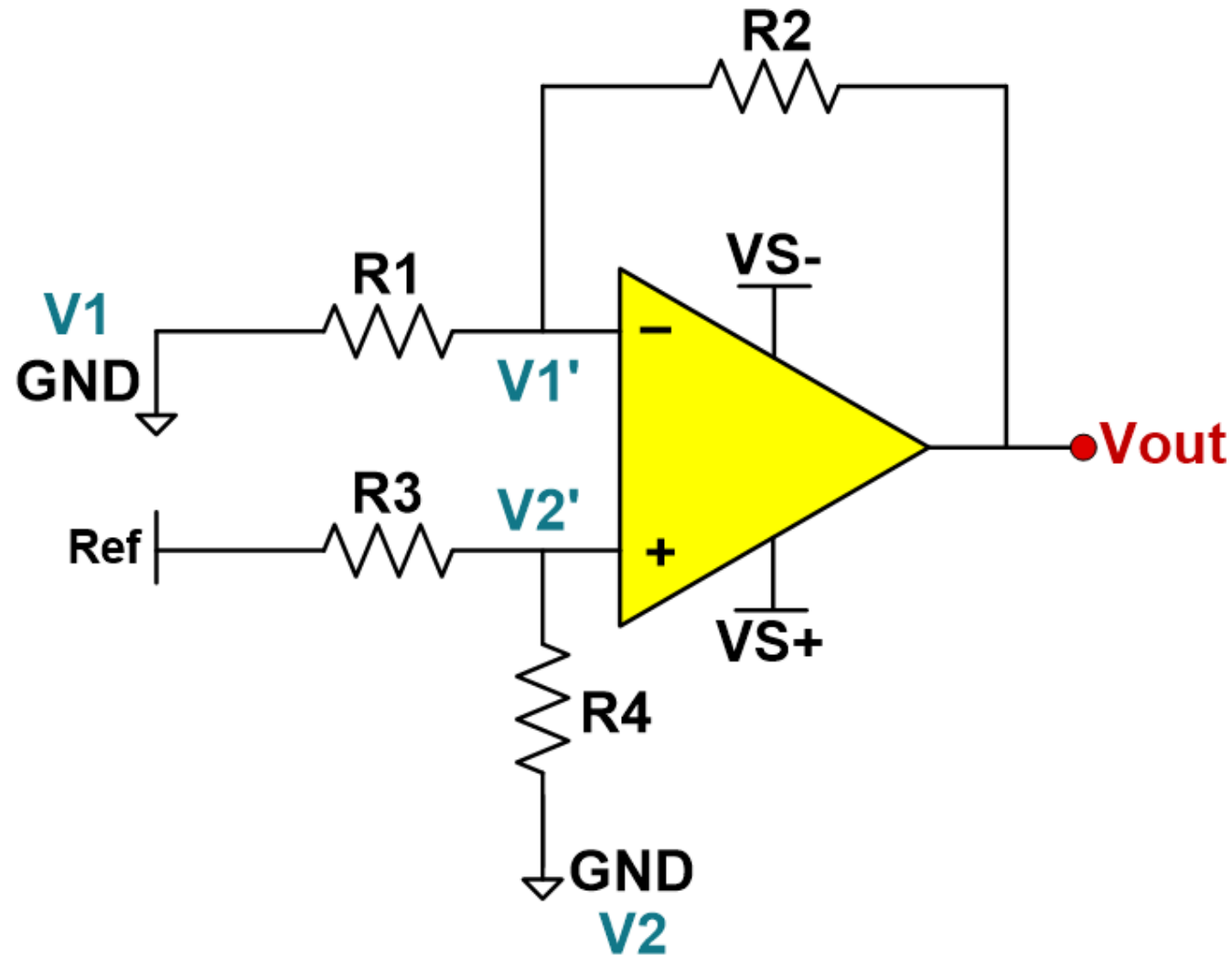
$$V_{out} = V_2 \text{ (Equation } V_2^*)$$

# Superposition – Ground V1 and V2



**Derive output due to Ref:**  
Ground inverting and non-inverting inputs  
Since  $R1 = R2 = R3 = R4$ ,  
Ref and  $V2$  are interchangeable

# Superposition – Ground V1 and V2



Looks like a non-inverting configuration with the following output equation:

$$V_{out} = \left(1 + \frac{R2}{R1}\right) \times V2'$$

$$V2' = \frac{R4}{R3 + R4} \times Ref$$

Since  $R1 = R2 = R3 = R4$ ,

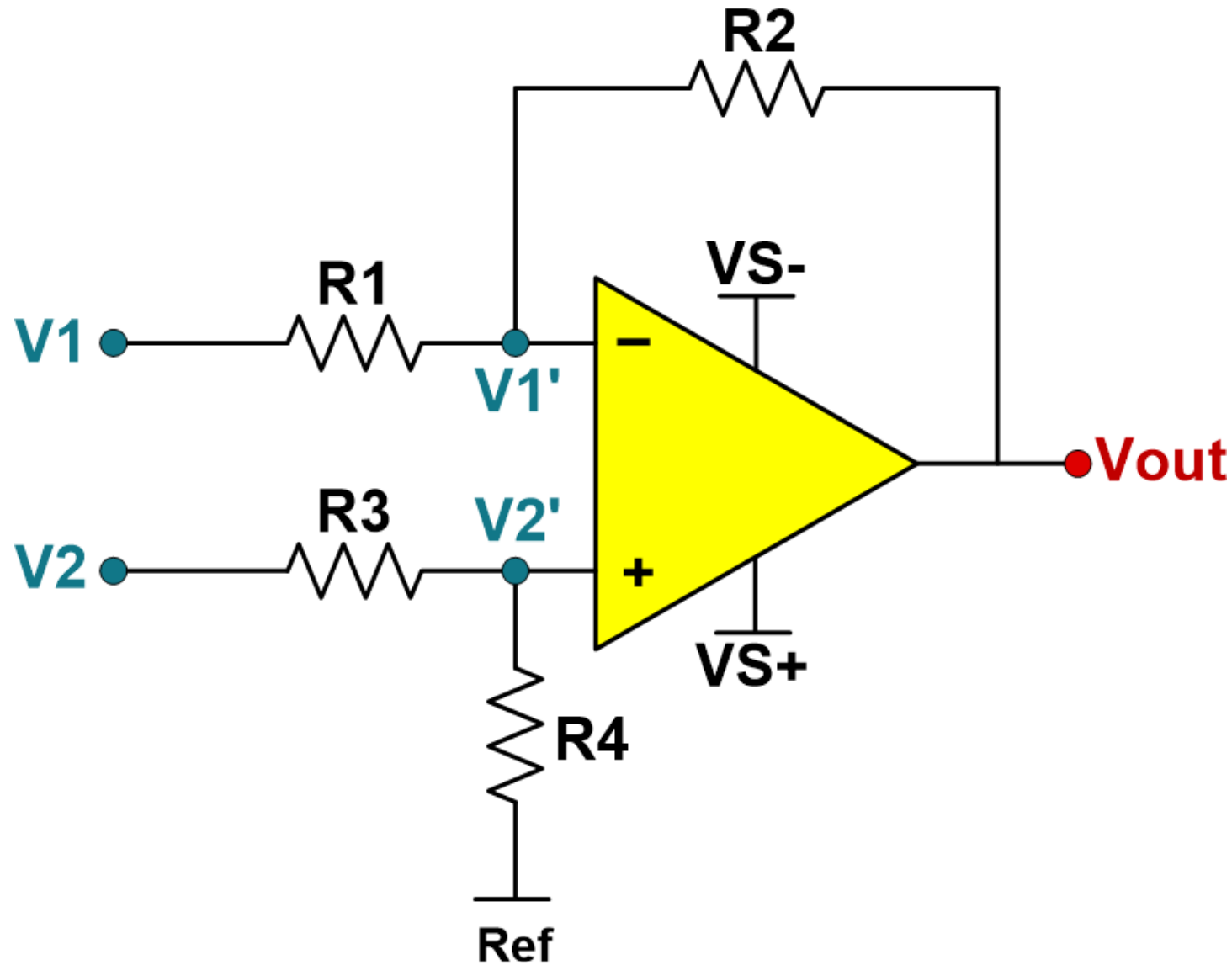
$$V2' = \frac{1}{2} \times Ref, \text{ and}$$

$$V_{out} = \left(1 + \frac{R2}{R1}\right) \times \frac{1}{2} \times Ref = Ref$$

**$V_{out} = Ref$  (Equation Ref\*)**



# One-amp IA topology – Ideal model analysis, $V_d$



	$V_1$	$V_2$	$Ref$
$V_1^* = -V_1$	Keep	Short	Short
$V_2^* = V_2$	Short	Keep	Short
$Ref^* = Ref$	Short	Short	Keep
$V_{out} = V_1^* + V_2^* + Ref^*$			

Combine Equations  $V_1^*$ ,  $V_2^*$  and  $Ref^*$ :

$$V_{out} = V_2 - V_1 + Ref$$

Where  $V_2 - V_1 =$  differential voltage,  $V_d$

# One-amp IA topology – Ideal model analysis, $V_{CM}$

$$V_{out} = V_2 - V_1 + Ref$$

$$(V_2 - V_1) = V_d$$

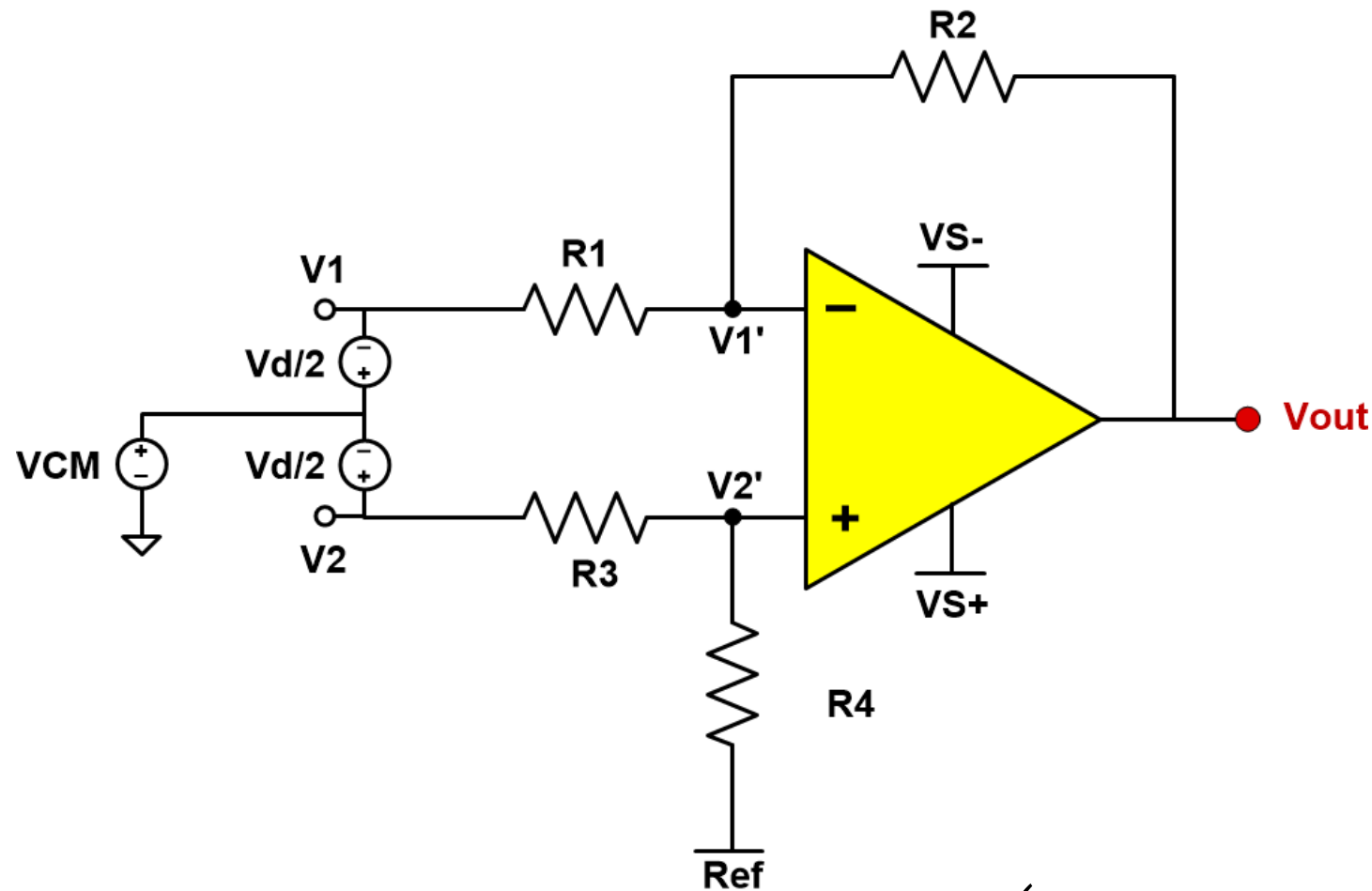
Common mode rejection analysis:

