## 用于体重秤和人体成分测量的 <br> AFE4300 低成本集成模拟前端

1 特性

- 体重科前端：
- 支持最多四路称重传感器输入
- 通过片上称重传感器 1.7 V 激励电压进行比例式测量
－68nVrms 输入参考噪声 （ 0.1 Hz 至 2 Hz ）
- 最佳线性：满量程的 $0.01 \%$
- 体重计测量： $540 \mu \mathrm{~A}$
- 主体组成部分前端：
- 支持高达 3 个双向四电极波（Tetra－Polar）复杂阻抗测量
－ 6 位，每秒1百万次采样（1－MSPS）正弦波生成数模转换器（DAC）
- $247.5 \mu \mathrm{Arms}, ~ \pm 20 \%$ 激励源
- 在 2 Hz 带宽中具有 $0.1 \Omega$ 测量 RMS 噪声
- 人体成分测量： $970 \mu \mathrm{~A}$
- 模数转换器（ADC）：
- 16 位，860SPS
- 电源电流： $110 \mu \mathrm{~A}$

2 应用
可进行人体成分测量的体重秤

## 3 说明

AFE4300 是一款低成本模拟前端，此模拟前端有两个独立的信号链：一个信号链用于体重计（WS）测量，而另外一个信号链用于体成分测量（BCM）分析。一个 16位，860SPS 模数转换器（ADC）在两个信号链间复用。体重测量信号链包括一个可由外部电阻器设定增益的仪器放大器（INA），后接一个用于偏移校正的 6 位数模转换器（DAC），和一个驱动外部桥／负载单元（有一个用于比例式测量的 1.7 V 固定电压）的电路。

AFE4300 还可通过产生一个进入人体的正弦电流来测量人体成分。此正弦电流由一个内部模式生成器和一个 6 位，1MSPS DAC 生成。一个电压电流转换器将这个正弦电流应用在两个端子之间的人体上。在这两个端子上生成的电压是由人体的阻抗生成的，此电压由一个差分放大器测量，再经过整流，且其振幅由 16 位 ADC提取并测量。

AFE4300 的工作电压范围为 2 V 至 3.6 V ，额定温度为 $0^{\circ} \mathrm{C}$ 至 $+70^{\circ} \mathrm{C}$ ，并采用 LQFP－80 封装。

器件信息 ${ }^{(1)}$

| 器件型号 | 封装 | 封装尺寸（标称值） |
| :--- | :---: | :---: |
| AFE4300 | LQFP $(80)$ | $12.00 \mathrm{~mm} \times 12.00 \mathrm{~mm}$ |

（1）如需了解所有可用封装，请参阅数据表末尾的可订购产品附录。


An IMPORTANT NOTICE at the end of this data sheet addresses availability，warranty，changes，use in safety－critical applications， intellectual property matters and other important disclaimers．PRODUCTION DATA．

## 目录

1 特性 ..... 1
2 应用 ..... 1
3 说明 ..... 1
4 修订历史 ..... 2
5 Pin Configuration and Functions ..... 4
6 Specifications ..... 6
6．1 Absolute Maximum Ratings ..... 6
6．2 ESD Ratings ..... 6
6．3 Recommended Operating Conditions ..... 6
6．4 Thermal Information ..... 6
6．5 Electrical Characteristics：Front－End Amplification （Weight－Scale Signal Chain） ..... 7
6．6 Electrical Characteristics：Body Composition Measurement Front－End ..... 8
6．7 Electrical Characteristics：Analog－to－Digital Converter ..... 9
6．8 Electrical Characteristics：Digital Input／Output ..... 9
6．9 Timing Requirements：Serial Interface Timing ..... 10
6．10 Typical Characteristics ..... 11
7 Detailed Description ..... 12
7．1 Overview ..... 12
7．2 Functional Block Diagram ..... 12
7．3 Feature Description ..... 13
7．4 Device Functional Modes ..... 20
7．5 Programming ..... 21
7．6 Register Maps ..... 23
8 Application and Implementation ..... 30
8．1 Application Information ..... 30
8．2 Typical Application ..... 32
9 Power Supply Recommendations ..... 34
9．1 Power－Supply Recommendation and Initialization ..... 34
10 Layout． ..... 35
10．1 Layout Guidelines ..... 35
10．2 Layout Example ..... 35
11 器件和文档支持 ..... 36
11.1 接收文档更新通知 ..... 36
11.2 社区资源 ..... 36
11.3 商标 ..... 36
11.4 静电放电警告 ..... 36
11.5 Glossary ..... 36
12 机械，封装和可订购信息 ..... 36

## 4 修订历史

Changes from Revision B（June 2013）to Revision C Page
－添加了器件信息 表，ESD 额定值 表，特性 描述 部分，器件功能模式 部分，编程 部分，应用和实施 部分，电源建议 部分，布局 部分，器件和文档支持 部分以及机械，封装和可订购信息 部分 ..... 1
－已更改 人体成分 特性 项目：在激励源子项目中将 375 更改为 247.5 ，并删除了动态范围子项目 ..... 1
－通篇将 TQFP 更改为 LQFP ..... 1
－Deleted Package Information section ..... 4
－Changed Pin Functions table title ..... 4
－Changed clock to serial clock in SCLK pin description of Pin Functions table ..... 5
－Changed VSENSEN to VSENSEM in pins 41 and 42 in Pin Functions table ..... 5
－Changed AVSS parameter name to Ground from Supply voltage in Recommended Operating Conditions table． ..... 6
－Changed symbol R1 to $R_{F B 1}$ in Electrical Characteristics：Front－End Amplification（Weight－Scale Signal Chain）table ..... 7
－Changed typical specification of DAC full－scale voltage parameter from 1 to 1.05 in Electrical Characteristics：Body Composition Measurement Front－End table ..... 8
－Changed Electrical Characteristics：Digital Input／Output table title ..... 9
－Changed multiplication signs $(\times)$ to minimum and maximum specifications of Electrical Characteristics：Digital Input／Output table ..... 9
－Changed x－axis unit from $\mu \mathrm{Arms}$ to $\mu \mathrm{Apk}$ in BCM DAC Output Current Distribution figure ..... 11
－Changed Functional Block Diagram：swapped positions of RP1，RP0 and RN1，RN0 pins． ..... 12
－Changed BCM in AC Rectifier Mode figure：swapped positions of RP1，RP0 and RN1，RN0 pins． ..... 15
－Changed AC Rectification section：changed images to high－frequency images in second paragraph，VDAC to VDACOUT in Equation 5，and changed third paragraph ..... 16
－Changed third paragraph of $A C$ Rectification section：deleted（still within the $500-\mu$ Arms limit）from fourth sentence， changed last sentence． ..... 16
－Changed BCM in I／Q Demodulator Mode figure：swapped positions of RP1，RP0 and RN1，RN0 pins ..... 17
－Changed Operating Modes section． ..... 20
－Changed negative input to output in descriptions of IOUTP［5：0］and RP［1：0］and output to negative input in
Texas INSTRUMENTS
AFE4300
www．ti．com．cn
修订历史（接下页）
descriptions of IOUTN［5：0］and RN［1：0］in ISW＿MUX register ..... 26
－Changed bit 9 to DAC9 from 0 in BCM＿DAC＿FREQ register and changed bit count in bit descriptions to reflect this change ..... 27
－Changed $\mathrm{f}_{\text {CLK }}=1 \mathrm{MHz}$ to $\mathrm{f}_{\mathrm{CLK}}=1.024 \mathrm{MHz}$ in BCM＿DAC＿FREQ register ..... 27
－Changed Component Values Corresponding to Figure 12 table：changed title of second column from Suggested Value to Illustrative Value，R3，R4 illustrative value to $10 \mathrm{k} \Omega$ from $100 \mathrm{k} \Omega$ ，and changed table footnote ..... 30
－Changed 1 MHz to 1.024 MHz in Example Value column of Weight Scale Design Requirements table ..... 32
－Deleted touch from list of possible power－up interrupts in third paragraph of Detailed Design Procedure section ..... 33
－Changed first sentence of Application Curve section to reference Figure 15 ..... 33
－Changed capacitor to capacitances in last bullet of Layout Guidelines section ..... 35
Changes from Revision A（June 2012）to Revision B Page
－Changed title condition for Electrical Charancteristics ..... 7
－Changed test condition for rectifier bandwidth parameter ..... 8
－Changed y－axis unit in Figure 5 ..... 11
－Changed R1 percentage in Functional Block Diagram ..... 12
－Changed feedback resistor percentage in second paragraph after Figure 6 ..... 13
－Changed description for last row of Table 2 ..... 23
－Changed bit descriptions of ISW＿MUX register ..... 26
－Changed bit 9 for BCM＿DAC＿FREQ（Address 0x0E） ..... 27
－Changed bit numbers for MISC＿REGISTER3（Address 0x1A） ..... 29
Changes from Original（June 2012）to Revision A Page
－已将数据表从产品预览更改为生产数据 ..... 1

## 5 Pin Configuration and Functions



Pin Functions

| PIN |  | I/O |  |
| :--- | :---: | :---: | :--- |
| NAME | NUMBER |  | Auxiliary input to the ADC |
| AAUX1 | 15 | I | Auxiliary input to the ADC |
| AAUX2 | 51 | - | Supply $(3.3 \mathrm{~V})$ |
| AVDD | $18,46,80$ | - | Ground |
| AVSS | $1,6,9,14,21,32,45,60,77$ | I | 1-MHz clock |
| CLK | 79 | I | Current generator input. Connect ac blocking capacitor between this pin and pin 19. |
| DAC_FILT_IN | 20 | O | DAC output. Connect ac blocking capacitor between this pin and pin 20. |
| DACOUT | 19 |  |  |