Common mode input voltage is equal at each input

$$V_1 = V_{CM} - \frac{V_d}{2}$$

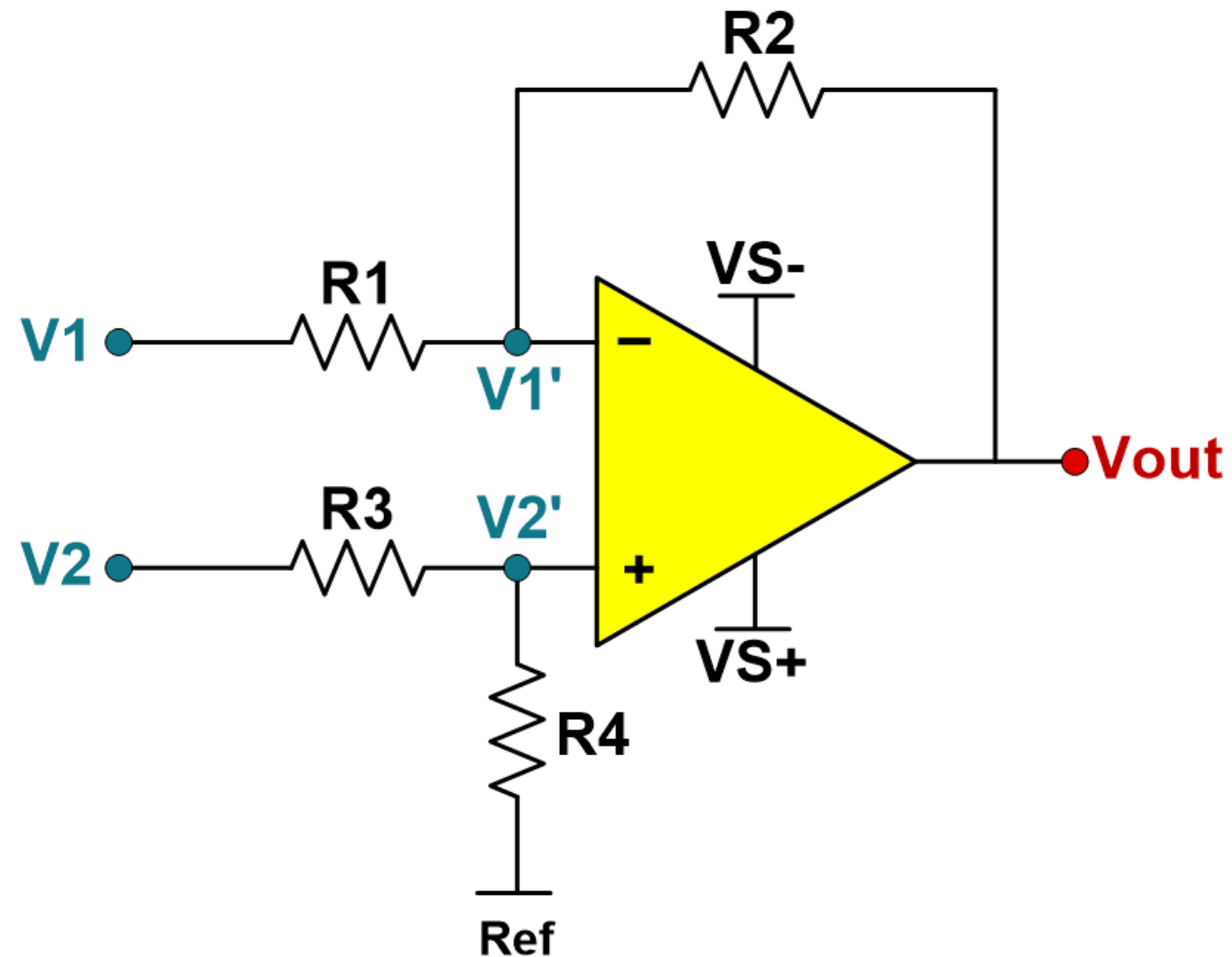
$$V_2 = V_{CM} + \frac{V_d}{2}$$

$$V_{out} = V_2 - V_1 + Ref = \left( V_{CM} + \frac{V_d}{2} \right) - \left( V_{CM} - \frac{V_d}{2} \right) + Ref = V_d + Ref$$

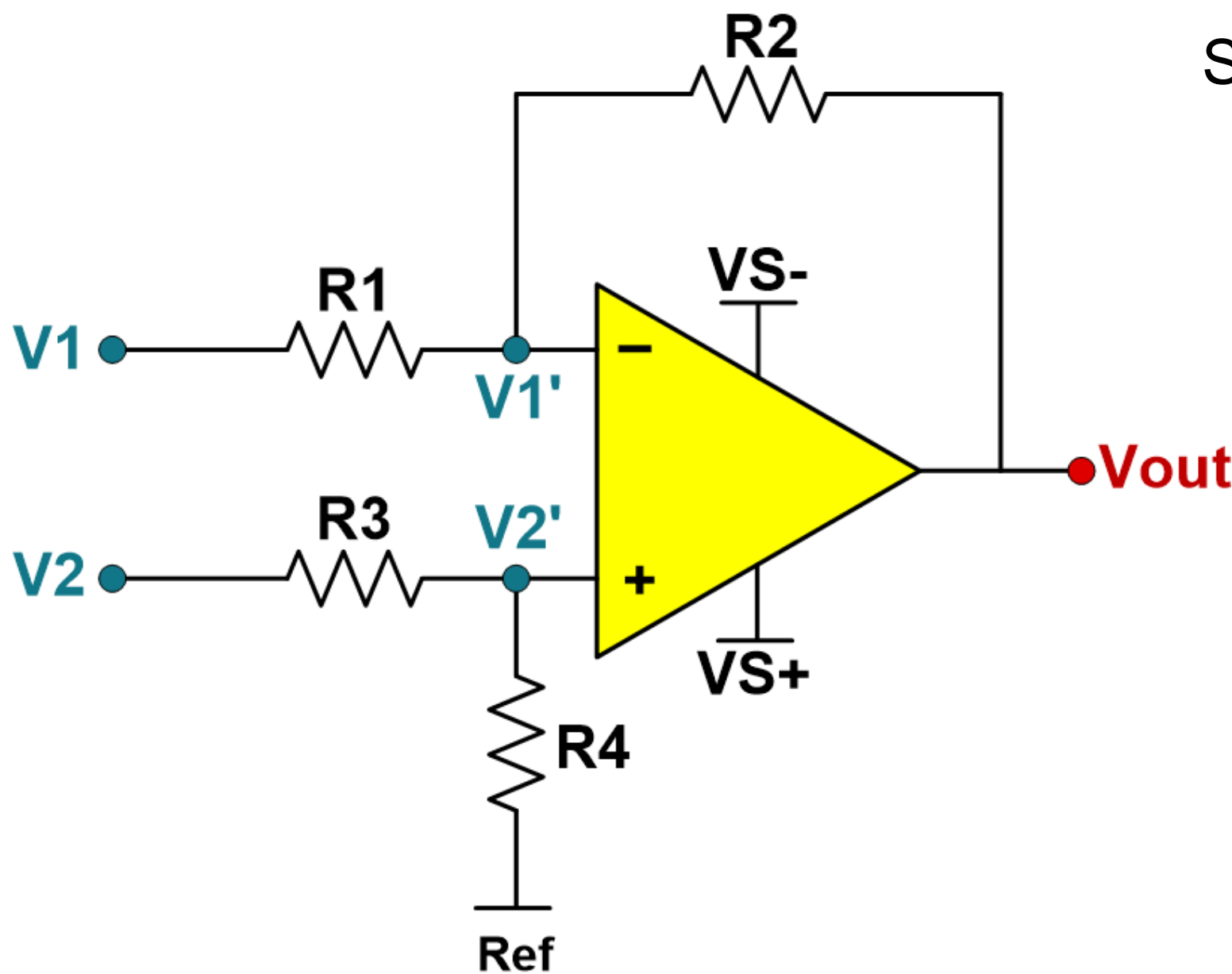


# One-amp IA topology – General equation

$$V_{out} = \left( -V_1 \times \frac{R_2}{R_1} \right) + \left( \text{Ref} + (V_2 - \text{Ref}) \times \frac{R_4}{R_3 + R_4} \right) \times \left( \frac{R_1 + R_2}{R_1} \right)$$



# One-amp IA topology – Simplified equation



Simplified equation:

*“Differential gain, Ad”*

$$V_{out} = \left( \frac{R2}{R1} \right) \times (V2 - V1) + Ref$$

*“Differential input voltage, V<sub>d</sub>”*

$$V_{out} = A_d \times V_d + Ref$$

# Bandwidth – Noise gain versus signal gain

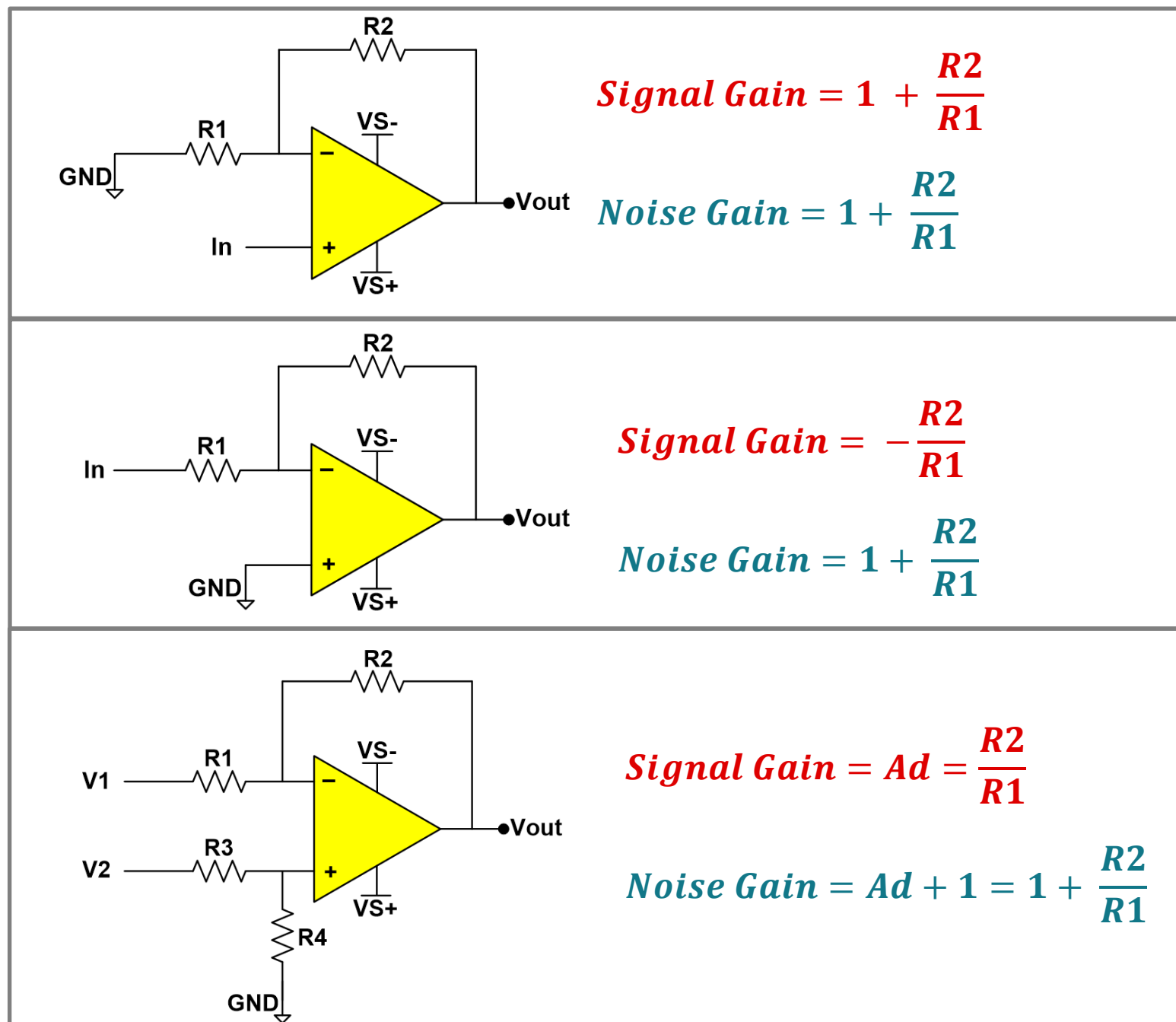
## Gain – two types:

### 1. Signal gain:

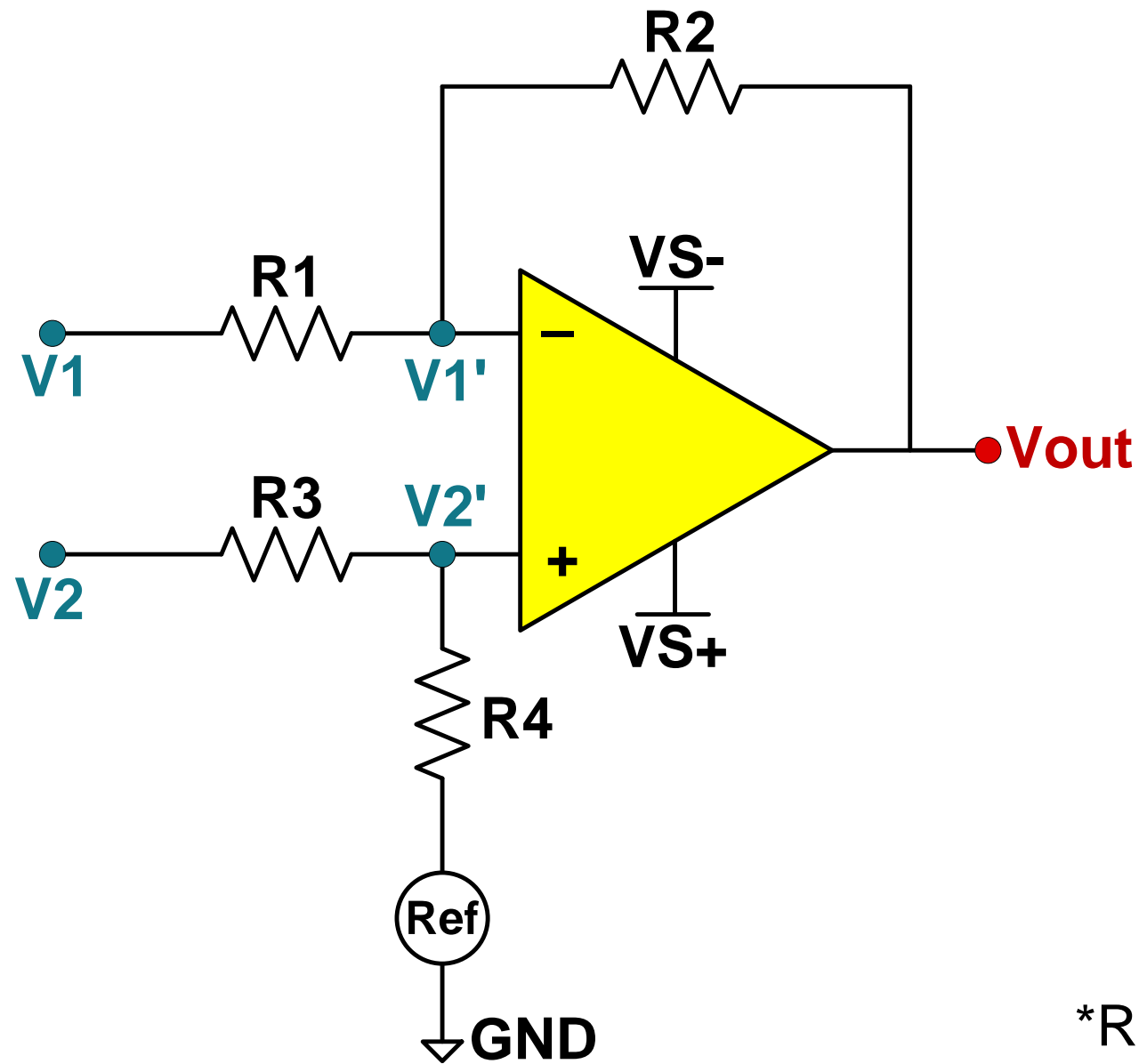
- Determines the input-output relationship
- Dependent on amplifier configuration
- Defined as  $A_d$  in an difference amplifier

### 2. Noise gain:

- Non-inverting gain of the amplifier
- Determines bandwidth, stability, and more
  - $GBW = \text{Noise gain} * BW$
- Noise gain =  $1 + A_d$  for the difference amplifier



# One-amp IA topology – General equation



General equation:

*“Differential gain, Ad”*

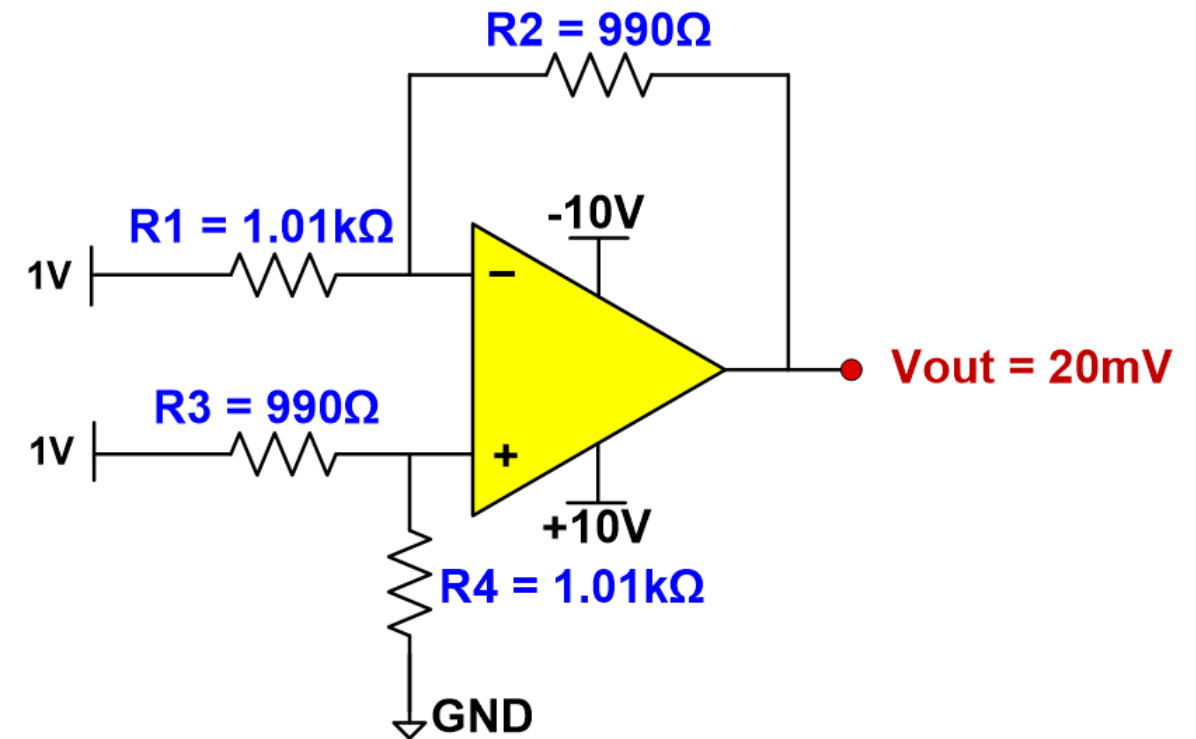
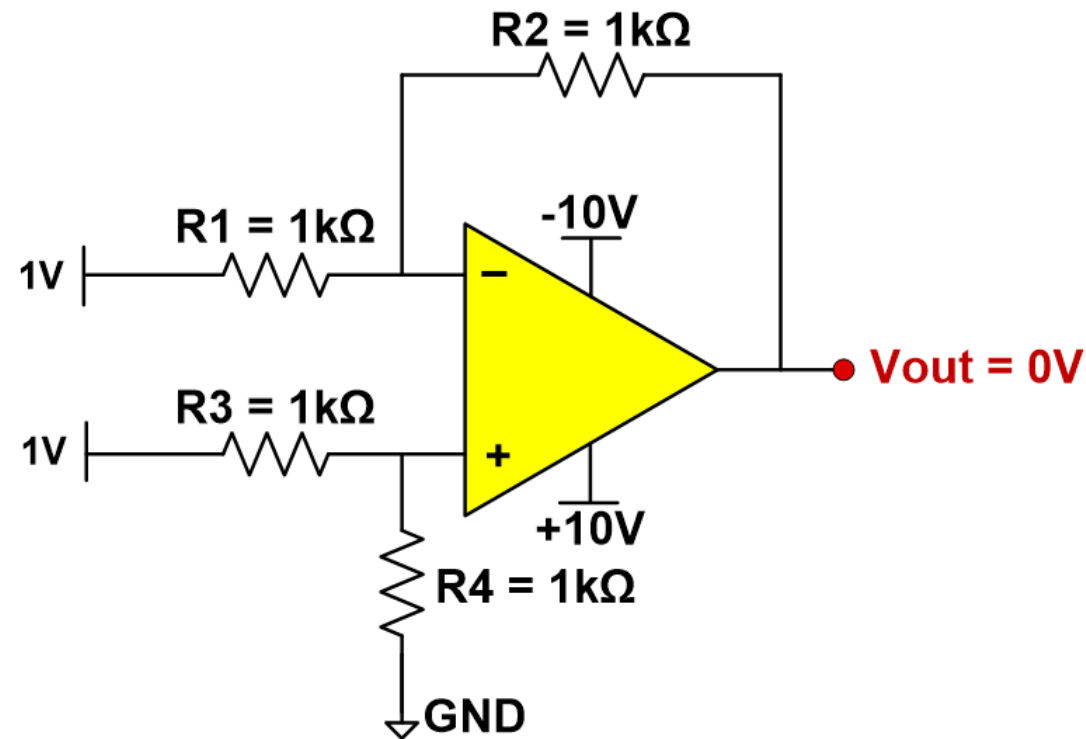
$$V_{out} = \left( \frac{R2}{R1} \right) \times (V2 - V1) + Ref$$

*“Differential input voltage, V<sub>d</sub>”*

\*Resistors cannot be perfectly matched so  
R1 ≠ R2 ≠ R3 ≠ R4 and CMRR will be degraded!\*



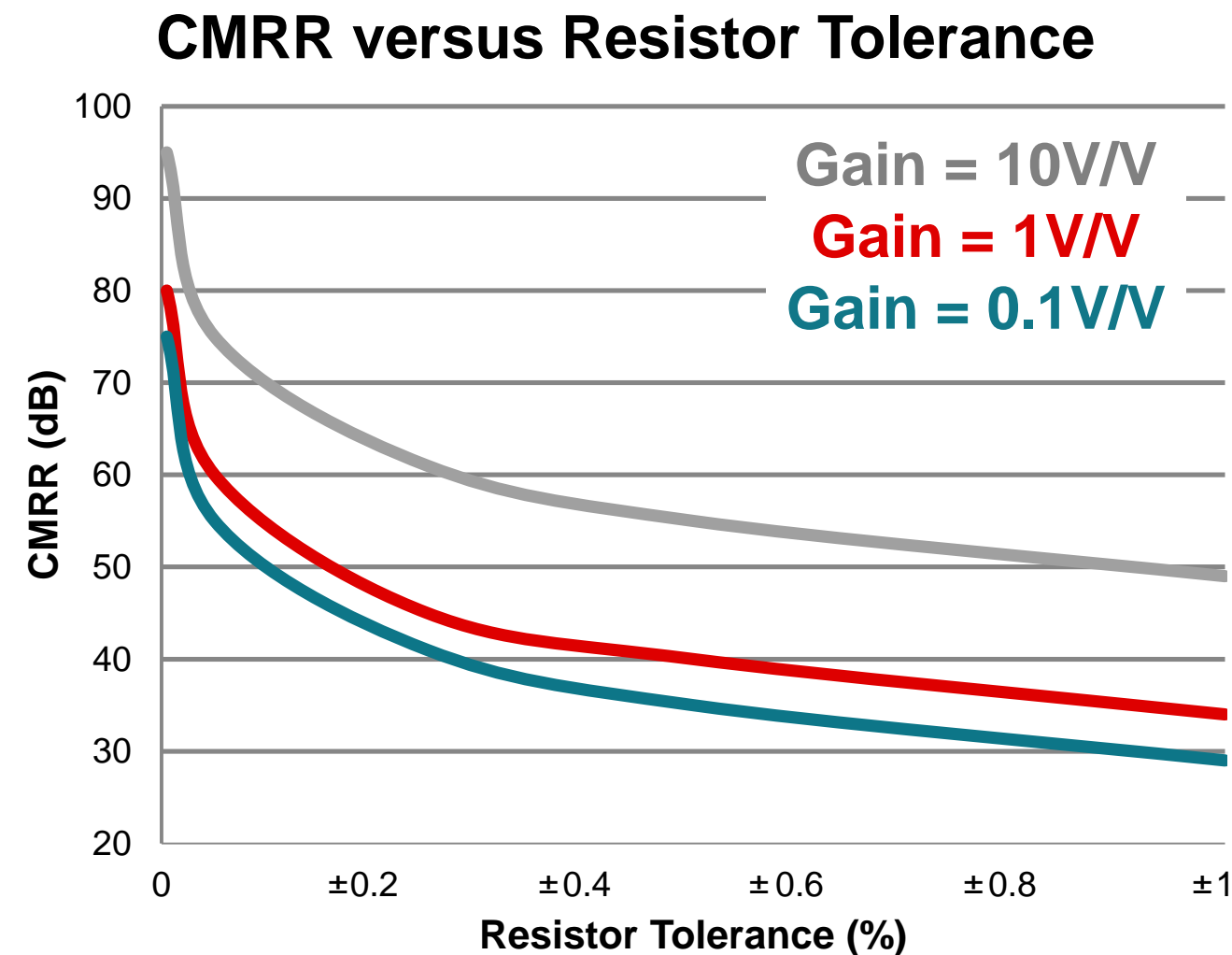
# Resistor matching – Mismatch effect



$$CMRR = 20 \times \log_{10} \left( \frac{1}{\Delta V_{CM}} \right) = 20 \times \log_{10} \left( \frac{1}{20m} \right)$$
$$CMRR = 34dB$$