AFE4300
www.ti.com.cn
ZHCS987C -JUNE 2012-REVISED SEPTEMBER 2017

## Pin Functions (continued)

| PIN |  | I/O | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| NAME | NUMBER |  |  |
| INM1 | 3 | 1 | Instrumentation amplifier differential inputs for each of the four weight-scale channels |
| INM2 | 5 |  |  |
| INM3 | 11 |  |  |
| INM4 | 13 |  |  |
| INP1 | 2 |  |  |
| INP2 | 4 |  |  |
| INP3 | 10 |  |  |
| INP4 | 12 |  |  |
| INM_R | 8 | - | Connection of gain setting resistor for the instrumentation amplifier |
| INP_R | 7 | - |  |
| IOUTO | 27 | 0 | Current source output to electrodes |
| IOUT1 | 26 |  |  |
| IOUT2 | 25 |  |  |
| IOUT3 | 24 |  |  |
| IOUT4 | 23 |  |  |
| IOUT5 | 22 |  |  |
| NC | 43, 44, 52, 55, 61-76, 78 | - | Do not connect |
| OUTM_I_FILT | 47 | - | I channel demodulator low pass filter, connect $10 \mu \mathrm{~F}$ between both pins |
| OUTP_I_FILT | 48 |  |  |
| OUTM_Q_FILT | 49 | - | Q channel demodulator low pass filter, connect $10 \mu \mathrm{~F}$ between both pins |
| OUTP_Q_FILT | 50 |  |  |
| $\overline{\text { RDY }}$ | 59 | 0 | Data ready |
| RN0 | 31 | 0 | Current source output to calibration resistors |
| RN1 | 30 |  |  |
| RP0 | 29 |  |  |
| RP1 | 28 |  |  |
| $\overline{\text { RST }}$ | 53 | 1 | Reset. 0: reset, 1: normal operation. |
| SCLK | 58 | I | Serial clock to latch input data (negative edge latch) |
| SDIN | 57 | 1 | Serial data input |
| SDOUT | 56 | O | Serial data output |
| STE | 54 | 1 | SPI enable. 0: shift data in, 1: disable. |
| VLDO | 16 | 0 | LDO output to supply the bridges ( $\sim 1.7 \mathrm{~V}$ ), connect 470 nF to AVSS |
| VREF | 17 | O | Reference voltage (connect 470 nF to AVSS) |
| VSENSEM_R0 | 42 | 1 | Input to differential amplifier from calibration resistors |
| VSENSEM_R1 | 41 |  |  |
| VSENSEP_R0 | 40 |  |  |
| VSENSEP_R1 | 39 |  |  |
| VSENSE0 | 38 | 1 | Input to differential amplifier from electrode |
| VSENSE1 | 37 |  |  |
| VSENSE2 | 36 |  |  |
| VSENSE3 | 35 |  |  |
| VSENSE4 | 34 |  |  |
| VSENSE5 | 33 |  |  |

## AFE4300

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ${ }^{(1)}$

|  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
|  | AVDD to AVSS | -0.3 | 4.1 |  |
|  | Any pin | -0.3 | AVDD + 0.3 |  |
| Diode current at any device pin |  |  | $\pm 2$ | mA |
| Maximum operating junction temperature, $\mathrm{T}_{\mathrm{J}} \max$ |  |  | 105 | ${ }^{\circ} \mathrm{C}$ |
| Storage humidity |  | 10\% | 90\% | Rh |
| Storage temperature, $\mathrm{T}_{\text {stg }}$ |  | -25 | 85 | ${ }^{\circ} \mathrm{C}$ |

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 6.2 ESD Ratings

|  |  | VALUE | UNIT |
| :---: | :---: | :---: | :---: |
| Electrostatic discharge | Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ${ }^{(1)}$ | $\pm 2000$ | V |
|  | Charged-device model (CDM), per JEDEC specification JESD22-C101 ${ }^{(2)}$ | $\pm 1000$ |  |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

|  |  | MIN | NOM | MAX |
| :--- | :--- | ---: | :---: | :---: |
| AVDD | Supply voltage | 2 |  | 3.6 |
| AVSS | Ground |  | 0 | V |
| f CLK | External clock input frequency |  | 1 | V |
| $\mathrm{T}_{\mathrm{A}}$ | Ambient temperature range | 0 |  | MHz |

### 6.4 Thermal Information

| THERMAL METRIC ${ }^{(1)}$ |  | $\begin{gathered} \text { AFE4300 } \\ \hline \text { PN (LQFP) } \end{gathered}$ | UNIT |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  |  | 80 PINS |  |
| $\mathrm{R}_{\theta \mathrm{JA}}$ | Junction-to-ambient thermal resistance | 50.5 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\theta \text { өJC(top) }}$ | Junction-to-case (top) thermal resistance | 14.2 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {өJB }}$ | Junction-to-board thermal resistance | 25.3 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\text {JT }}$ | Junction-to-top characterization parameter | 0.5 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\text {JB }}$ | Junction-to-board characterization parameter | 24.9 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\theta \mathrm{\theta JC} \text { (bot) }}$ | Junction-to-case (bottom) thermal resistance | N/A | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report

### 6.5 Electrical Characteristics: Front-End Amplification (Weight-Scale Signal Chain)

over operating free-air temperature range, $\mathrm{AVDD}-\mathrm{AVSS}=3 \mathrm{~V}, \mathrm{G} 1=183$, and $\mathrm{G} 2=1$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS | AFE4300 |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN TYP | MAX |  |
| BRIDGE SUPPLY |  |  |  |  |  |
| $\mathrm{V}_{\text {(VLDO) }}$ | Output voltage (bridge supply voltage) |  |  | 1.7 |  | V |
| $\mathrm{I}_{0}$ | Output current | Current capability |  | 20 | mA |
|  |  | Short-circuit protection | 100 |  | mA |
| $\mathrm{t}_{\text {STBY }}$ | Enable, disable time | With 470-nF capacitor on the VLDO pin | 1 |  | ms |
| AMPLIFICATION CHAIN |  |  |  |  |  |
|  | Offset error | With offset correction DAC disabled | 80 |  | $\mu \mathrm{V}$ |
|  | Offset drift vs temperature | With offset correction DAC disabled | 0.25 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  | Input bias current |  | $\pm 70$ |  | fA |
|  | Input offset current |  | $\pm 140$ |  | fA |
| $\mathrm{V}_{\mathrm{n}}$ | Noise voltage, equivalent input | $\mathrm{G} 1=183,0.01 \mathrm{~Hz}<\mathrm{f}<2 \mathrm{~Hz}$ | 68 |  | nV rms |
| $\mathrm{I}_{\mathrm{n}}$ | Noise current, equivalent input | $\mathrm{f}=10 \mathrm{~Hz}$ | 100 |  | $\mathrm{fA} / \sqrt{\mathrm{Hz}}$ |
| $\mathrm{z}_{\text {id }}$ | Differential input impedance |  | $100\|\mid 4$ |  | $\mathrm{G} \Omega \\| \mathrm{pF}$ |
| $\mathrm{z}_{\mathrm{ic}}$ | Common-mode input impedance |  | 100 \|| 8 |  | $\mathrm{G} \Omega \\| \mathrm{pF}$ |
| CMRR | Input common-mode rejection ratio | $\mathrm{G} 1=183$ | 95 |  | dB |
| $\mathrm{INL}_{\text {ws }}$ | Gain nonlinearity | From input to digital output (including ADC) | 0.01 |  | \% of FS ${ }^{(1)}$ |
|  | First-stage gain equation |  | $\left(1+2 \times 100 k / R_{G}\right)$ |  | V/V |
| $\mathrm{t}_{\text {up }}$ | Power-up time | From power up to valid reading | 1 |  | ms |
| $\mathrm{R}_{\mathrm{FB} 1}$ | Internal feedback resistors |  | 95100 | 105 | $\mathrm{k} \Omega$ |
| Gain2 | Second-stage gain settings |  | 1, 2, 3, 4 |  |  |
|  | Total gain error |  | $\pm 5 \%$ |  |  |
|  | Offset DAC number of bits |  | 6 |  | Bits |
| $\mathrm{I}_{\text {DAC }}$ | Full-scale offset DAC output current |  | $\pm 6.5$ |  | $\mu \mathrm{A}$ |

(1) $\mathrm{FS}=$ full-scale.

## AFE4300

ZHCS987C -JUNE 2012-REVISED SEPTEMBER 2017
www.ti.com.cn

### 6.6 Electrical Characteristics: Body Composition Measurement Front-End

over operating free-air temperature range, AVDD - AVSSS $=3 \mathrm{~V}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS | AFE4300 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MIN | TYP | MAX |  |
| WAVEFORM GENERATOR |  |  |  |  |  |  |
|  | DAC resolution |  |  |  | 6 |  | Bits |
|  | DAC full-scale voltage | Common-mode voltage $=0.9 \mathrm{~V}$ |  | 1.05 |  | $\mathrm{V}_{\text {(PP) }}$ |
|  | DAC sample rate |  |  | 1 |  | MSPS |
| BW ${ }_{\text {LPF }}$ | -3 dB bandwidth of the 2nd-order low-pass filter |  |  | $150 \pm 30$ |  | kHz |
| R1 | Internal current-setting resistor |  |  | $1.5 \pm 20 \%$ |  | $\mathrm{k} \Omega$ |
| DEMODULATION CHAIN |  |  |  |  |  |  |
|  | Input Impedance |  |  | 50 |  | $\mathrm{k} \Omega$ |
|  | Gain | From impedance to dc output of demodulator, IQ mode and FWR mode |  | 0.72 |  | $\mathrm{V} / \mathrm{k} \Omega$ |
|  | Gain error (without calibration) | FWR mode and I/Q mode |  | 2.5 |  | \% of FS |
|  | Offset error (without calibration) | FWR mode and I/Q mode |  | $\pm 5$ |  | mV |
| CMRR | Common-mode rejection ratio |  |  | 75 |  | dB |
| Nonlinearity |  | $0-\Omega$ to $1.25-\mathrm{k} \Omega$ range |  | 0.15 |  | \% of FS |
|  |  | $0-\Omega$ to $2.50-\mathrm{k} \Omega$ range |  | 3 |  | \% of FS |
| BW ${ }_{\text {demod }}$ | Rectifier bandwidth | Internal resistor $=5 \mathrm{k} \Omega$, external capacitor $=4.7 \mu \mathrm{~F}$ |  | $3.5 \pm 20 \%$ |  | Hz |
|  | Output noise at rectifier output | $20-\mathrm{kHz}$ waveform, noise integrated from 0.01 Hz to 2 Hz |  | 15 |  | $\mu \mathrm{Vrms}$ |

AFE4300
www.ti.com.cn

### 6.7 Electrical Characteristics: Analog-to-Digital Converter

over operating free-air temperature range, AVDD - AVSS $=3 \mathrm{~V}$ (unless otherwise noted)


### 6.8 Electrical Characteristics: Digital Input/Output

over operating free-air temperature range, AVDD - AVSS $=3 \mathrm{~V}$ (unless otherwise noted)

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{IH}}$ | High-level input voltage |  | $\begin{aligned} & 0.75 \times \\ & \text { AVDD } \end{aligned}$ |  | AVDD | V |
| $\mathrm{V}_{\text {IL }}$ | Low-level input voltage |  | AVSS |  | $\begin{aligned} & 0.25 \times \\ & \text { AVDD } \end{aligned}$ | V |
| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | $\mathrm{l} \mathrm{OL}=1 \mathrm{~mA}$ | $\begin{array}{r} 0.8 \times \\ \text { AVDD } \end{array}$ |  |  | V |
| $\mathrm{V}_{\text {OL }}$ | Low-level output voltage | $\mathrm{I}_{\mathrm{OL}}=1 \mathrm{~mA}$ | GND |  | $\begin{array}{r} 0.2 \times \\ \text { AVDD } \end{array}$ | V |
| $\mathrm{I}_{\mathrm{IN}}$ | Input current |  | $\pm 30$ |  |  | $\mu \mathrm{A}$ |

## AFE4300

ZHCS987C -JUNE 2012-REVISED SEPTEMBER 2017
www.ti.com.cn

### 6.9 Timing Requirements: Serial Interface Timing

at $\mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ and $\mathrm{VDD}=2 \mathrm{~V}$ to 3.6 V (unless otherwise noted)

|  |  | MIN | NOM | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {cssc }}$ | $\overline{\text { STE }}$ low to first SCLK setup time ${ }^{(1)}$ | 100 |  |  | ns |
| tsCLK | SCLK period | 250 |  |  | ns |
| tspwh | SCLK pulse duration high | 100 |  |  | ns |
| tspWL | SCLK pulse duration low | 100 |  |  | ns |
| $\mathrm{t}_{\text {DIST }}$ | Valid SDIN to SCLK falling edge setup time | 50 |  |  | ns |
| $\mathrm{t}_{\text {IIHD }}$ | Valid SDIN to SCLK falling edge hold time | 50 |  |  | ns |
| $\mathrm{t}_{\text {DOPD }}$ | SCLK rising edge to valid new SDOUT propagation delay ${ }^{(2)}$ |  |  | 50 | ns |
| $\mathrm{t}_{\text {DOHD }}$ | SCLK rising edge to DOUT invalid hold time | 0 |  |  | ns |
| tCSDOD | STE low to SDOUT driven propagation delay | 100 |  |  | ns |
| tcsioz | STE high to SDOUT Hi-Z propagation delay | 100 |  |  | ns |
| $\mathrm{t}_{\mathrm{CSH}}$ | STE high pulse | 200 |  |  | ns |
| tsccs | Final SCLK falling edge to STE high | 100 |  |  | ns |

(1) $\overline{\text { STE }}$ can be tied low.
(2) DOUT load $=20 \mathrm{pF} \| 100 \mathrm{k} \Omega$ to DGND.