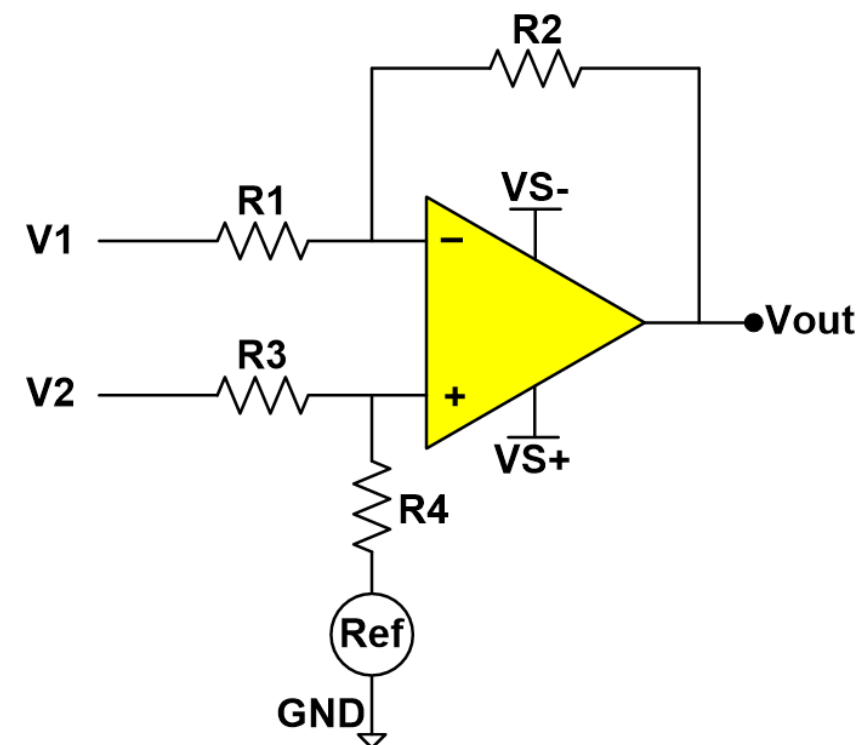
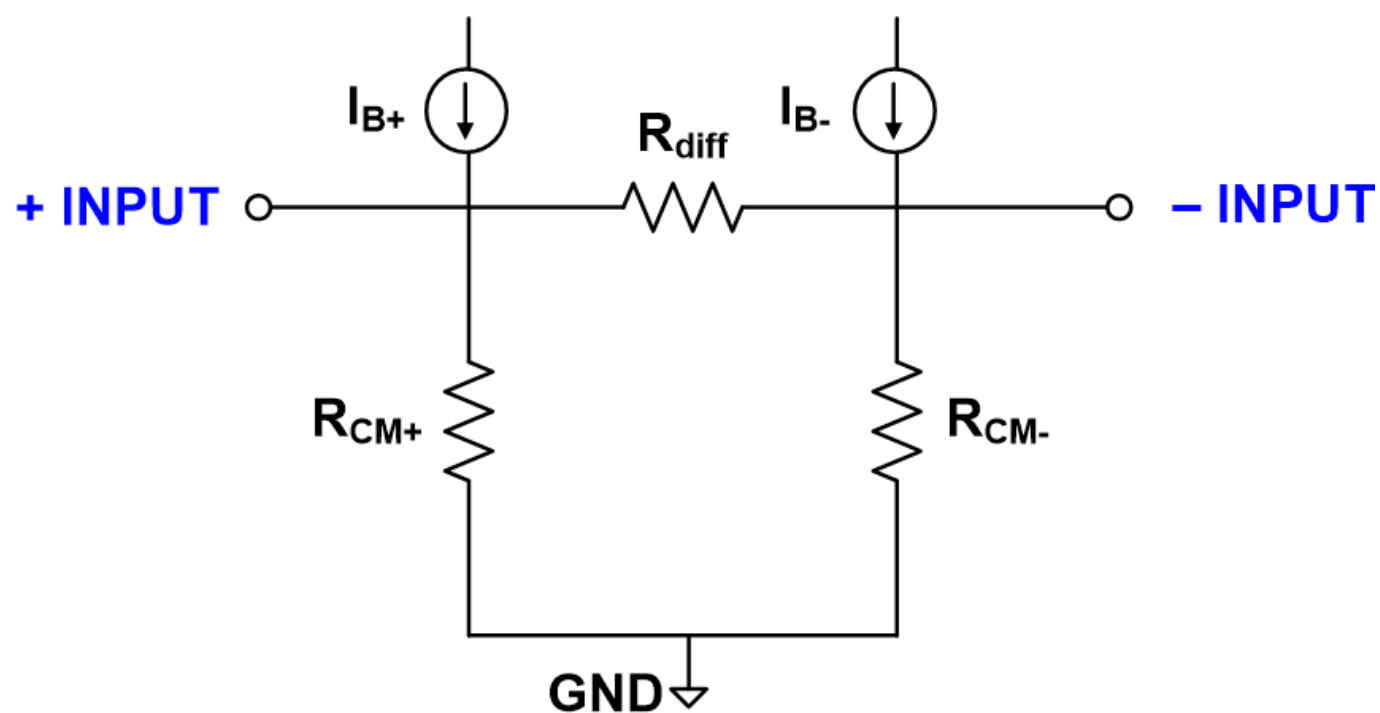
# Resistor analysis – CMRR performance

Resistor tolerance mismatch	CMRR Gain = 1V/V	CMRR Gain = 10V/V	CMRR Gain = 0.1V/V
±1%	34dB	49dB	29dB
±0.5%	40dB	55dB	35dB
±0.25%	46dB	61dB	41dB
±0.1%	54dB	69dB	49dB
±0.05%	60dB	75dB	55dB
±0.005%	80dB	95dB	75dB

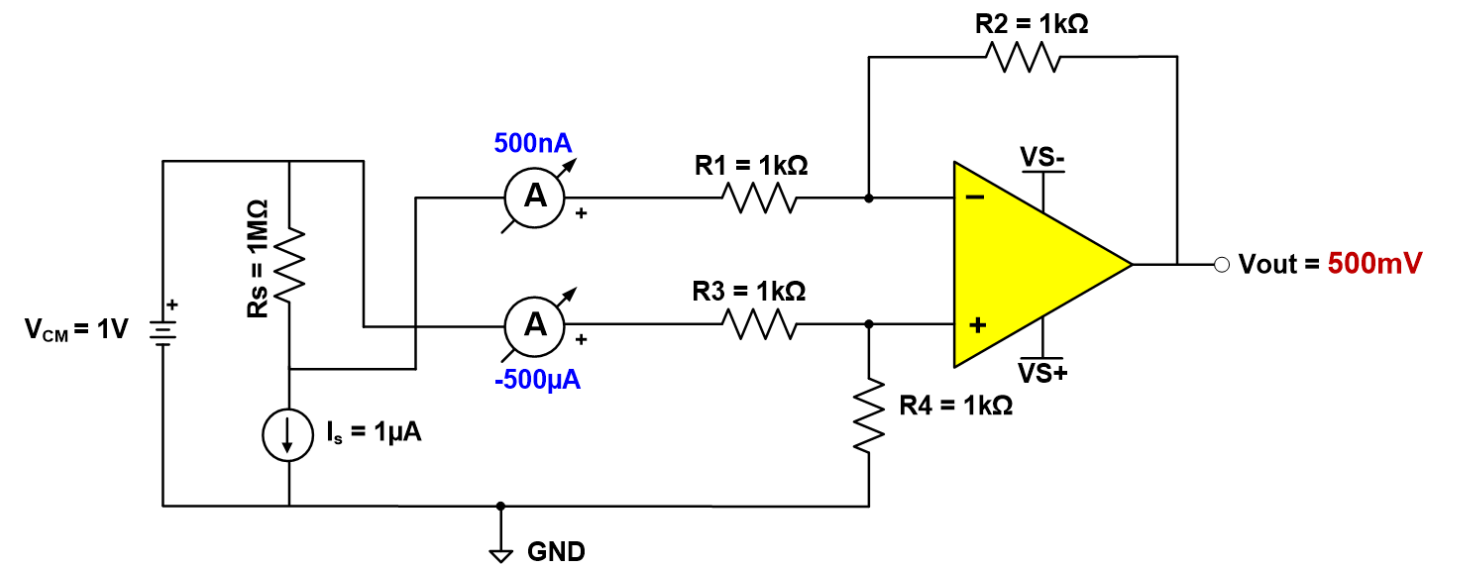
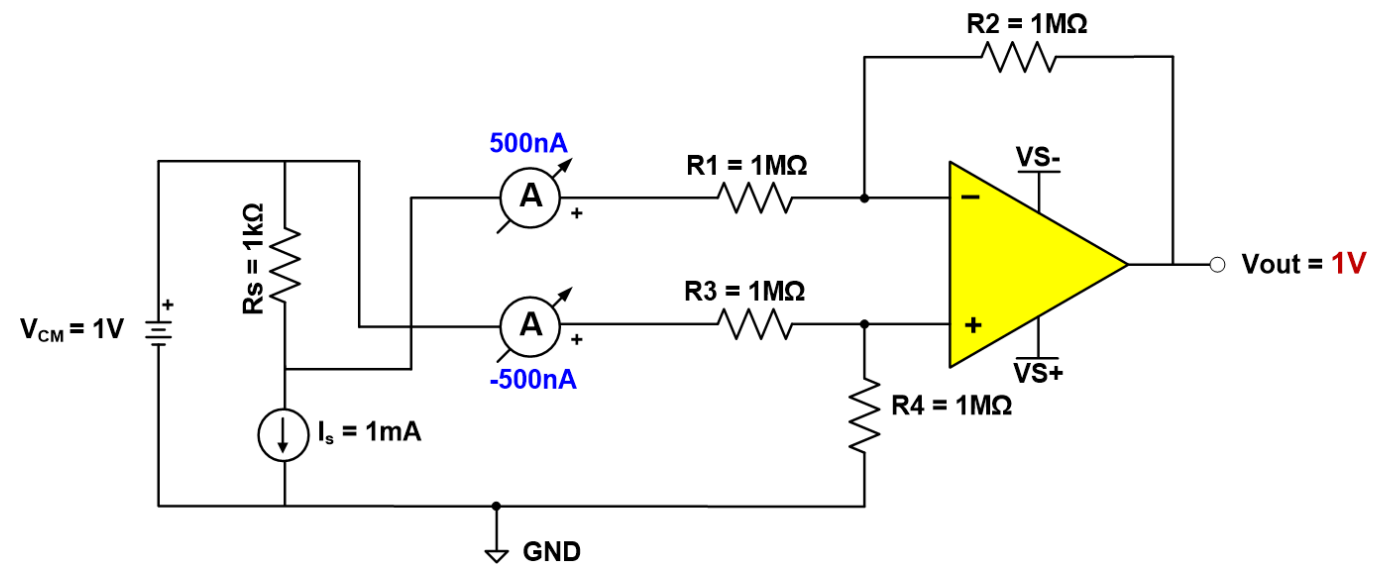
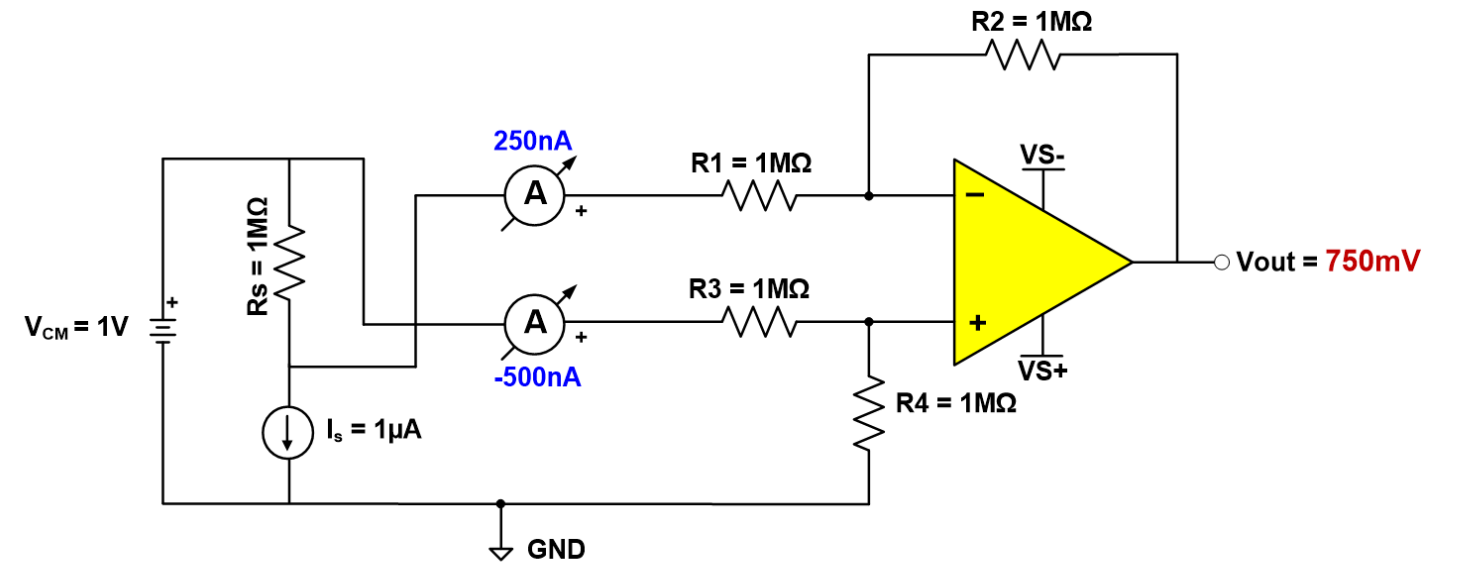
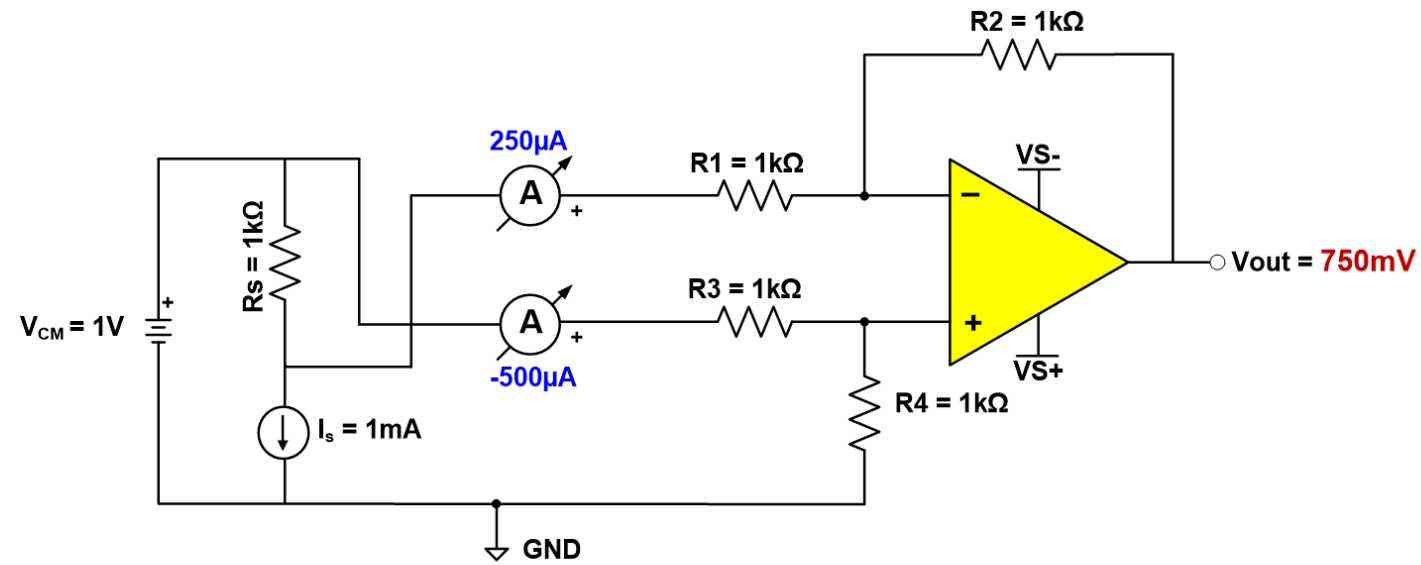


# Difference amplifier – Input impedance

- **Input impedance:** change of input voltage divided by the corresponding change in input current.
- Two types:
  1. Differential input impedance:  $R_{diff} = R1 + R3$
  2. Common mode input impedance:  $R_{cm+}$  and  $R_{cm-} = (R3+R4) || (R1+R2)$

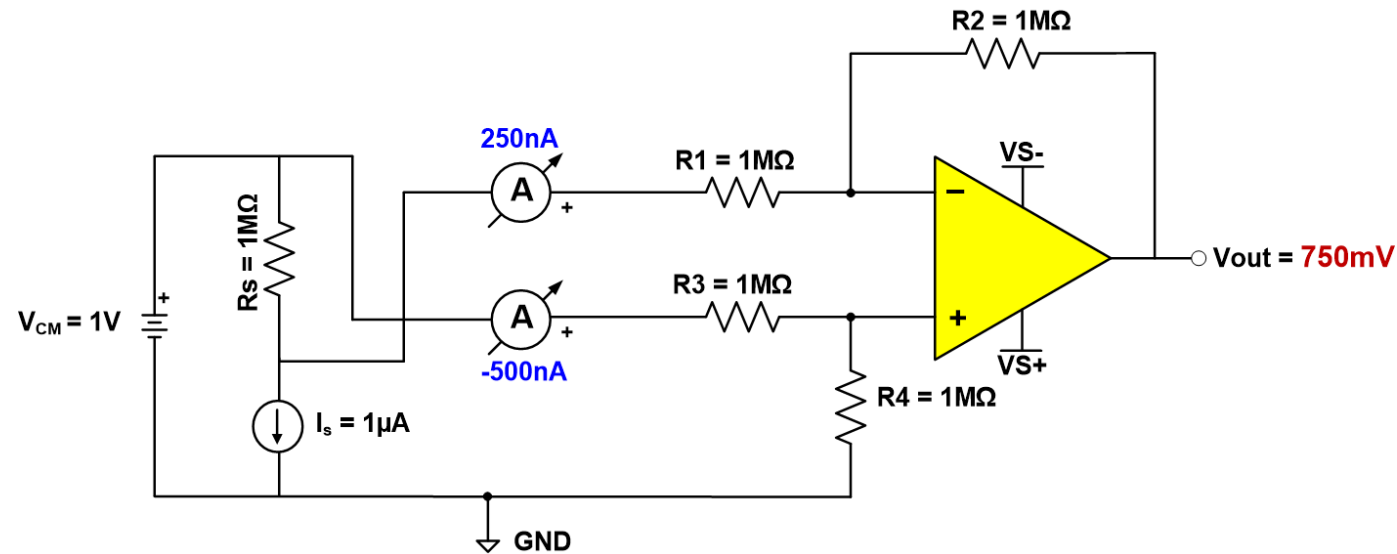


# Input impedance – Current sensing



**Rule-of-thumb:**  $R_{IN_{DA}} \geq 100 \times R_{OUT_{Source}}$

# Input impedance – Current sensing cont'd



Differential input impedance:  $R_{diff} = R1 + R3$

$$R_{diff} = R_s + R1 + R3 = 3M\Omega$$

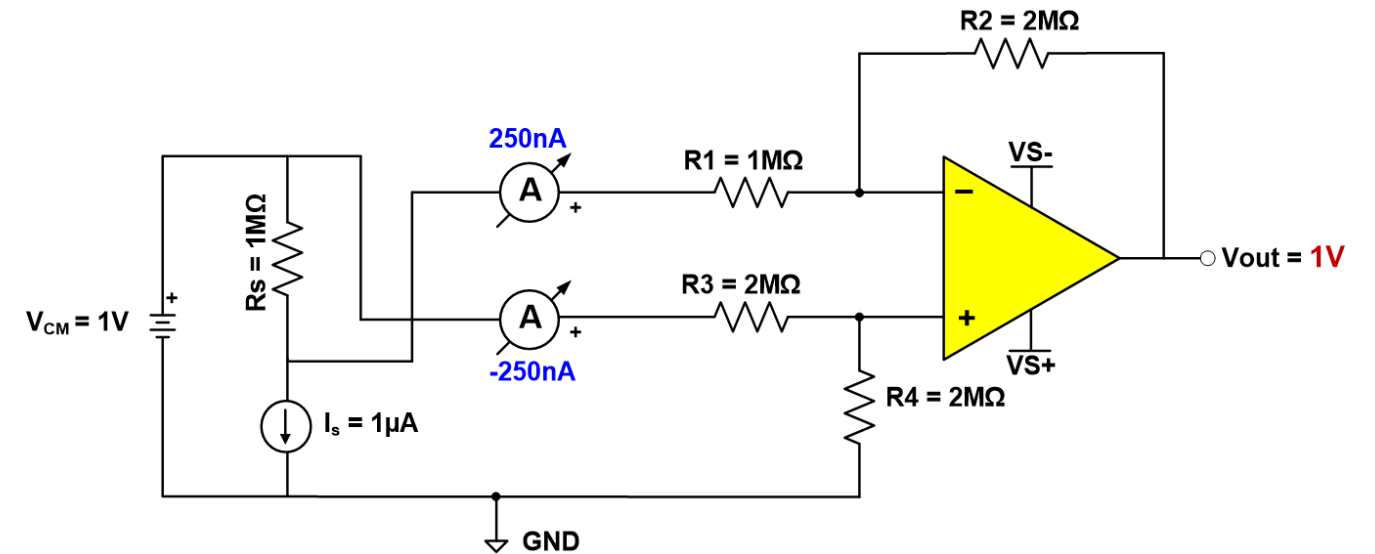
$$R_{diff-} = R_s + R1 = 2M\Omega$$

$$R_{diff+} = R3 = 1M\Omega$$

Common mode input impedance:  $R_{cm+}$  and

$$R_{cm-} = (R3+R4) \parallel (R1+R2+R_s)$$

$$R_{cm} = 1.2M\Omega$$



Differential input impedance:  $R_{diff} = R1 + R3$

$$R_{diff} = R_s + R1 + R3 = 4M\Omega$$

$$R_{diff-} = R_s + R1 = 2M\Omega$$

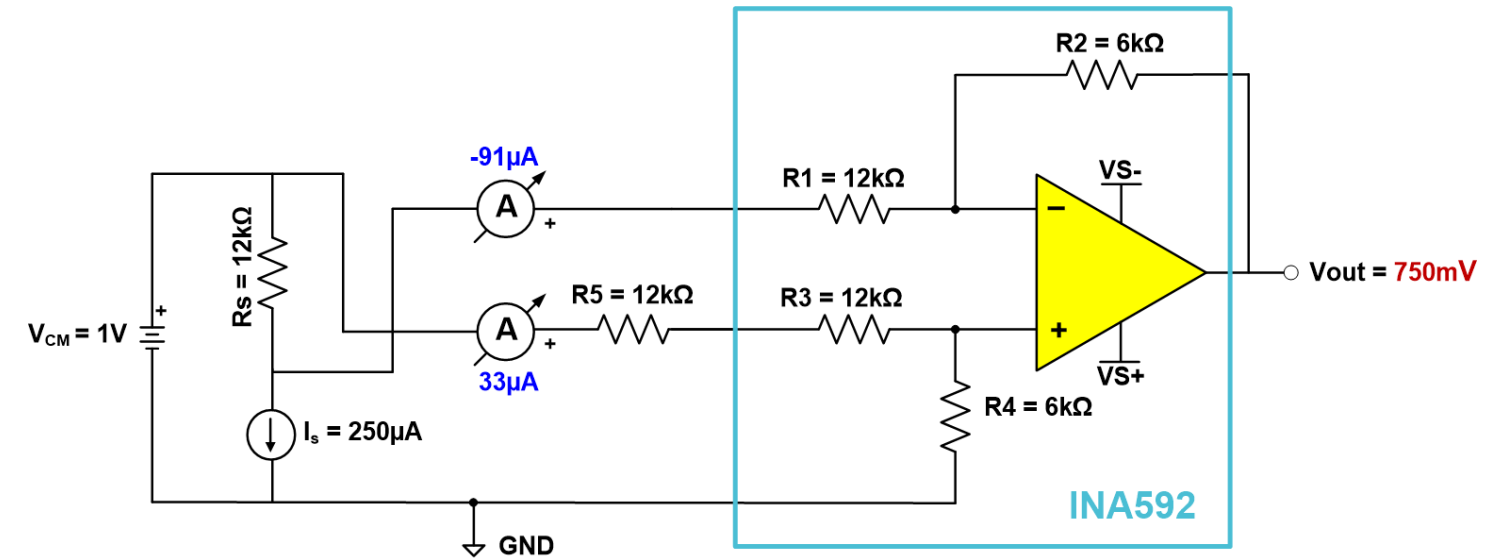
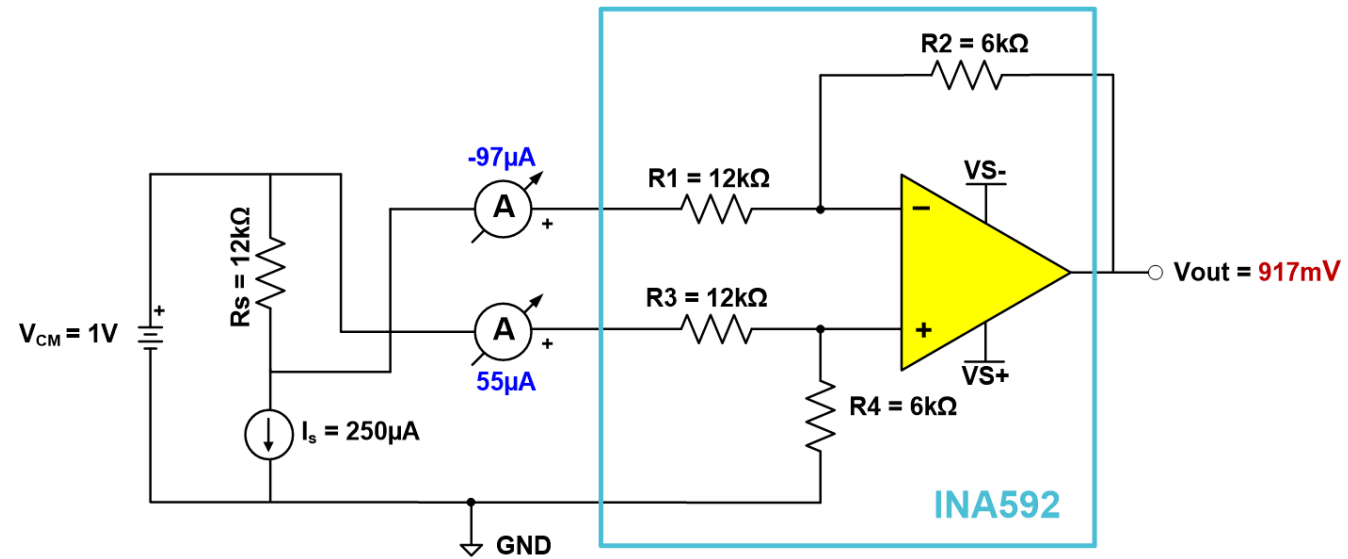
$$R_{diff+} = R3 = 2M\Omega$$

Common mode input impedance:  $R_{cm+}$  and

$$R_{cm-} = (R3+R4) \parallel (R1+R2+R_s)$$

$$R_{cm} = 2M\Omega$$

# Input impedance – Current sensing cont'd



Differential input impedance:

$$R_{diff} = R_s + R_1 + R_3 = 36k\Omega$$

$$R_{diff-} = R_s + R_1 = 24k\Omega$$

$$R_{diff+} = R_3 = 12k\Omega$$

Common mode input impedance:  $R_{cm+}$  and

$$R_{cm-} = (R_3 + R_4) \parallel (R_1 + R_2 + R_s)$$

$$R_{cm} = 11.25k\Omega$$

Differential input impedance:

$$R_{diff} = R_s + R_1 + R_3 = 36k\Omega$$

$$R_{diff-} = R_s + R_1 = 24k\Omega$$

$$R_{diff+} = R_3 + R_5 = 24k\Omega$$

Common mode input impedance:  $R_{cm+}$  and

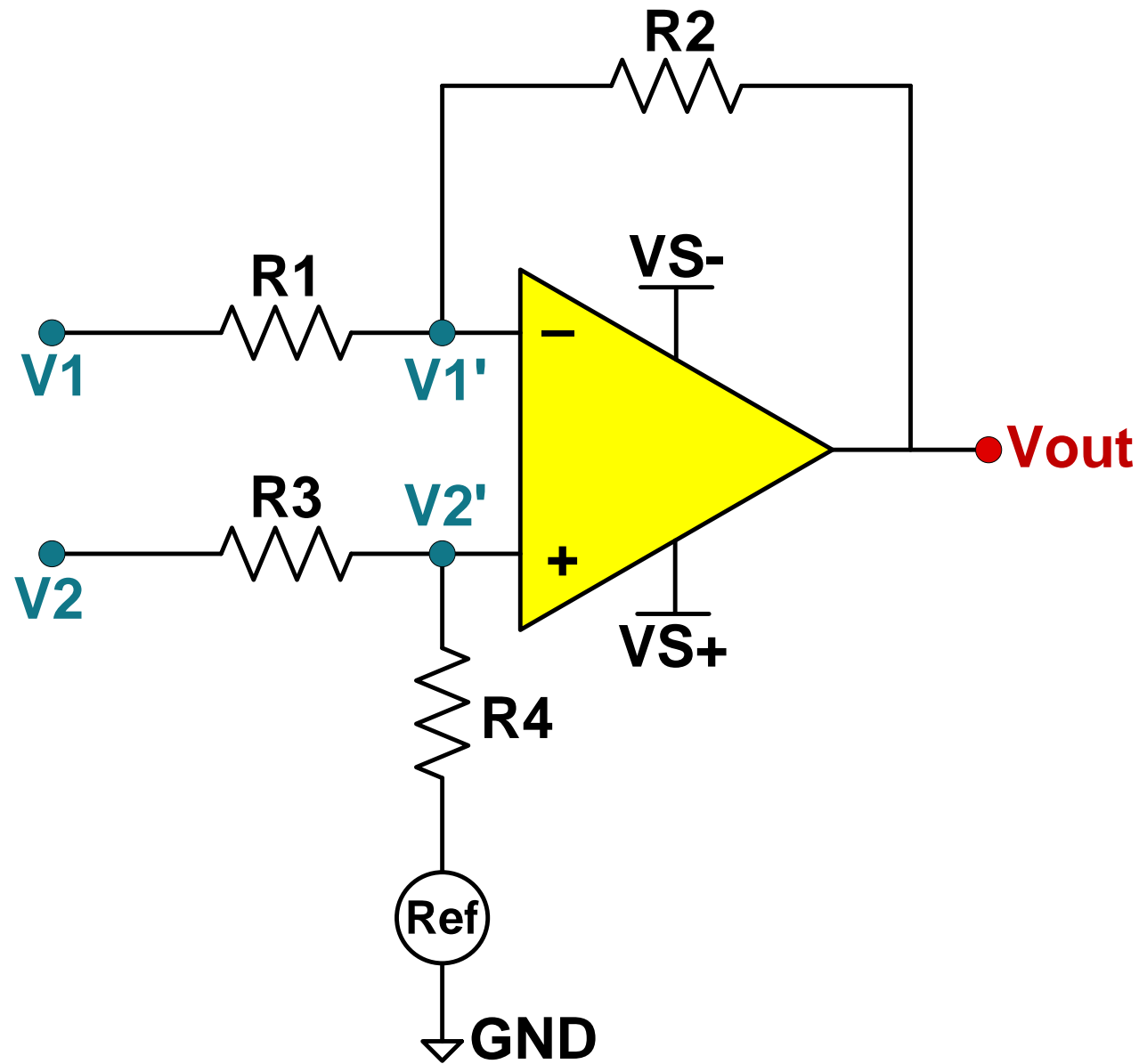
$$R_{cm-} = (R_3 + R_4 + R_5) \parallel (R_1 + R_2 + R_s)$$

$$R_{cm} = 15k\Omega$$

$$V_{out} = V_d \times A_d = 3V \times \frac{1}{4} V/V = 750mV$$



# One amp IA topology – Design summary



## Design challenges:

- ▶ Low input impedance
- ▶ Challenge to match resistances

## Summary:

If you have an application where you have low impedance sources and high common mode voltages, consider a one-amp IA (difference amplifier) topology

**Thanks for your time!**  
**Please try the quiz.**

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# Quiz: Instrumentation Amplifier (IA) topologies: one-amp

TI Precision Labs – Instrumentation Amplifiers

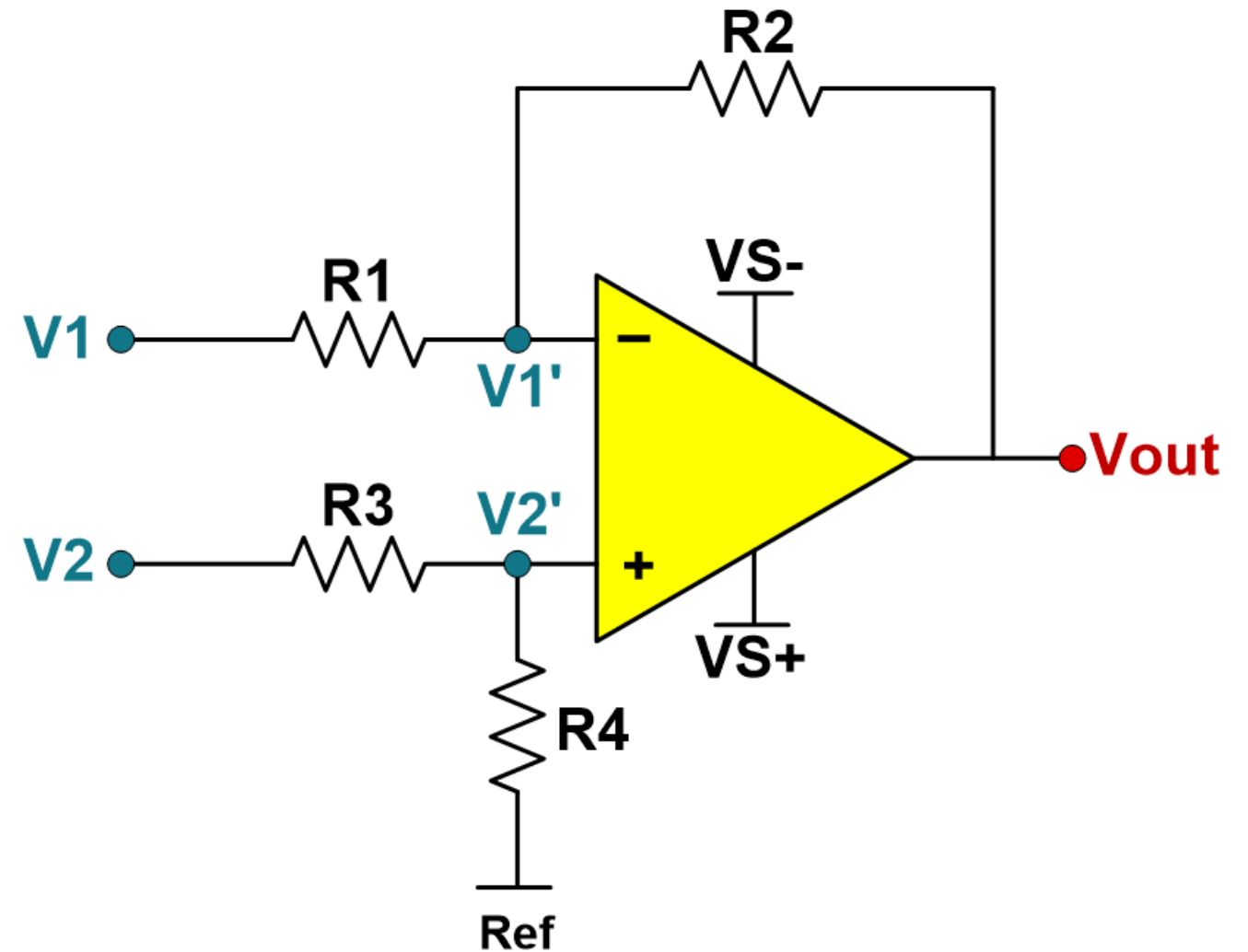
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# Quiz: (IA) topologies: one-amp || Question

1. What is the output equation of a one-amp IA assuming all resistances are equal to each other?

- a)  $V_{out} = V2 \times V1$
- b)  $V_{out} = V2 - V1 + Ref$
- c)  $V_{out} = Ref \times (V2 - V1)$
- d)  $V_{out} = V1 \times V2 \times Ref$



# Quiz: (IA) topologies: one-amp || Answer

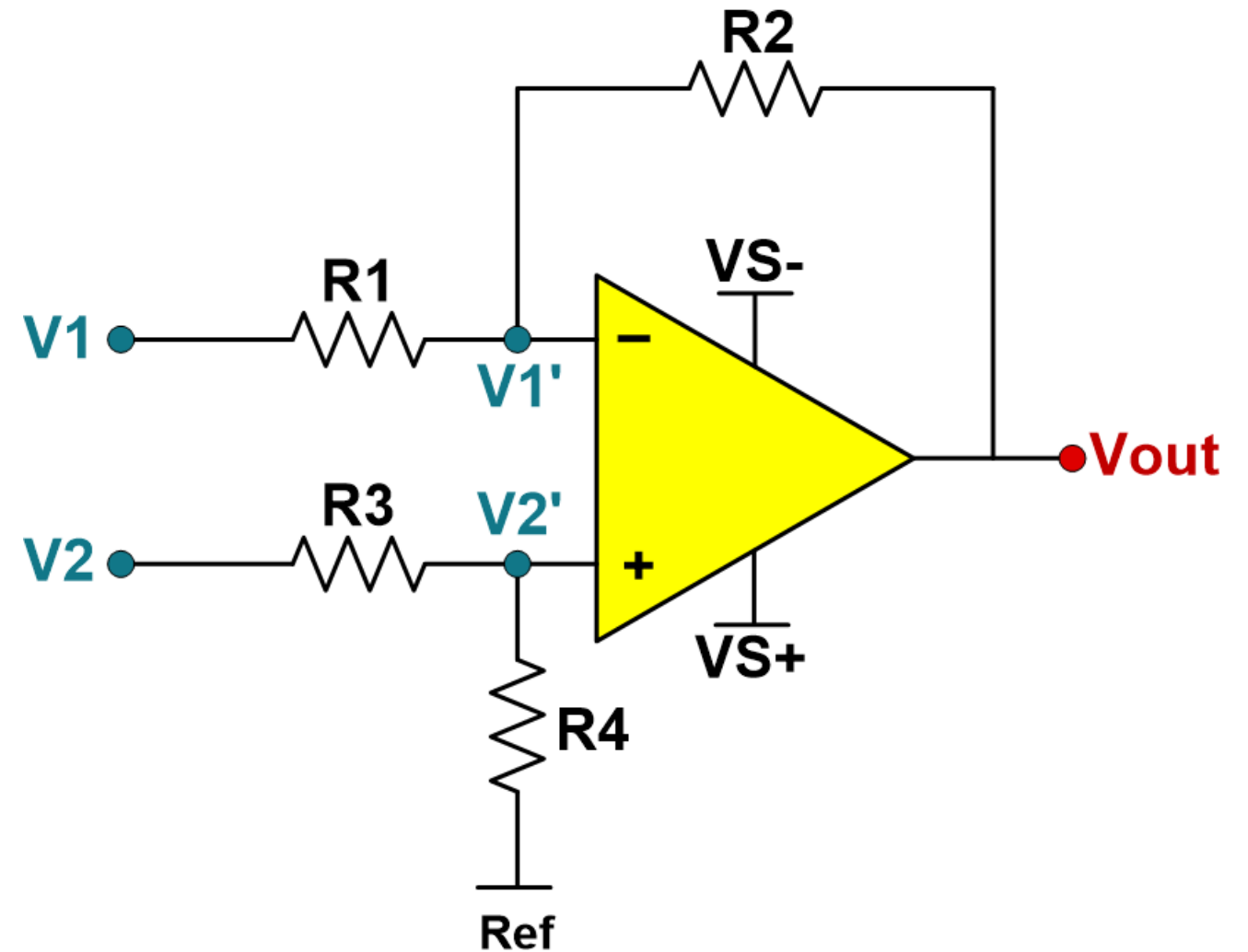
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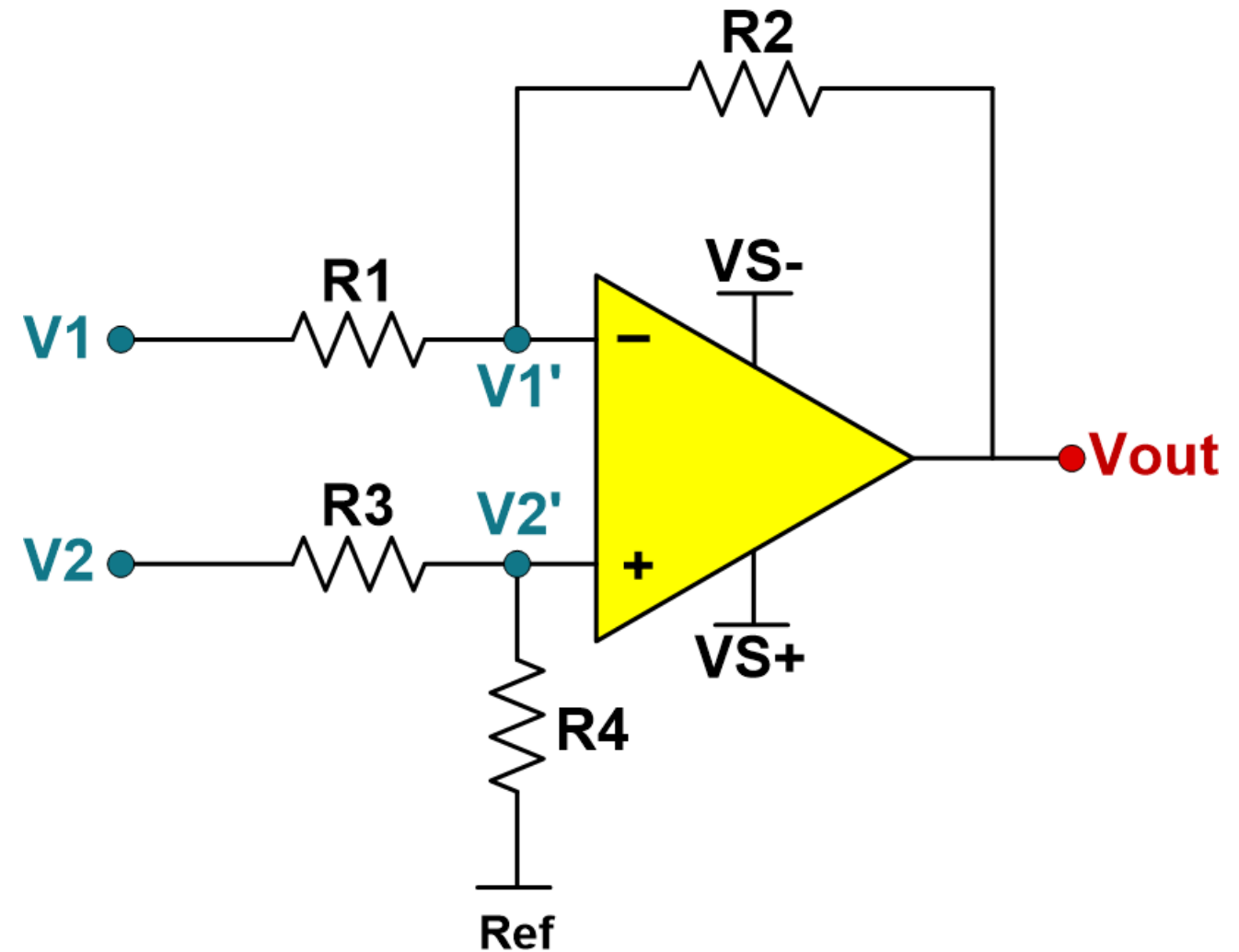