Figure 1. Serial Interface Timing

AFE4300
www.ti.com.cn

### 6.10 Typical Characteristics

all measurements at room temperature with $\mathrm{AVDD}=3 \mathrm{~V}$ (unless otherwise specified)


Figure 2. Weight-Scale Chain Noise vs Frequency


Figure 4. BCM DAC Output Current Distribution


Figure 3. Weight-Scale Chain Nonlinearity


Figure 5. Body Impedance to Output Voltage Transfer Curve

## 7 Detailed Description

### 7.1 Overview

The AFE4300 is a low-cost, integrated front-end designed for weight scales incorporating body-composition measurements. The AFE4300 integrates all the components typically used in a weight scale. The device has two signal chains: one for weight scale measurements and the other for body composition measurements. Both signal chains share a 16 -bit, delta-sigma converter that operates at a data rate of up to 860 SPS. This device also integrates a reference and a low-dropout regulator (LDO) that generates a 1.7-V supply that can be used as the excitation source for the load cells, thus simplifying ratiometric measurements. Both the signal chains use a single digital-to-analog converter (DAC). The DAC is used to generate the dc signal for load-cell offset cancellation in the weight-scale chain. The same DAC is also used to generate the sine-wave modulation signal for the body-composition signal chain. Therefore, only one of the two signal chains can be activated at a time (using the appropriate register bits).
Two unique features of the AFE4300 are that the device provides an option for connecting up to four separate load cells, and supports tetrapolar measurements with I/Q measurements.

### 7.2 Functional Block Diagram



AFE4300

### 7.3 Feature Description

This section describes the details of the AFE4300 internal functional elements. The analog blocks are reviewed first, followed by the digital interface. The theory behind the body-composition measurement using the full-wave rectification method and the I/Q demodulation method are also described. The analog front-end is divided in two signal chains: a weight-measurement chain and a body-composition measurement front-end chain; both use the same 16 -bit ADC and 6 -bit DAC.
Throughout this document:

- $\mathrm{f}_{\text {CLK }}$ denotes the frequency of the signal at the CLK pin.
- $\mathrm{t}_{\mathrm{CLK}}$ denotes the period of the signal at the CLK pin.
- $f_{D R}$ denotes the output data rate of the ADC.
- $t_{D R}$ denotes the time period of the output data.
- $f_{\text {MOD }}$ denotes the frequency at which the modulator samples the input.


### 7.3.1 Weight-Scale Analog Front-End

Figure 6 shows a top-level view of the front-end section devoted to weight-scale measurement. The weight-scale front-end has two stages of gain, with an offset correction DAC in the second gain stage. The first-stage gain is set by the external resistor and the second-stage gain is set by progamming the internal registers. For access and programming information, see the Register Maps section.


Figure 6. Weight-Scale Front-End
Though not shown in the diagram, an antialiasing network is required in front of the INA to filter out electromagnetic interference (EMI) signals or any other anticipated interference signals. A simple RC network is sufficient, combined with the attenuation provided by the on-chip decimation filter.
An internal reference source provides a constant voltage of 1.7 V at the VLDO output to drive the external bridge. The output of the bridge is connected to an INA (first stage). The first-stage gain ( $\mathrm{A}_{1}$ ) is set by the external resistor $\left(R_{G}\right)$ and the $100-k \Omega( \pm 5 \%)$ internal feedback resistors $\left(R_{F B 1}\right)$ as shown in Equation 1:

$$
\begin{equation*}
A_{1}=\left(1+2 \times 100 k / R_{G}\right) \tag{1}
\end{equation*}
$$

The second-stage gain $\left(A_{2}\right)$ is controlled by feedback resistors $R_{F B 2}$, which have four possible values: $80 \mathrm{k} \Omega$, $160 \mathrm{k} \Omega, 240 \mathrm{k} \Omega$, and $320 \mathrm{k} \Omega$. Because the gain is $\mathrm{R}_{\mathrm{F}} / 80 \mathrm{k} \Omega$, the gain setting can be 1,2 , 3 , or 4 . See the Register Maps section for details on setting the appropriate register bits.

## Feature Description (continued)

### 7.3.1.1 Input Common Mode Range

The usable input common mode range of the weight-scale front-end depends on various parameters, including the maximum differential input signal, supply voltage, and gain. The output of the first-stage amplifier must be within 250 mV of the power supply rails for linear operation. The allowed common-mode range is determined by Equation 2:

$$
\text { AVDD }-0.25-\frac{G A I N \times V_{\text {MAX_DIFF }}}{2}>C M>A V S S+0.25+\frac{G A I N \times V_{\text {MAX_DIFF }}}{2}
$$

Where:

- $\mathrm{V}_{\text {MAX_DIFF }}=$ maximum differential input signal at the input of the first gain stage,
- $C M=$ Common-mode range.

For example, If $A V D D=2 \mathrm{~V}$, the first stage gain $=183$, and $\mathrm{V}_{\text {MAX_DFF }}=7.5 \mathrm{mV}(\mathrm{dc}+$ signal $)$, then:
$1.06 \mathrm{~V}>\mathrm{CM}>0.936 \mathrm{~V}$

### 7.3.1.2 Input Differential Dynamic Range

The max differential (INP - INN) signal depends on the analog supply, reference used in the system. This range is shown in Equation 3:

$$
\begin{equation*}
\operatorname{MAX}(I N P-I N N)<\frac{\text { VREF }}{\text { GAIN }} ; \text { Full-Scale Range }=2 \times \frac{\text { VREF }}{\text { GAIN }} \tag{3}
\end{equation*}
$$

The gain in Equation 3 is the product of the gains of the INA and the second-stage gain. The full-scale input from the bridge signal typically consists of a differential dc offset from the load cell plus the actual weight signal. Having a high gain in the first stage helps minimize the effect of the noise addition from the subsequent stages. However, make sure to choose a gain that does not saturate the first stage with the full-scale signal. Also, the common-mode of the signal must fall within the range, as per Equation 2.

### 7.3.1.3 Offset Correction DAC

One way to increase the dynamic range of the signal chain is by calibrating the inherent offset of the load cell during the initial calibration cycle. The offset correction is implemented in the second stage with a 6 -bit differential DAC, where each output is a mirror of the other and can source or sink up to $6.5 \mu \mathrm{~A}$. The effect at the output of the second stage is an addition of up to $\pm 6.5 \mu \mathrm{~A} \times 2 \times \mathrm{R}_{\mathrm{FB} 2}$. This effect is equivalent to a voltage at the input of the second stage ( $\mathrm{A}+/ \mathrm{A}-$ ) of up to $\pm 6.5 \mu \mathrm{~A} \times 2 \times 80 \mathrm{k} \Omega= \pm 1 \mathrm{~V}$, when $\mathrm{R}_{\mathrm{FB} 2}=80 \mathrm{k} \Omega$. The first-stage saturation cannot be avoided using this DAC. Because the offset correction DAC is a 6 -bit DAC, the offset compensation step is $2 \mathrm{~V} / 2^{6}=31.2 \mathrm{mV}$ when referred to the input of the second stage.

### 7.3.1.3.1 Offset Correction Example

As an example, use a bridge powered from 1.7 V with $1.5 \mathrm{mV} / \mathrm{V}$ sensitivity and a potential offset between -4 mV and 4 mV . Worst case, the maximum signal is 4 mV of offset plus $1.7 \times 1.5 \mathrm{mV} / \mathrm{V}=2.55 \mathrm{mV}$ of signal, for a total of 6.55 mV . The bridge common-mode voltage is $\sim 0.85 \mathrm{~V}$. The maximum excursion is $0.85 \mathrm{~V}-0.25 \mathrm{~V}=0.6 \mathrm{~V}$ (bottom rail) single-ended, on each output ( $\mathrm{A}+$ or $\mathrm{A}-$ ). Therefore, $\pm 1.2 \mathrm{~V}$ differentially at the output of the first stage prevents saturation. This result means that the first stage can have up to a gain of $1.2 \mathrm{~V} / 6.55 \mathrm{mV}=183$.
Using this same example, the swing at the output of the first stage corresponding only to the potential offset range is $183 \times \pm 4 \mathrm{mV}= \pm 0.732 \mathrm{~V}$. This swing can be completely removed at the output of the second stage by the offset correction (because the offset correction DAC has a $\pm 1-\mathrm{V}$ range) except for a maximum error of 31.2 mV .

AFE4300
www.ti.com.cn

## Feature Description (continued)

### 7.3.2 Body Composition Measurement Analog Front-End

Body composition is traditionally obtained by measuring the impedance across several points on the body and matching the result in a table linking both the impedance measured and the body composition. This table is created by each manufacturer and is usually based on age group, sex, weight, and other parameters.

The body impedance that we want to measure, $Z(f)$, is a function of the excitation frequency, and can be represented by polar or cartesian notations:

$$
Z(f)=|Z(f)| \cdot e^{j \theta(f)}=R(f)+j X(f)
$$

where:

$$
\begin{align*}
& \text { - } \quad|Z|=\operatorname{sqrt}\left(R^{2}+X^{2}\right) \\
& \text { - } \quad \theta=\operatorname{arctg}(X / R) \tag{4}
\end{align*}
$$

The AFE4300 provides two options for body impedance measurement: ac rectification and I/Q demodulation. Both options work by injecting a sinusoidal current into the body and measuring the voltage across the body. The portion of the circuit injecting the current into the body is the same for each of those options. The difference, however, lies in how the measured voltage across the impedance is processed to obtain the final result.

### 7.3.2.1 AC Rectification

Figure 7 shows the portion of the AFE4300 devoted to body composition measurement in the RMS detector mode.


Figure 7. BCM in AC Rectifier Mode

## Feature Description (continued)

The top portion of Figure 7 represents the current-injection circuit. A direct digital synthesizer (DDS) generates a sinusoidal digital pattern with a frequency obtained by dividing a $1-\mathrm{MHz}$ clock with a 10 -bit counter. The digital pattern drives a 6 -bit, 1-MSPS DAC. The output of the DAC is filtered by a $150-\mathrm{kHz}$, second-order filter to remove the high-frequency images, followed by a series external capacitor to block the dc current and avoid any dc current injection into the body. The output of the filter (after the dc blocking capacitor) drives a resistor setting the amplitude of the current to be injected in the body, as shown in Equation 5:

$$
\begin{equation*}
I(t)=V D A C O U T / R 1=A \sin \left(w_{0} t\right) \tag{5}
\end{equation*}
$$

The nominal DACOUT voltage (VDACOUT) is $1.05 \mathrm{~V}_{\mathrm{PP}}(371.23 \mu \mathrm{Vrms})$. The nominal value of R 1 is $1.5 \mathrm{k} \Omega$. So the nominal excitation current is $247.5 \mu$ Arms. R1 can have a $\pm 20 \%$ device-to-device variation, so the highest current is close to $300 \mu \mathrm{Arms}\left(850 \mu \mathrm{~A}_{\mathrm{PP}}\right.$ ). The maximum voltage swing for the excitation electrodes (IOUT1IOUTO) is $1 \mathrm{~V}_{\mathrm{pp}}$. This swing limits the recommended total impedance in feedback to approximately $1175 \Omega$. To reduce the excitation current, place an external resistor, $\mathrm{R}_{\text {DAC }}$, (between DACOUT and DAC_FILT_IN) in series with R1. For example, with a $1.5-\mathrm{k} \Omega$ external resistor, the currents roughly reduce by 2 X , thereby extending the range of the measured impedance.

Current flows into the body through an output analog multiplexer (mux) that allows the selection of up to six different contact points on the body. The same mux allows the connection of four external impedances for calibration. The current crosses the body impedance and a second mux selects the return path (contact) on the body, closing the loop to the output of the amplifier.
At the same time that the current is injected, a second set of multiplexers connects a differential amplifier across the same body impedance in order to measure the voltage drop created by the injected current, shown by Equation 6:

$$
\begin{equation*}
v(t)=A|Z| \sin \left(\omega_{0} t+\theta\right) \tag{6}
\end{equation*}
$$

where $Z$ and $\theta$ are the module and phase of the impedance at $\omega_{0}$, respectively.
The output of the amplifier is routed to a pair of switches that implement the demodulation at the same frequency as the excitation current source in order to drive the control of those switches. This circuit performs a full-wave rectification of the differential amplifier output and a low-pass filter at the output, recovers the dc level, and finally routes the amplifier output to the same 16 -bit digitizer used in the weight-scale chain.

$$
\begin{equation*}
D C=\frac{2}{T} \int_{T / 2} A|Z| \sin \left(\omega_{0} t+\theta\right) d t=\frac{2 A|Z|}{\pi} \tag{7}
\end{equation*}
$$

Ultimately, the dc output is proportional to the module of the impedance. The proportionality factor can be obtained through calibration with the four external impedances. Although, with one single frequency or measurement, only the module of the impedance can be obtained; two different frequencies could be used to obtain both the real and the imaginary parts.

AFE4300
www.ti.com.cn

## Feature Description (continued)

### 7.3.2.2 I/Q Demodulation

The AFE4300 includes a second circuit that with a single frequency measurement, obtains both the real and the imaginary portions, as shown in Figure 8. As explained previously, the portion of the circuit injecting the current into the body is the same for both configurations. Therefore, the circuit is the same in Figure 7 and Figure 8. The difference between them is that an I/Q demodulator is used in this second approach, as shown in Figure 8.


Figure 8. BCM in I/Q Demodulator Mode
As with the case of the RMS detector, a differential amplifier measures the voltage drop across the impedance, as shown in Equation 8:

$$
\mathrm{v}(\mathrm{t})=\mathrm{A}|\mathrm{Z}| \sin \left(\omega_{0} \mathrm{t}+\theta\right)
$$

where:

- $\mathrm{Z}=$ the module of the impedance at $\omega_{0}$
- $\theta=$ phase of the impedance at $\omega_{0}$

The I/Q demodulator takes the $\mathrm{v}(\mathrm{t})$ signal and outputs two dc values. These two values are used to extract the impedance module and phase with a single frequency measurement. Figure 8 shows the block diagrm of the implementation. Using the I/Q demodulator helps reduce power consumption and still yields excellent performance. The local oscillator (LO) signals for the mixers are generated from the same clock driving the DDS/DAC and are of the same phase and frequency as the sinusoidal $i(t)$ (see Equation 5). The LO signals directly control the switches on the in-phase (I) path, and after a delay of $90^{\circ}$ degrees, control the switches on the quadrature $(\mathrm{Q})$ path. This switching results in multiplying the $\mathrm{v}(\mathrm{t})$ signal by a square signal swinging from -1 to 1 .

## Feature Description (continued)

Breaking down the LO signal into Fourier terms results in Equation 9:

$$
\begin{equation*}
L O_{1}(t)=\frac{4}{\pi}\left(\sin \left(\omega_{0} t\right)+\frac{1}{3} \sin \left(3 \omega_{0} t\right)+\frac{1}{5} \sin \left(5 \omega_{0} t\right)+\ldots\right) \tag{9}
\end{equation*}
$$

Therefore, the output voltage of the mixer is as shown in Equation 10:

$$
\begin{equation*}
I(t)=A|Z| \frac{4}{\pi}\left(\sin \left(\omega_{0} t+\theta\right) \sin \left(\omega_{0} t\right)+\frac{1}{3} \sin \left(\omega_{0} t+\theta\right) \sin \left(3 \omega_{0} t\right)+\frac{1}{5} \sin \left(\omega_{0} t+\theta\right) \sin \left(5 \omega_{0} t\right)+\ldots\right) \tag{10}
\end{equation*}
$$

Where $I(t)=$ in-phase output (not to be confused with $i(t)$, the current injected in the impedance).
Applying fundamental trigonometry gives Equation 11:

$$
\begin{equation*}
\sin a \sin b=-\frac{1}{2} \cos (a+b)+\frac{1}{2} \cos (a-b) \tag{11}
\end{equation*}
$$

Each product of sinusoids can be broken up in an addition of two sinusoids. Equation 12 shows the first term:

$$
\begin{equation*}
\sin \left(\omega_{0} t+\theta\right) \sin \left(\omega_{0} t\right)=\frac{1}{2} \cos \left(\omega_{0} t+\theta-\omega_{0} t\right)-\frac{1}{2} \cos \left(\omega_{0} t+\omega_{0} t+\theta\right)=\frac{1}{2} \cos (\theta)-\frac{1}{2} \cos \left(2 \omega_{0} t+\theta\right) \tag{12}
\end{equation*}
$$

Equation 13 shows the 2nd product:

$$
\begin{equation*}
\sin \left(\omega_{0} t+\theta\right) \sin \left(3 \omega_{0} t\right)=\frac{1}{2} \cos \left(\omega_{0} t+\theta-3 \omega_{0} t\right)-\frac{1}{2} \cos \left(3 \omega_{0} t+\omega_{0} t+\theta\right)=\frac{1}{2} \cos \left(-2 \omega_{0} t+\theta\right)-\frac{1}{2} \cos \left(4 \omega_{0} t+\theta\right) \tag{13}
\end{equation*}
$$

And so on. Performing the same analysis on the Q side, the output voltage of the mixer is shown in Equation 14:

$$
\begin{equation*}
Q(t)=A|Z| \frac{4}{\pi}\left(\sin \left(\omega_{0} t+\theta\right) \cos \left(\omega_{0} t\right)+\frac{1}{3} \sin \left(\omega_{0} t+\theta\right) \cos \left(3 \omega_{0} t\right)+\frac{1}{5} \sin \left(\omega_{0} t+\theta\right) \cos \left(5 \omega_{0} t\right)+\ldots\right) \tag{14}
\end{equation*}
$$

Agiain, applying fundamental trigonometry gives Equation 15:

$$
\begin{equation*}
\sin a \cos b=\frac{1}{2} \sin (a+b)+\frac{1}{2} \sin (a-b) \tag{15}
\end{equation*}
$$

Each of the products can be broken up into sums. Starting with the first product, as shown in Equation 16:

$$
\begin{equation*}
\sin \left(\omega_{0} t+\theta\right) \cos \left(\omega_{0} t\right)=\frac{1}{2} \sin \left(2 \omega_{0} t+\theta\right)+\frac{1}{2} \sin (\theta) \tag{16}
\end{equation*}
$$

And so on. Note that on $I(t)$ as well as on $Q(t)$, all the terms beyond the cutoff frequency of the low-pass filter at the output of the mixers (setup by the two $1-\mathrm{k} \Omega$ resistors and an external capacitor) are removed, leaving only the dc terms, giving Equation 17 for $\mathrm{I}_{\mathrm{DC}}$ and Equation 18 for $\mathrm{Q}_{\mathrm{DC}}$ :

$$
\begin{align*}
& \mathrm{I}_{\mathrm{DC}}=\frac{2 \mathrm{~A}|\mathrm{Z}|}{\pi} \cos (\theta)=\mathrm{K}|\mathrm{Z}| \cos (\theta)  \tag{17}\\
& \mathrm{Q}_{\mathrm{DC}}=\frac{2 \mathrm{~A}|\mathrm{Z}|}{\pi} \sin (\theta)=\mathrm{K}|\mathrm{Z}| \sin (\theta) \tag{18}
\end{align*}
$$

In reality, the LO amplitude is not known (likely, not $\pm 1$ ) and affects the value of K in Equation 17 and Equation 18. Solving these two equations gives Equation 19:

$$
\begin{align*}
& \theta=\arctan \frac{Q_{D C}}{I_{D C}} \\
& Z=\frac{1}{K} \sqrt{I_{D C}^{2}+Q_{D C}{ }^{2}} \tag{19}
\end{align*}
$$

In order to account for all the nonidealities in the system, the AFE4300 also offers four extra terminals on the driving side (two to drive, and two for the currents to return) and four extra terminals on the receive/differentialamplifier side. As with RMS mode, these spare terminals allow for connection of up to four external calibration impedances, and they also compute $K$.

AFE4300
www.ti.com.cn

## Feature Description (continued)

### 7.3.3 Digitizer

The digitizer block includes an analog mux and a 16-bit sigma-delta ADC.

### 7.3.3.1 Multiplexer

There are two levels of analog mux. The first level selects from among the outputs of the weight scale, the body composition function, two auxiliary inputs, and the battery monitor. A second mux is used to obtain the measurement of the outputs coming from the first mux, either differentially or with respect to ground (singleended). Note that when measuring single-ended inputs, the negative range of the output codes are not used. For battery or AVDD monitoring, an internal $1 / 3$ resistor divider is included that enables the measurement using only one reference setting for any battery voltage, thus simplifying the monitoring routine.