# Quiz: (IA) topologies: one-amp || Question

2. If we match R1 to R3 and R2 to R4, what is the differential gain ( $A_d$ ) of the following circuit?

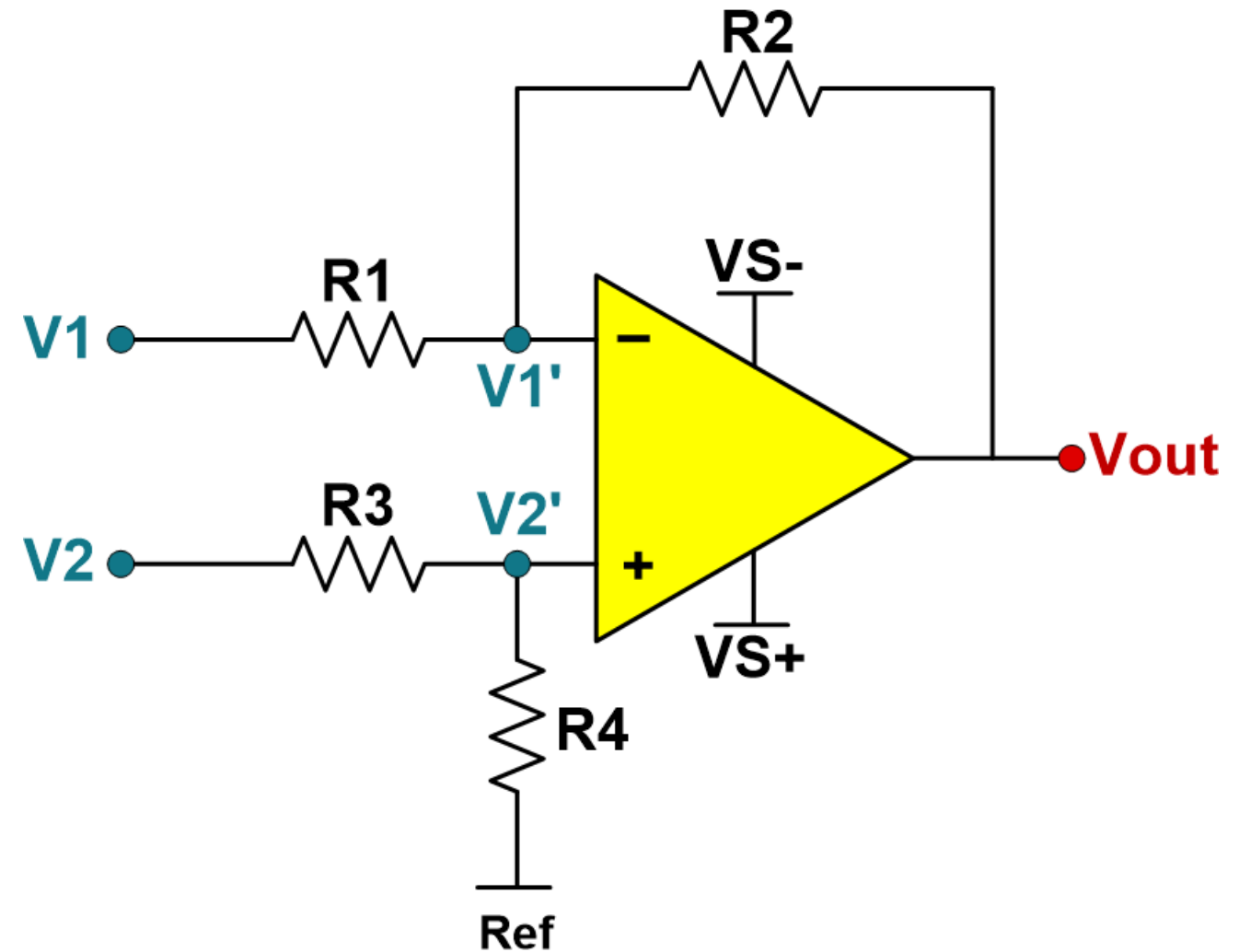
- a)  $A_d = R2 / R1$
- b)  $A_d = R1 \times R2$
- c)  $A_d = R1 / R2$
- d)  $A_d = R3 / R4$



# Quiz: (IA) topologies: one-amp || Answer

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- c)  $A_d = R1 / R2$
- d)  $A_d = R3 / R4$



# Quiz: (IA) topologies: one-amp || Question

3. Which of the following statements is true of signal gain and noise gain?
- a) Signal gain determines the bandwidth of the circuit, and noise gain is the non-inverting gain of the amplifier
  - b) Signal gain is dependent on the amplifier's configuration and determines the input-output relationship.
  - c) The noise gain of a circuit determines many features of the amplifier, including bandwidth and stability, and is defined as the non-inverting gain.
  - d) For a difference amplifier, noise gain is defined as  $A_d$  and signal gain is defined as  $A_d + 1$
  - e) B & C

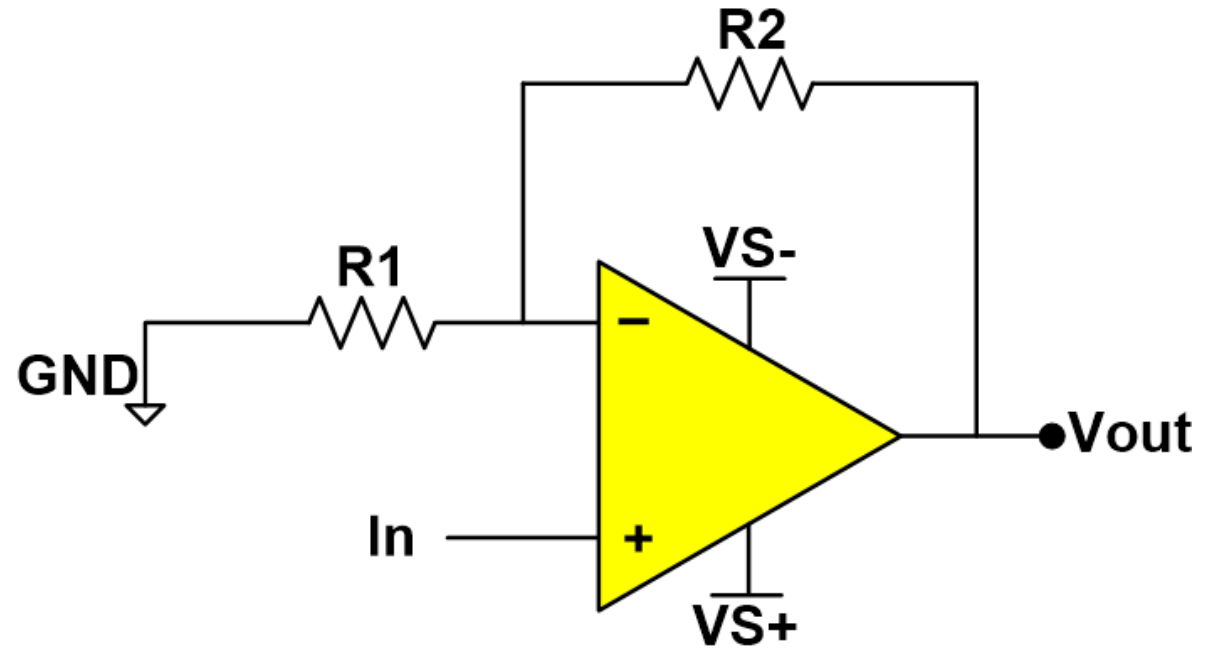
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  - e) **B & C**

# Quiz: (IA) topologies: one-amp || Question

4. What is the signal gain and noise gain of the following circuit?

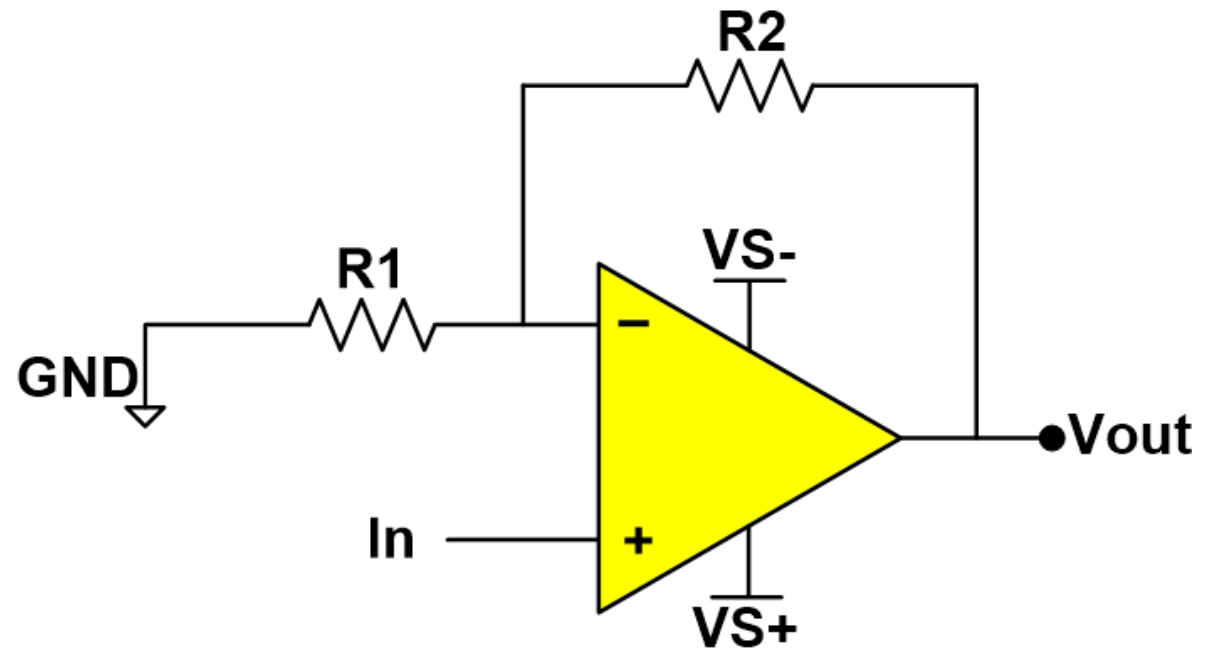
- a) Signal gain =  $-R2 / R1$   
Noise gain =  $1 - (R2 / R1)$
- b) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $R2 / R1$
- c) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $1 + (R2 / R1)$
- d) None of the above



# Quiz: (IA) topologies: one-amp || Answer

4. What is the signal gain and noise gain of the following circuit?

- a) Signal gain =  $-R2 / R1$   
Noise gain =  $1 - (R2 / R1)$
- b) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $R2 / R1$
- c) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $1 + (R2 / R1)$**
- d) None of the above