### 7.3.3.2 Analog-to-Digital Converter

The 16 -bit, delta-sigma, ADC operates at a modulator frequency of 250 kHz with an $\mathrm{f}_{\mathrm{CLK}}$ of 1 MHz . The full-scale voltage of the ADC is set by the voltage at the reference ( $\mathrm{V}_{\text {REF }}$ ). The reference can be either the LDO output (1.7 V ) for the weight-scale front-end or the internally-generated reference signal ( 1.7 V ) for the BCM front-end.

The decimation filter at the output of the modulator is a single-order sinc filter. The decimation rate can be programmed to provide data rates from 8 SPS to 860 SPS with an $\mathrm{f}_{\text {CLK }}$ of 1 MHz . Refer to the ADC_CONTROL_REGISTER1 register in the Register Maps section for details on programming the data rates. Figure 9 shows the frequency response of the digital filter for a data rate of 8 SPS. Note that the modulator has pass band around integer multiples of the modulator sampling frequency of 250 kSPS . Set the corner frequency of the antialiasing network before the INA so that there is adequate attenuation at the first multiple of the modulator frequency.


Figure 9. Frequency Response
The output format of the ADC is twos complement binary. Table 1 describes the output code versus the input signal, where full-scale (FS) is equal to the $\mathrm{V}_{\text {REF }}$ value.

Table 1. Input Signal Versus Ideal Output Code
$\left.\begin{array}{|c|c|}\hline \begin{array}{c}\text { INPUT SIGNAL, } \mathbf{V}_{\mathbf{I N}} \\ \left(\text { AIN }_{\mathbf{P}}-\text { AIN }_{\mathbf{N}}\right)\end{array} & \text { IDEAL OUTPUT CODE }\end{array}\right]$ 7FFFh

### 7.3.4 Reset and Power-Up

After power up, the device needs to be reset to get all the internal registers to their default state. Resetting the device is done by applying a zero pulse in the RST line for more than 20 ns after the power is stable for 5 ms . After 30 ns , the first access can be initiated (first falling edge of STE). As part of the reset process, the AFE4300 sets all of the register bits to the respective default settings. Some of the register bits must be written after reset and power up for proper operation. Refer to the Register Maps section for more details. By default, the AFE4300 enters into a power-down state at start-up. The device interface and digital are active, but no conversion occurs until the ADC_PD bit is written to. The initial power-down state of the AFE4300 is intended to relieve systems with tight power-supply requirements from encountering a surge during power-up.

### 7.3.5 Duty Cycling for Low Power

For many applications, improved performance at low data rates may not be required. For these applications, the AFE4300 supports duty cycling that can yield significant power savings by periodically requesting high data-rate readings at an effectively lower data rate. For example, an AFE4300 in power-down mode with a data rate set to 860 SPS could be operated by a microcontroller that instructs a single-shot conversion every 125 ms ( 8 SPS ). Because a conversion at 860 SPS only requires approximately 1.2 ms , the AFE4300 automatically enters powerdown mode for the remaining 123.8 ms . In this configuration, the digitizer consumes about 1/100th the power of the digitizer when operated in Continuous-Conversion mode. The rate of duty cycling is completely arbitrary and is defined by the master controller.

### 7.4 Device Functional Modes

### 7.4.1 Operating Modes

The ADC operates in one of two conversion modes: Continuous-Conversion or Single-Shot conversion. The conversion mode is set using the ADC_CONV_MODE bit. In Continuous-Conversion mode, the ADC continuously performs conversions when the ADC_PD bit is set to 0 . When a conversion completes, the ADC places the result in a register, issues an interrupt on the RDY pin, and immediately begins another conversion. In this mode, if ADC_PD is set to 1 , then the ADC goes into a power-down state.
To get a Single-Shot conversion, the ADC_PD bit is to be first set to 1. When the ADC_CONV_MODE is subsequently set to 1, then the Single-Shot conversion is enabled. When enabled, the ADC does a single conversion and gives an interrupt on the RDY pin. To do one more Single-Shot conversion, the ADC_CONV_MODE bit must be set to 0 and then 1 again (with the ADC_PD bit at 1).

### 7.5 Programming

### 7.5.1 Serial Interface

The SPITM-compatible serial interface consists of either four signals ( $\overline{\text { STE }}$, SCLK, SDIN, and SDOUT) or three signals (in which case, STE can be tied low). The interface is used to read conversion data, read from and write to registers, and control AFE4300 operation. The data packet (between falling and rising edge of STE) is 24 bits long and is serially shifted into SDIN with the MSB first. The first eight bits (MSB) represent the address of the register being accessed and last 16 bits (LSB) represent the data to be stored or read from that address. For the eight bits address, the lower five bits [20:16] are the real address bits. Bit 21 is the read and write bit.

- ' 0 ' in bit 21 defines a write operation of the 16 data bits [15:0] into the register defined by the address bits [20:16].
- '1' in bit 21 triggers a read operation of the register defined by the address bits [20:16]. The data are output into SDOUT with every rising edge of SCLK, starting at the ninth rising edge. At the same time, data in SDIN are shifted inside the 16 data bits of that given register. Note that every time a register is read, the register must be rewritten except when reading the data output register.


### 7.5.1.1 SPI Enable (STE)

The STE pin selects the AFE4300 for SPI communication. This feature is useful when multiple devices share the serial bus. STE must remain low for the duration of the serial communication. When STE is taken high, the serial interface is reset, and SCLK is ignored.

### 7.5.1.2 Serial Clock (SCLK)

The SCLK pin features a Schmitt-triggered input and is used to clock data on the DIN and $\overline{\text { RDY }}$ pins into and out of the AFE4300. Even though the input has hysteresis, SCLK is recommended to be kept as clean as possible to prevent glitches from accidentally shifting the data. When the serial interface is idle, hold SCLK low.

### 7.5.1.3 Data Input (SDIN)

The data input pin (SDIN) is used along with SCLK to send data to the AFE4300 (opcode commands and register data). The device latches data on SDIN on the falling edge of SCLK. The AFE4300 never drives the SDIN pin. Note that every time a register is read, the register must be rewritten, except when reading the data output register.

### 7.5.1.4 Data Output (SDOUT)

The data output and data ready pin ( $\overline{\mathrm{RDY}})$ are used with SCLK to read conversion and register data from the AFE4300. In Read Data Continuous mode, RDY goes low when conversion data are ready, and goes high 8 s before the data ready signal. Data on RDY are shifted out on the rising edge of SCLK. If the AFE4300 does not share the serial bus with another device, STE may be tied low. Note that every time a register is read, the register must be rewritten, except when reading the data output register.

## Programming (continued)

### 7.5.1.5 Data Ready ( $\overline{R D Y}$ )

$\overline{\mathrm{RDY}}$ acts as a conversion ready pin in both Continous-Conversion mode and Single-Shot mode. When in Continuous-Conversion mode, the AFE4300 provides a brief ( $\sim 8 \mu \mathrm{~s}$ ) pulse on the $\overline{\text { RDY }}$ pin at the end of each conversion. In Single-Shot mode, the RDY pin asserts low at the end of a conversion. Figure 10 and Figure 11 show the timing diagram for these two modes.


Note 1 : Write ADC_CONTROL_REGISTER[7] = 1, ADC_CONTROL_REGISTER1[15] = 1 ,
Note 2 : tconv = Time to internally set ADC_CONTROL_REGISTER[15] to logic ' 0 ', ADC power up, single conversion, ADC power down, ADC_CONTROL_REGISTER1[15] internally set to logic ' 1 '

Figure 10. Timing for Single-Shot Mode


Note 1 : Write ADC_CONTROL_REGISTER[7] = 0
Figure 11. Timing for Continuous Mode

### 7.6 Register Maps

### 7.6.1 Register Map

Table 2 describes the registers of the AFE4300.
Table 2. Register Map

| REGISTER NAME | CONTROL | ADDRESS | DESCRIPTION | DEFAULT |
| :---: | :---: | :---: | :---: | :---: |
| DEVICE CONTROLS |  |  |  |  |
| DEVICE_CONTROL1 | (See Description) | 0x09[14:13] | Write '11' after power up and/or reset | 00b |
|  | DAC_PD | 0x09[3] | Enable DAC for WS, BC measurements | 0b |
|  | PDB | 0x09[2] | Chip power down | 0b |
|  | BCM_PDB | 0x09[1] | Body composition measurement front-end power down | 0b |
|  | WS_PDB | 0x09[0] | Weight-scale front-end power down | 0b |
| DEVICE_CONTROL2 | BAT_MON_EN1 | $0 \times 0 \mathrm{~F}[7]$ | Enables battery monitoring along with bit[0] | 0b |
|  | BAT_MON_EN2 | $0 \times 0 \mathrm{~F}[0]$ | Enables battery monitoring along with bit[7] | 0b |

## ADC CONTROLS

| ADC_DATA_RESULT | (See Description) | $0 \times 00[15: 0]$ | ADC data result, read only register |  |
| :--- | :---: | :---: | :--- | :---: |
| ADC_CONTROL_REGISTER1 | ADC_CONV_MODE | $0 \times 01[15]$ | Continuous-Conversion or Single-Shot mode | 0 b |
|  | ADC_MEAS_MODE | $0 \times 01[13: 11]$ | Single-Ended or Differential mode | 000 b |
|  | ADC_PD | $0 \times 01[7]$ | ADC power down | 1 b |
|  | ADC_DATA_RATE | $0 \times 01[6: 4]$ | ADC data-rate control bits | 100 b |
| ADC_CONTROL_REGISTER2 | ADC_REF_SEL | $0 \times 10[6: 5]$ | Reference selection bits | 00 b |
|  | PERIPHERAL_SEL | $0 \times 10[4: 0]$ | Peripheral selection bits | 00000 b |

## WEIGHT-SCALE MODES

| DEVICE_CONTROL2 | BRIDGE_SEL | $0 \times 0 F[2: 1]$ | Selects one of the four bridge inputs | 00 b |
| :--- | :---: | :---: | :--- | :---: |
| WEIGHT_SCALE_CONTROL | WS_PGA_GAIN | $0 \times 0 D[14: 13]$ | PGA gain of weight-scale front-end | 00 b |
|  | OFFSET_DAC_VALUE | $0 \times 0 \mathrm{D}[5: 0]$ | Offset DAC setting for weight-scale front-end | 000000 b |

## BCM CONTROLS

| ISW_MUX | ISW_MUXP | 0x0A[15:8] | Control for switches IOUTP and RP | $0 \times 00$ |
| :---: | :---: | :---: | :---: | :---: |
|  | ISW_MUXM | 0x0A[7:0] | Control for switches IOUTN and RN | $0 \times 00$ |
| VSENSE_MUX | VSENSE_MUXP | 0x0B[15:8] | Control for switches VSENSEP and VSENSEP R | 0x00 |
|  | VSENSE_MUXM | 0x0B[7:0] | Control for switches VSENSEN and VSENSN_R | $0 \times 00$ |
| BCM_DAC_FREQ | DAC_FREQ | 0x0E[9:0] | Sets the frequency of BCM excitation current source | 0x00 |
| IQ_MODE_ENABLE | IQ_MODE_ENABLE | 0x0C[11] | Enable IQ demodulator | Ob |
| DEVICE_CONTROL2 | IQ_DEMOD_CLK_DIV_ FAC | 0x0F[13:11] | IQ Demodulator clock frequency | 000b |
| MISCELLANEOUS REGISTERS |  |  |  |  |
| MISC_REGISTER1 | (See Description) | 0x02[15:0] | Write 0x0000 after power up and/or reset | 0x8000 |
| MISC_REGISTER2 | (See Description) | 0x03[15:0] | Write 0xFFFF after power up and/or reset | 0x7FFF |
| MISC_REGISTER3 | (See Description) | 0x1A[15:0] | Write 0x0030 after power up and/or reset | 0x0000 |

### 7.6.1.1 ADC_DATA_RESULT (Address 0x00, Default 0x0000)

This register stores the most recent conversion data in twos complement format with the MSB in bit 15 and the LSB in bit 0 .

### 7.6.1.2 ADC_CONTROL_REGISTER1 (Address 0x01, Default 0x01C3)

This register is used in conjunction with ADC_PD (bit 7). Refer to the description of the ADC_PD bit for more details.

| 15 | 14 | 13 | 11 | 10 | 9 | 8 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADC_CON <br> V_MODE | 1 | ADC_MEAS_MODE | 0 | 0 | 1 | ADC_- | ADC_DATA_RATE | 0 | 0 | 0 | 0 |  |  |


| Bit 15 | ADC_CONV_MODE: ADC conversion mode/ADC single-shot conversion start. |  |  |
| :---: | :---: | :---: | :---: |
|  | This bit determines the operational status of the device. This bit can only be written when in the ADC power-down mode. When read, this bit gives the status report of the conversion. |  |  |
|  | For a write status: <br> 0 : No effect (default) <br> 1 : Single-shot conversion mode |  |  |
|  | For a read status: <br> 0 : Device currently performing a conversion <br> 1 : Device not currently performing a conversion |  |  |
| Bit 14 | Always write ' 1 '. |  |  |
| Bits[13:11] | ADC_MEAS_MODE: ADC measurement mode selection. |  |  |
|  | These bits set the ADC measurements to be either single-ended or differential. |  |  |
|  | ADC_MEAS_MODE | ADC AINP, AINM |  |
|  | 000 (default) <br> 001 <br> 010 | $\begin{gathered} \text { A1, A2 = differential (default) } \\ \text { A1, AVSS }=\text { single-ended } \\ \text { A2, AVSS }=\text { single-ended } \\ \hline \end{gathered}$ |  |
| Bits[10:8] | Always write '001' |  |  |
| Bit 7 | ADC_PD: ADC Powerdown |  |  |
|  | This bit powers down the ADC_PGA and the ADC. By default, the ADC is powered down (ADC_PDN = ' 1 '). For continuous conversion mode, this bit must to set to ' 0 '. <br> For single-shot mode, this bit must be set to ' 1 ' along with bit 15. During single-shot conversion mode, the device automatically powers up the ADC, triggers one ADC conversion, and then powers down the ADC. |  |  |
|  | ADC_CONV_MODE (Bit 15) | ADC_PDN (Bit 7) | MODE |
|  | $X$ 0 1 | 0 1 (default) 1 (default) | Continuous conversion ADC PD Single-shot |
| Bits[6:4] | ADC_DATA_RATE: Conversion rate select bits. |  |  |
|  | These bits select one of eight diffe <br> 000: 8 SPS <br> 001: 16 SPS <br> 010: 32 SPS <br> 011: 64 SPS <br> 100: 128 SPS (default) <br> 101: 250 SPS <br> 110: 475 SPS <br> 111: 860 SPS | conversion rates. The data rat | ssume a master clock of 1 N |
| Bits[3:0] | Always write '0000'. At power up, | are set as '0011'. |  |

### 7.6.1.3 MISC_REGISTER1 (Address 0x02, Default 0x8000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Bit 15 Always write ' 0 '. At power up, this bit is set as ' 1 '.
Bits[14:0] Not used, always write ' 0 '. At power up, these bits are set as ' 0 '.

### 7.6.1.4 MISC_REGISTER2 (Address Ox03, Default 0x7FFF)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |


| Bit 15 | Always write '1'. At power up, this bit is set as ' 0 '. |
| :--- | :--- |
| Bits[14:0] | Always write '1'. At power up, these bits are set as '1'. |

### 7.6.1.5 DEVICE_CONTROL1 (Address 0x09, Default 0x0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} \mathrm{DAC} \\ \mathrm{PD} \end{gathered}$ | PDB | BCM PDB | $\begin{aligned} & \text { WS } \\ & \text { PD } \end{aligned}$ |


| Bits[15] | Not used. Always write '0'. |
| :---: | :---: |
| Bits[14:13] | Not used. Always write '1'. |
| Bits[12:4] | Not used. Always write '0'. |
| Bit 3 | DAC_PDB: Power down DAC. <br> This bit powers down the weight-scale front-end offset correction DAC and the BCM front-end current source DAC. <br> 0 : Power up DAC (default) <br> 1: Power down DAC |
| Bit 2 | PDB: Power down device. <br> This bit in conjunction with the other power-down bits determines the power state of the device. <br> 0 : Power down (default) <br> 1: Power up of front-end |
| Bit 1 | BCM_PDB: Body composition measurement front-end power-down bit. <br> 0: Power down body compositionmeasurement front-end (default) <br> 1: Power up body composition measurement front-end. Power down the weight scale when powering up the BCM. |
| Bit 0 | WS_PDB: Weight-scale front-end power-down bit. <br> 0: Power down weight-scale front-end (default) <br> 1: Power up weight-scale front-end. Power down BCM when powering up the weight scale. |

Table 3 shows the available power-down modes.
Table 3. Power-Down Modes

| DAC_PDB (Bit3) | $\begin{gathered} \text { PDB } \\ \text { (Bit 2) } \end{gathered}$ | BCM_PDB | $\begin{aligned} & \text { WS_PDB } \\ & \text { (Bit 0) } \end{aligned}$ | ADC_PD <br> (Bit 7, ADC Control Register) | MODE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| X | 0 | 0 | 0 | 1 | Full device power down |
| 1 | 1 | 0 | 0 | 1 | Sleep mode |
| 0 | 1 | 1 | 0 | 0 | Weight-scale power down, body composition measurement |
| 0 | 1 | 0 | 1 | 0 | Body composition measurement power down, weight-scale measurement |
| 0 | 1 | 0 | 0 | 0 | Weight-scale and body composition measurement power down (aux/battery measurement) |

## 7．6．1．6 ISW＿MUX（Address Ox0A，Default 0x0000）

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| n $\stackrel{0}{5}$ $\underline{0}$ | $\begin{aligned} & \text { t} \\ & \stackrel{\rightharpoonup}{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \text { © } \\ & \stackrel{\varrho}{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{\vdots}{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \overline{\mathrm{a}} \\ & \stackrel{1}{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{5} \\ & \underline{0} \end{aligned}$ | RP1 | RP0 | $\begin{aligned} & \text { ñ } \\ & \underline{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \underset{Z}{Z} \\ & \underline{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \stackrel{m}{2} \\ & \underline{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \underset{y}{2} \\ & \underline{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \overline{\mathrm{z}} \\ & \underline{5} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & \text { 은 } \\ & \stackrel{0}{0} \end{aligned}$ | RN1 | RN0 |


| Bits［15：10］ | IOUTP［5：0］ |
| :---: | :---: |
|  | These bits close the switches routing IOUTPx to the output of OPAMP1． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［9：8］ | RP［1：0］ |
|  | These bits close the switches routing the calibration signal to the output of OPAMP1． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［7：2］ | IOUTN［5：0］ |
|  | These bits close the switches routing IOUTNx to the negative input of OPAMP1． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［1：0］ | RN［1：0］ |
|  | These bits close the switches routing the calibration signal to the negative input of OPAMP1． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |

## 7．6．1．7 VSENSE＿MUX（Address 0x0B，Default 0x0000）

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\bar{\square}$ |  |  |  |  |  |  |  | $\underset{\square}{\square}$ | $\stackrel{\square}{\square}$ |
| － | － | － | － | － | － |  |  | $\sum_{u}$ | $\underset{\sim}{\square}$ | U | $\underset{\sim}{u}$ | $\underset{\sim}{7}$ | U | $\sum$ | $\sum_{i}^{1}$ |
| $\stackrel{0}{2}$ | $\stackrel{0}{2}$ | $\stackrel{0}{2}$ | $\stackrel{0}{2}$ | $\stackrel{0}{2}$ | $\stackrel{0}{2}$ | 心 | $\stackrel{\rightharpoonup}{\mathscr{\infty}}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | 0 | © | ๗ |
| 山 | 山 | 山 | 山 | 山 | 山 | $\geq$ | $\geq$ | 山 | 山 | 山 | 山 | 山 | 山 | Z | 2 |
| $>$ |  |  |  |  |  | $\stackrel{\omega}{\infty}$ | $\stackrel{\omega}{\infty}$ | $9$ | $9$ | $9$ | $\stackrel{\square}{3}$ |  | 9 | $\stackrel{3}{3}$ |  |


| Bits［15：10］ | VSENSEPx［5：0］ |
| :---: | :---: |
|  | These bits close the switches routing VSENSEPx to the positive input of the receive amplifier． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［9：8］ | VSENSEP＿Rx［1：0］ |
|  | These bits close the switches routing the calibration signal to the positive input of the receive amplifier． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［7：2］ | VSENSENx［5：0］ |
|  | These bits close the switches routing VSENSENx to the negative input of the receive amplifier． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |
| Bits［1：0］ | VSENSEM＿Rx［1：0］ |
|  | These bits close the switches routing the calibration signal to the negative input of the receive amplifier． |
|  | 0 ：Switch is open（default） <br> 1：Switch is closed |

### 7.6.1.8 IQ_MODE_ENABLE (Address Ox0C, Default Ox0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | IQ MODE ENABLE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| Bits[15:12] | Not used. Always write ' 0 '. |
| :--- | :--- |
| Bit 11 | IQ_MODE_ENABLE: Enable the I/Q demodulator. |
|  | This bit sets the impedece measurement mode to either full-wave rectifier mode or I/Q demodulator mode. For I/Q |
|  | Demodulator mode, the DAC_FREQ bits of the BCM_DAC_FREQ register and the IQ_DEMOD_CLK_DIV_FAC bits of |
| the DEVICE_CONTROL2 register must be set appropriately. Refer to the respective register section for more details. |  |
|  | 0: Full-Wave Rectifier mode (default) <br>  <br>  <br>  <br> 1: I/Q Demodulator mode |
|  | Not used. Always write ' $\mathbf{0}$ '. |

### 7.6.1.9 WEIGHT_SCALE_CONTROL (Address OxOD, Default 0x0000)

| 15 | 1413 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | WS_PGA GAIN | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | OFFSET_DAC_VALUE |  |  |  |  |

Bit 15 Not used. Always write ' 0 '.
Bits[14:13] WS_PGA_GAIN: Sets the second-stage gain of the weight-scale front-end.
00: Gain = 1 (default)
01: Gain $=2$
10: Gain $=3$
11: Gain = 4
Bits[12:6] Not used. Always write ' 0 '.
Bit[5:0]
OFFSET_DAC_VALUE: Offset correction DAC setting.
These bits set the value for the DAC used to correct the input offset of the weight-scale front-end. The correction is made at the second stage. The offset correction at the output of the first stage is given by OFFSET_DAC_VALUE $\times$ 31.2 mV . Note that OFFSET_DAC_VALUE is a number from -32 to 31 , in twos complement; default is ' 000000 '.