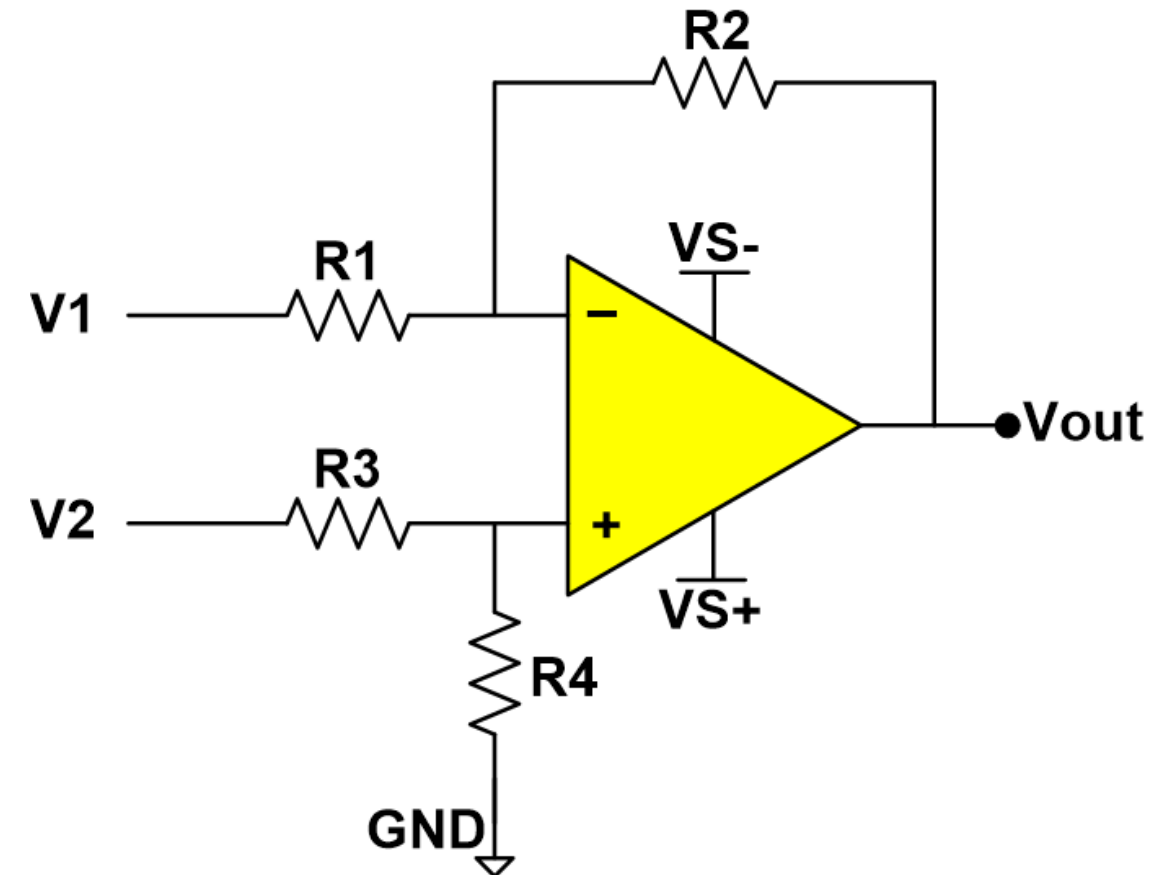




# Quiz: (IA) topologies: one-amp || Question

5. What is the signal gain and noise gain of the following circuit?

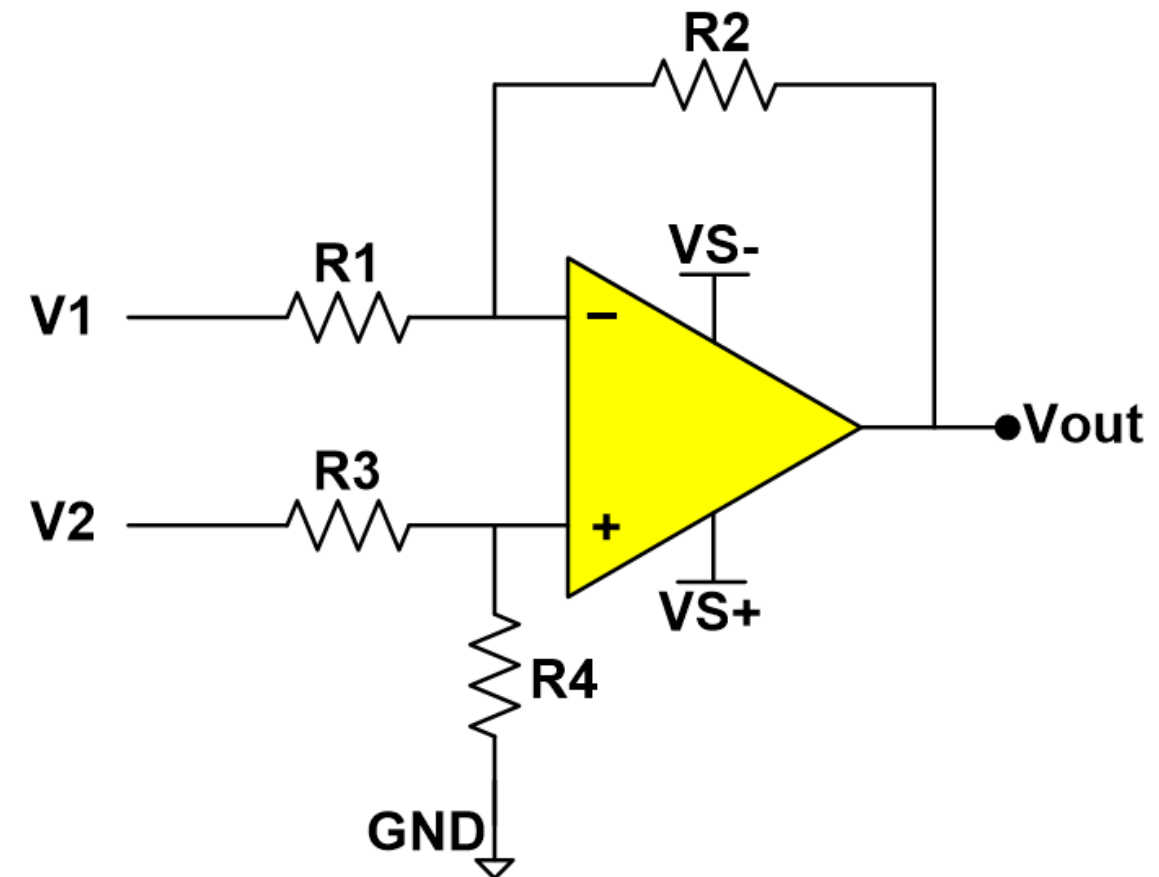
- a) Signal gain =  $-R2 / R1$   
Noise gain =  $1 - (R2 / R1)$
- b) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $R2 / R1$
- c) Signal gain =  $R2 / R1$   
Noise gain =  $1 + (R2 / R1)$
- d) None of the above



# Quiz: (IA) topologies: one-amp || Answer

5. What is the signal gain and noise gain of the following circuit?

- a) Signal gain =  $-R2 / R1$   
Noise gain =  $1 - (R2 / R1)$
- b) Signal gain =  $1 + (R2 / R1)$   
Noise gain =  $R2 / R1$
- c) Signal gain =  $R2 / R1$   
Noise gain =  $1 + (R2 / R1)$**
- d) None of the above



## Quiz: (IA) topologies: one-amp || Question

6. Which of the following is true of resistor CMRR performance?

- a) CMRR performance due to resistor mismatch is improved in low gain or attenuated circuits
- b) CMRR performance due to resistor mismatch is independent of gain
- c) CMRR performance due to resistor mismatch is improved for higher gain circuits
- d) None of the above

# Quiz: (IA) topologies: one-amp || Answer

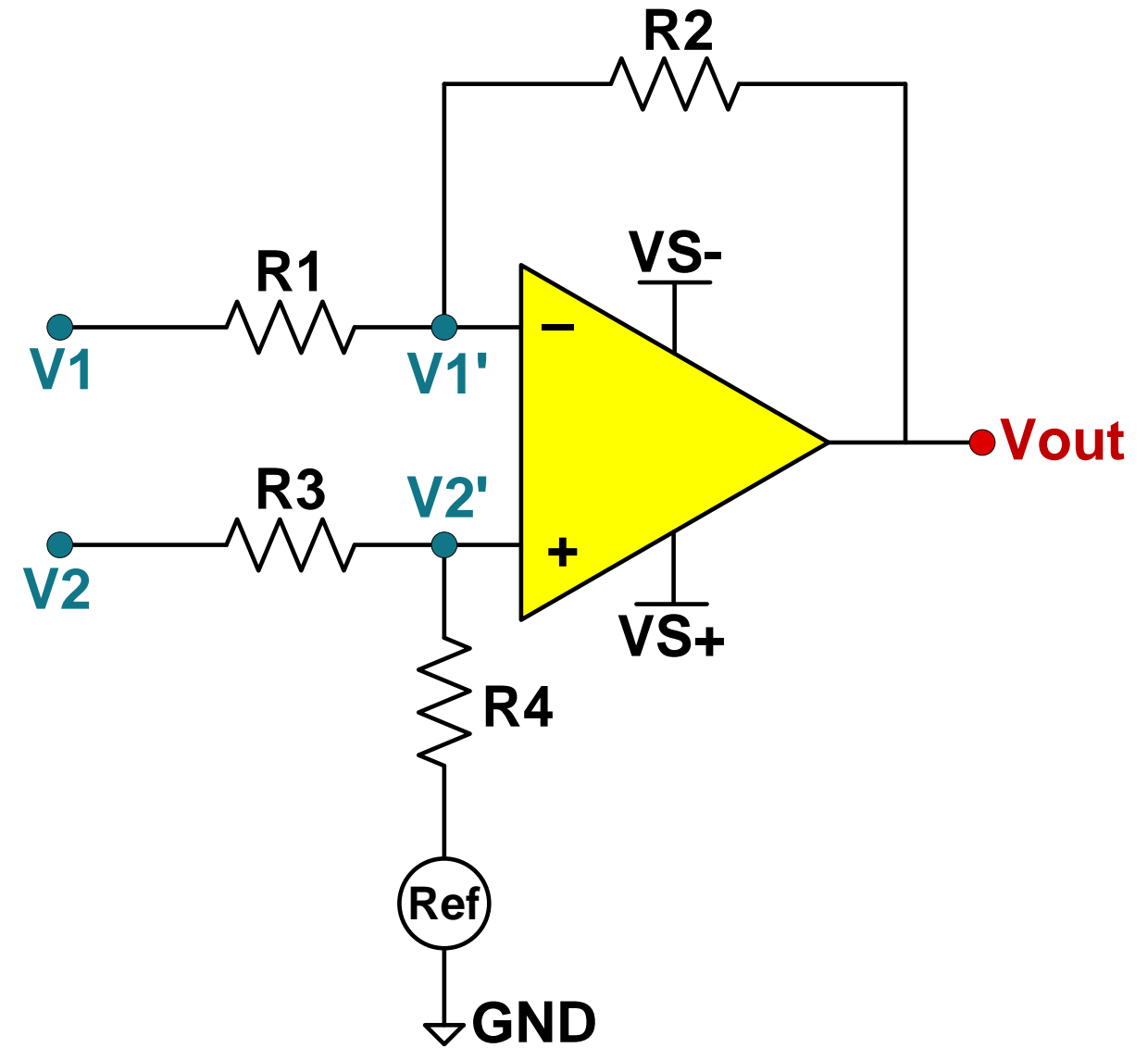
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- d) None of the above

# Quiz: (IA) topologies: one-amp || Question

7. Which of the following is true of one-amp IAs?

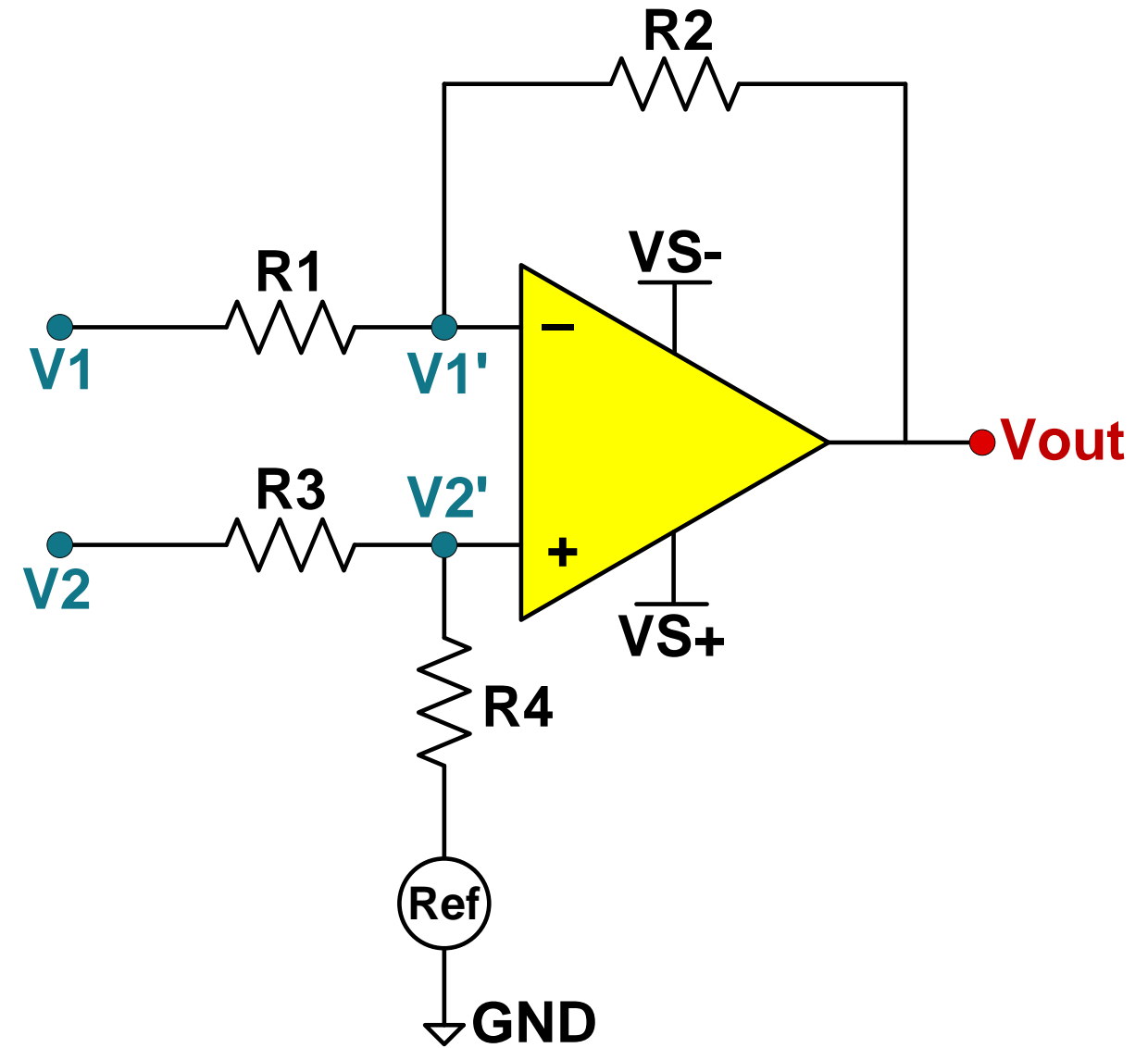
- a) Resistor matching is not crucial, as long as the value of the resistors are high
- b) One-amp IAs exhibit low input impedance. If paired with a non-zero output impedance source, accuracy will be degraded.
- c) The precision of a one-amp IA relies heavily on resistor matching
- d) B & C



# Quiz: (IA) topologies: one-amp || Answer

7. Which of the following is true of one-amp IAs?

- a) Resistor matching is not crucial, as long as the value of the resistors are high
- b) One-amp IAs exhibit low input impedance. If paired with a non-zero output impedance source, accuracy will be degraded.
- c) The precision of a one-amp IA relies heavily on resistor matching
- d) **B & C**



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