### 7.6.1.10 BCM_DAC_FREQ (Address 0xOE, Default 0x0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | 0 | DAC9 | DAC8 | DAC7 | DAC6 | DAC5 | DAC4 | DAC3 | DAC2 | DAC1 | DAC0 |

## Bits[15:910]

Bits[9:0]

Not used. Always write '0'.
DAC[9:0]: Sets the frequency of the BCM excitation current source.
The DAC output frequency is given by DAC[9:0] $\times \mathrm{f}_{\mathrm{CLK}} / 1024$, where $f_{C L K}$ is the frequency of the device input clock (pin 79). All combinations of the DAC frequency can be used for the full-wave rectifier mode. However, only certain combinations of the DAC frequency can be used for the IQ demodulator mode. Refer to the description of the DEVICE_CONTROL2 register for more details.

For example, with $f_{C L K}=1.024 \mathrm{MHz}$ :
DAC $=0 \times 00 \mathrm{FF} \rightarrow 255 \mathrm{kHz}$
DAC $=0 \times 0001 \rightarrow 1 \mathrm{kHz}$

### 7.6.1.11 DEVICE_CONTROL2 (Address Ox0F, Default Ox0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | IQ_DEMOD_CLK_ <br> DIV_FAC | 0 | 0 | 0 | BAT_MON_ $^{\text {EN } 1}$ | 0 | 0 | 0 | 0 | BRIDGE_SEL | BAT_MON_ <br> ENO |  |  |


| Bits[15:14] | Not used. Always write '0'. |
| :---: | :---: |
| Bits[13:11] | IQ_DEMOD_CLK_DIV_FAC: I/Q demodulator clock frequency. |
|  | The clock for the IQ demodulator (IQ_DEMOD_CLK signal) is internally generated from the device input clock (f fLK ) by a divider controlled by this register. Note that the IQ_DEMOD_CLK must be four times the BCM_DAC_FREQ so that the phases for the mixers can be generated (that is, IQ_DEMOD_CLK $=\mathrm{f}_{\mathrm{CLK}} /(\operatorname{IQ}$ DEMOD_CLK_DIV_FAC) $=$ BCM_DAC_FREQ $\times 4$ ) |
|  | 000: Divide by 1 (default) |
|  | 001: Divide by 2 |
|  | 010: Divide by 4 |
|  | 011: Divide by 8 |
|  | 100: Divide by 16 |
|  | Others: Divide by 32 |
| Bit 7 | BAT_MON_EN1: This bit (along with BAT_MON_EN0, bit 0) enables battery monitoring. |
|  | When disabled, the battery monitoring block is powered down to save power. See the description of BAT_MON_ENO, bit 0 . |
| Bits[6:3] | Not used. Always write '0'. |
| Bits[2:1] | BRIDGE_SEL: Selects one of the four input pairs to be routed to the weight-scale front-end. |
|  | 00: Bridge 1 (INP1, INM1) connected to the weight-scale front-end (default) |
|  | 01: Bridge 2 (INP2, INM2) connected to the weight-scale front-end |
|  | 10: Bridge 3 (INP3, INM3) connected to the weight-scale front-end |
|  | 11: Bridge 4 (INP4, INM4) connected to the weight-scale front-end. |
| Bit 0 | BAT_MON_EN0: This bit along with BAT_MON_EN1 (Bit[7]) enables battery monitoring. |
|  | 00: Monitor disabled (default) <br> 11. Monitor enabled (AVDD / 3) |
|  | 11. Monitor enabled (AVDD 3) 3 |
|  | NOTE: The PERIPHERAL_SEL bits of the ADC_CONTROL_REGISTER2 must be set to ' 10001 ' in order to route the battey monitor output to the ADC. |

7.6.1.12 ADC_CONTROL_REGISTER2 (Address 0x10, Default 0x0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| Bits[15:7] | Not used. Always write '0'. |
| :--- | :--- |
| Bits[6:5] | ADC_REF_SEL[1:0]: Selects the reference for the ADC. |
|  | 00: ADCREF connected to VLDO. Used for ratiometric weight-scale measurement (default). |
| 01, 10: Do not use |  |
| Bits[4:0] | 11: ADCREF connected to VREF (internal voltage reference generator). Used for impedance measurement. |
|  | PERIPHERAL_SEL[4:0]: Selects the signals that are connected to the ADC. |
|  | 00000: Output of the weight-scale front-end (default) |
|  | 00011: Output of the body composition measurement front-end (OUTP_FILT/OUTM_FILT) |
|  | 00101: Output of the body composition measurement front-end (OUTP_Q_FILT/OUTM_Q_FILT) |
|  | 01001: AUX1 signal for single-ended measurement. Also set bit[13:11] of the ADC_CONTROL_REGISTER1 to '001'. |
|  | 10001: AUX2 signal for single-ended measurement. Also set bit[13:11] of the ADC_CONTROL_REGISTER1 to '010'. |
|  | 11001: AUX2 and AUX1 signal for differential measurement (AUX2-AUX1). Also set bit[13:11] of the |

NOTE: All other bit combinations are invalid.
7.6.1.13 MISC_REGISTER3 (Address 0x1A, Default 0x0000)

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |


| Bits[15:6] | Not used. Always write ' 0 '. |
| :--- | :--- |
| Bits[5:4] | Always write '1'. |
| Bits[3:0] | Not used. Always write ' 0 '. |

## 8 Application and Implementation

## NOTE

Information in the following applications sections is not part of the Tl component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

### 8.1.1 BCM Channel Connections

The suggested connections of the BCM excitation and sense electrodes to the device pins are shown in Figure 12. The circuit shows an electrical model of the body impedance being measured ( $\mathrm{R}_{\text {BODY }}$ ) along with models for the electrode contact impedances. The components connecting the electrodes to the IOUTx and VSENSEx pins are meant to be replicated in the path of the calibration impedances as well. Suggestions for the component values are shown in Table 4.


RE1, RE2, RE3, and RE4 model the electrode contact impedance.
$R_{\text {BODY }}$ models the body impedance (replaced by the calibration resistance in the calibration path).

Figure 12. Connection of BCM Pins to Electrodes

Table 4. Component Values Corresponding to Figure $12^{(1)}$

| COMPONENT | ILLUSTRATIVE VALUE |  |
| :--- | :--- | :--- |
| R1, R2 | $10 \mathrm{k} \Omega$ | Provides a dc feedback for the excitation op amp. |
| $\mathrm{C} 1, \mathrm{C} 2$ | $1 \mu \mathrm{~F}$ | Low-impedance path for the 50-kHz excitation, high impedance for dc currents. |
| C 3 | 47 pF | Optional shunt capacitor across the excitation op amp to improve stability. |
| R3, R4 | $10 \mathrm{k} \Omega$ | Sets the dc voltage at the VSENSEx pins. |
| C4, C5 | $1 \mu \mathrm{~F}$ | Low-impedance path for the $50-\mathrm{kHz}$ excitation, high impedance for dc currents <br> (patient safety). |

[^0]AFE4300
www.ti.com.cn

### 8.1.2 Handling Oscillation of the Excitation Amplifier

The phase margin of the excitation amplifier can degrade if there is high capacitance at the input and output terminals. High capacitances can result can result from the capacitances from the electrodes, from protection diodes (for instance, ESD diodes), as well as the capacitance presented by the human body. Degradation of phase margin resulting from high capacitances can result in oscillations leading to reduced measurement accuracy. One way to improve the phase margin of the excitation amplifier is to introduce a series R-C at the output of the excitation amplifier in every measurement. This process is done using the components $\mathrm{R}_{\mathrm{CM}}=1 \mathrm{k} \Omega$ and $\mathrm{C}_{\mathrm{CM}}=1 \mathrm{nF}$ in the simplistic model shown in Figure 13. This illustration is for a case where IOUT0 and IOUT1 are switched to the input and output of the excitation amplifier, respectively.


Figure 13. Oscillation Fix of the Excitation Amplifier
Such a scheme can be implemented in one of two methods:

1. A separate $\mathrm{R}_{\mathrm{CM}}-\mathrm{C}_{\mathrm{CM}}$ for every IOUTx and RPx pin that gets switched to the excitation amplifier output.
2. A single $R_{C M}-C_{C M}$ on one of the RPx pins that gets switched to the excitation amplifier output during calibration. When not using this RPx pin, still switch the same RPx pin to the output of the excitation amplifier (in addition to whichever other pin is switched to the output) so that the $\mathrm{R}_{\mathrm{CM}}-\mathrm{C}_{\mathrm{CM}}$ still gets connected to the output of the excitation amplifier.
Method 2 is preferable because this method involves only one $\mathrm{R}_{\mathrm{CM}}$ and one $\mathrm{C}_{\mathrm{CM}}$.

### 8.1.3 Achieving Deterministic Phase in the IQ Mode

The DAC frequency generator (DDS) is initialized on the register update of the DAC frequency register. The IQ demod clock divider is updated on the divider register value. Because the registers are written through the SPI interface (that is, asynchronous to the device clock), every time either of these registers are written, the phase relation between the DAC output and the I-Q demod clock can get altered. This alteration in phase relation can cause the phase of the I-Q measurement to be non-deterministic.
Two ways of circumventing this issue are:

1. Do a fresh calibration (measuring all the calibration impedances) each time the registers are reprogrammed for a new excitation frequency
2. Use an SPI clock synchronous with the device clock and follow the sequence below whenever the DACOUT frequency is to be changed:
3. Write 0 to register 15 (set the IQ divider to 1 )
4. Write 0 to register 14 (DACOUT frequency is cleared)
5. Write the required DAC frequency to register 14
6. Write the required IQ_DEMOD_CLK_DIV to register 15

### 8.2 Typical Application

A typical application of the AFE4300 is a weight scale, as shown in Figure 14, that includes a weight measurement as well as a body impedance measurement with the architecture.


Figure 14. Weight Scale Application
The weight applied on a load-cell generates the differential voltage that is converted by the weight scale signal chain of the AFE. For the body impedance measurement, a sinusoidal current (most commonly at a frequency of 50 kHz ) is injected into a pair of electrodes that make contact with the human body. Two more electrodes serve as sense electrodes and the differential voltage developed across the sense electrodes is measured and digitized by the AFE. The whole system is clocked using an external clock source.

### 8.2.1 Design Requirements

Table 5 shows the typical requirements of a weight scale design using the AFE.
Table 5. Weight Scale Design Requirements

| PARAMETER | EXAMPLE VALUE | COMMENTS |
| :---: | :---: | :---: |
| AVDD | 3.3 V | Have enough margin for the dc inaccuracy and minimize ripple. For the batteryoperated device, an LDO can be used to derive AVDD. Place decoupling capacitors close to the AFE. |
| Load-cell excitation voltage | 1.7 V | $\mathrm{V}_{\text {LDO }}$ is generated by the AFE and must be used as the load-cell excitation source. Because $\mathrm{V}_{\mathrm{LDO}}$ is used as the reference for the ADC in the weight scale signal chain, using $\mathrm{V}_{\text {LDO }}$ as the excitation voltage for the load-cell makes the measurement ratio-metric and compensates errors resulting from variation in $\mathrm{V}_{\text {LDO }}$. |
| External clock frequency | 1.024 MHz | - |
| BCM excitation frequency | 50 kHz (set by programming the AFE) | For single-frequency body impedance analysis, the most commonly used frequency is 50 kHz . |
| Skin-electrode contact impedance | A few $100 \Omega$ or lower | The electrodes must have a big enough contact area with the body in order to minimize the electrode-skin contact impedance (ac value at the excitation frequency). |

### 8.2.2 Detailed Design Procedure

A body impedance measurement is usually performed using four electrodes: a pair of excitation electrodes and a pair of sense electrodes. Body contact to each electrode involves a series impedance resulting from the skinelectrode interface. On the excitation side, this contact impedances come in series with the body impedance and cause the voltage swing on the excitation terminals of the AFE to increase. Excessive contact impedances on the excitation electrodes can therefore cause the excitation amplifier to saturate even while measuring normal ranges of body impedance. On the sense electrodes, the input impedance of the receiver is $50 \mathrm{k} \Omega$. As a result, the contact impedances on the sense electrodes cause a small attenuation in the effective signal input to the receiver. For these reasons, the ac contact impedance at the excitation frequency must be minimized on both the excitation and sense electrodes.
To deduce an accurate impedance value from the AFE output in the body impedance measurement requires calibration relative to known impedances. Calibration is usually performed by measuring two or more known impedances and by constructing a piece-wise linear curve between the AFE output and the impedance.
To conserve power when not used, the AFE can be put in a sleep mode in which all signal chains are powered down. This mode reduces the average power consumption significantly. When the user issues a power-up interrupt (pressing a button or so forth) to the system, the AFE can be programmed to come out of sleep mode, perform the measurement, and go back to sleep again. To account for drifts with time, TI recommends that calibration be done every time the AFE is woken up. For the BCM measurement, TI recommends measuring the calibration impedances before every fresh measurement of body impedance. For the weight scale measurement, TI recommends measuring the channel offset (the AFE output without any load) before the measurement of the load. Also after every wake-up, provide sufficient time for the signal chain to settle before doing any measurements.
To meet product-level ESD requirements, additional external ESD protection diodes may need to be used to protect the AFE pins that interface with the electrodes.

### 8.2.3 Application Curve

Figure 15 shows the linearity of the BCM up to $2.5 \mathrm{k} \Omega$. As seen the figure, the maximum impedance that can be measured for the default configuration using the AFE4300 is typically $2.5 \mathrm{k} \Omega$. However for better performance, TI suggests limiting the impedance to $1175 \Omega$. If higher impedance must be measured, the excitation current can be reduced by placing an external resistor of $1.5 \mathrm{k} \Omega$ (between DACOUT and DAC_FILT_IN), which increases the range by roughly $2 x$.


Figure 15. Body Impedance to Output Voltage Transfer Curve

## AFE4300

## 9 Power Supply Recommendations

### 9.1 Power-Supply Recommendation and Initialization

The device has an analog supply (AVDD). Drive these pins with a clean supply and connect bypass capacitors close to the pins. After power up, the device must be reset to set all internal registers to their default state. Resetting the device is done by applying an active low pulse on the RST pin after the power supplies stabilize. As part of the reset process, the AFE4300 sets all register bits to the respective default settings.
Some register bits must be written to values different from their default values after reset for proper operation. By default, the AFE4300 enters into a power-down state at start-up. The startup and initialization for the device is shown in Figure 16 and Table 6 lists the recommended timing values.


Figure 16. Power-Up and Initialization

Table 6. Timing Parameters for Figure 16

|  |  | NOM | UNIT |
| :--- | :--- | ---: | :---: |
| $\mathrm{t}_{1}$ | Time between supplies turning on and an active $\overline{\text { RST }}$ | $>10$ | ms |
| $\mathrm{t}_{2}$ | Active $\overline{\text { RST }}$ duration | $>50$ | $\mu \mathrm{~s}$ |
| $\mathrm{t}_{3}$ | Time between $\overline{\text { RST }}$ and register writes | $>1$ | ms |

## 10 Layout

## 10．1 Layout Guidelines

The following points must be considered during layout：
－All input signals（INPx，INMx，VSENSEx，IOUTs）must be routed differentially with equal length
－Input signals must be isolated from high－frequency signals using a ground plane or a ground trace
－Special care（such as avoiding vias，test points，and so forth）must be given to minimize the parasitic capacitances in the input circuit of the BCM

## 10．2 Layout Example



Figure 17．Example Layout

## 11 器件和文档支持

## 11.1 接收文档更新通知

要接收文档更新通知，请导航至 TI．com 上的器件产品文件夹。单击右上角的通知我 进行注册，即可每周接收产品信息更改摘要。有关更改的详细信息，请查看任何已修订文档中包含的修订历史记录。

## 11.2 社区资源

下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商＂按照原样＂提供。这些内容并不构成 TI 技术规范，并且不一定反映 TI 的观点；请参阅TI的《使用条款》。
TI E2ETM 在线社区 $T I$ 的工程师对工程师（E2E）社区。此社区的创建目的在于促进工程师之间的协作。在 e2e．ti．com 中，您可以咨询问题，分享知识，拓展思路并与同行工程师一道帮助解决问题。
设计支持 $\quad T I$ 参考设计支持 可帮助您快速查找有帮助的 E2E 论坛，设计支持工具以及技术支持的联系信息。
11.3 商标

E2E is a trademark of Texas Instruments．
SPI is a trademark of Motorola Mobility LLC．
All other trademarks are the property of their respective owners．
11.4 静电放电警告

ESD 可能会损坏该集成电路。德州仪器（TI）建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序，可能会损坏集成电路。
ESD 的损坏小至导致微小的性能降级，大至整个器件故障。精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

## 11．5 Glossary

SLYZ022－TI Glossary．
This glossary lists and explains terms，acronyms，and definitions．

## 12 机械，封装和可订购信息

以下页面包含机械，封装和可订购信息。这些信息是指定器件的最新可用数据。这些数据如有变更，恕不另行通知和修订此文档。如欲获取此数据表的浏览器版本，请参阅左侧的导航。

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE4300PN | ACTIVE | LQFP | PN | 80 | 119 | RoHS \& Green | NIPDAU | Level-3-260C-168 HR | 0 to 70 | AFE4300 | Samples |
| AFE4300PNR | ACTIVE | LQFP | PN | 80 | 1000 | RoHS \& Green | NIPDAU | Level-3-260C-168 HR | 0 to 70 | AFE4300 | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as " Pb -Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the $<=1000$ ppm threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer:The information provided on this page represents Tl's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

TeXAS

## TAPE AND REEL INFORMATION


*All dimensions are nominal

| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> W1 $(\mathbf{m m})$ | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | W <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE4300PNR | LQFP | PN | 80 | 1000 | 330.0 | 24.4 | 16.0 | 16.0 | 2.0 | 24.0 | 24.0 | Q2 |

PACKAGE MATERIALS INFORMATION


All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE4300PNR | LQFP | PN | 80 | 1000 | 367.0 | 367.0 | 55.0 |

## TRAY



Chamfer on Tray corner indicates Pin 1 orientation of packed units.
*All dimensions are nominal

| Device | Package <br> Name | Package <br> Type | Pins | SPQ | Unit array <br> matrix | Max <br> temperature <br> $\left({ }^{\circ} \mathbf{C}\right)$ | L (mm) | W <br> $(\mathbf{m m})$ | K0 <br> $(\boldsymbol{\mu m})$ | P1 <br> $(\mathbf{m m})$ | $\mathbf{C L}$ <br> $(\mathbf{m m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE4300PN | PN | LQFP | 80 | 119 | $7 \times 17$ | 150 | 315 | 135.9 | 7620 | 17.9 | 14.3 |
| $(\mathbf{m m})$ |  |  |  |  |  |  |  |  |  |  |  |



NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC registration MS-026.


NOTES: (continued)
4. Publication IPC-7351 may have alternate designs.
5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
6. For more information, see Texas Instruments literature number SLMA004 (www.ti.com/lit/slma004).


SOLDER PASTE EXAMPLE BASED ON 0.1 mm THICK STENCIL

SCALE:6X

NOTES: (continued)
7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.

## 重要声明和免责声明

TI＂按原样＂提供技术和可靠性数据（包括数据表），设计资源（包括参考设计），应用或其他设计建议，网络工具，安全信息和其他资源不保证没有瑕疵且不做出任何明示或暗示的担保，包括但不限于对适销性，某特定用途方面的适用性或不侵犯任何第三方知识产权的暗示担保。

这些资源可供使用 TI 产品进行设计的熟练开发人员使用。您将自行承担以下全部责任：（1）针对您的应用选择合适的 TI 产品，（2）设计，验证并测试您的应用，（3）确保您的应用满足相应标准以及任何其他功能安全，信息安全，监管或其他要求。
这些资源如有变更，恕不另行通知。TI 授权您仅可将这些资源用于研发本资源所述的 TI 产品的应用。严禁对这些资源进行其他复制或展示。您无权使用任何其他 TI 知识产权或任何第三方知识产权。您应全额赔偿因在这些资源的使用中对 TI 及其代表造成的任何索赔，损害，成本，损失和债务，TI 对此概不负责。

TI 提供的产品受 TI 的销售条款或 ti．com 上其他适用条款／TI 产品随附的其他适用条款的约束。TI 提供这些资源并不会扩展或以其他方式更改 TI 针对 TI 产品发布的适用的担保或担保免责声明。

TI 反对并拒绝您可能提出的任何其他或不同的条款。

邮寄地址：Texas Instruments，Post Office Box 655303，Dallas，Texas 75265
Copyright © 2022 ，德州仪器（TI）公司


[^0]:    (1) The indicated component values are only for illustration. The actual choice of circuit configuration and component values in a product can be governed by other considerations (such as patient safety and so forth).

