## Test Data <br> For PMP7969 <br> 3/9/2015

## 惟 Texas Instruments

Test SPECIFICATIONS

| Vin Min. | 9V DC |
| :--- | :--- |
| Vin Max. | 16V DC |
| Vout | 24 V DC |
| lout | $25 \mathrm{~A} \mathrm{Max}$. |
| Target Switching Frequency | 1.6 MHz (400KHz per phase) |

## Circuit Description

PMP7969 is a 4-Phase Synchronous Boost Converter with the added capability of enabling and disabling each individual phase either manually, via 5 pin jumper, or using an MCU or other control circuitry. It is designed to accept an input range of 9VDC-to-16VDC. The output is set to 24VDC and can supply a maximum of 25 A of current to the load.

Note that hiccup mode will function only when all four phases are enabled. If three or less phases are enabled switching of all enabled phases will stop, all FETs will be OFF, and current will conduct through the body diode of all four synchronous FETs and the output voltage will be the input voltage minus the voltage drop of the four paralleled synchronous FET body diodes.

## FABRICATION

Board Dimensions: 4.5" x 7"


Board Photo (Top)

INSTRUMENTS


Board Photo (Bottom)

Thermal Data


IR thermal image taken at steady state at 18A load and Vin $=9 \mathrm{~V}$ with no airflow (thermal image taken is upside-down relative to photo of board displayed above; for improved thermal performance, it is recommended to use $\mathbf{2 o z}$ Copper or heavier, heatsinks for the FETs, and/or airflow)


IR thermal image taken at steady state at Full (25A) load and Vin $=16 \mathrm{~V}$ with no airflow (thermal image taken is upside-down relative to photo of board displayed above; for improved thermal performance, it is recommended to use $\mathbf{2 o z}$ Copper or heavier, heatsinks for the FETs, and/or airflow)

TYPICAL PERFORMANCE

## EFFICIENCY



## Efficiency Data

| $\operatorname{Vin}(\mathrm{V})$ | $\operatorname{lin}(\mathrm{A})$ | $\operatorname{Vout}(\mathrm{V})$ | $\operatorname{lout}(\mathrm{A})$ | Efficiency(\%) |
| ---: | ---: | ---: | ---: | ---: |
| 9.008 | 0.31 | 24.026 | 0 | 0 |
| 9.008 | 4.2 | 24.023 | 1.42 | 90.165 |
| 9.007 | 6.95 | 24.022 | 2.42 | 92.867 |
| 9.007 | 9.76 | 24.021 | 3.42 | 93.452 |
| 9.007 | 12.58 | 24.02 | 4.42 | 93.699 |
| 9.006 | 15.32 | 24.019 | 5.42 | 94.355 |
| 9.006 | 18.08 | 24.017 | 6.42 | 94.694 |
| 9.006 | 20.86 | 24.016 | 7.42 | 94.855 |
| 9.005 | 23.63 | 24.015 | 8.42 | 95.027 |
| 9.005 | 26.4 | 24.014 | 9.42 | 95.154 |
| 9.004 | 29.2 | 24.012 | 10.42 | 95.165 |
| 9.004 | 32.02 | 24.011 | 11.42 | 95.109 |
| 9.004 | 34.83 | 24.01 | 12.42 | 95.088 |
| 9.003 | 37.65 | 24.008 | 13.42 | 95.051 |
| 9.003 | 40.5 | 24.007 | 14.42 | 94.943 |

INSTRUMENTS

| 9.003 | 43.37 | 24.006 | 15.42 | 94.804 |
| ---: | ---: | ---: | ---: | ---: |
| 9.002 | 46.24 | 24.004 | 16.42 | 94.689 |
| 9.002 | 49.1 | 24.003 | 17.42 | 94.6 |
| 9.002 | 51.99 | 24.002 | 18.42 | 94.467 |
| 9.001 | 54.9 | 24 | 19.42 | 94.319 |
| 9.001 | 57.82 | 23.999 | 20.44 | 94.255 |


| Vin(V) | $\operatorname{lin}(\mathrm{A})$ | Vout(V) | lout(A) | Efficiency(\%) |
| :---: | :---: | :---: | :---: | :---: |
| 12.01 | 0.28 | 24.029 | 0 | 0 |
| 12.008 | 3.18 | 24.027 | 1.42 | 89.349 |
| 12.009 | 5.21 | 24.026 | 2.42 | 92.929 |
| 12.008 | 7.25 | 24.025 | 3.42 | 94.38 |
| 12.009 | 9.32 | 24.024 | 4.42 | 94.873 |
| 12.009 | 11.4 | 24.024 | 5.42 | 95.111 |
| 12.008 | 13.5 | 24.022 | 6.42 | 95.135 |
| 12.007 | 15.56 | 24.021 | 7.42 | 95.401 |
| 12.007 | 17.61 | 24.02 | 8.42 | 95.651 |
| 12.009 | 19.66 | 24.019 | 9.42 | 95.833 |
| 12.007 | 21.72 | 24.018 | 10.42 | 95.964 |
| 12.006 | 23.8 | 24.016 | 11.42 | 95.982 |
| 12.006 | 25.87 | 24.015 | 12.42 | 96.031 |
| 12.006 | 27.93 | 24.014 | 13.42 | 96.105 |
| 12.005 | 30.02 | 24.013 | 14.42 | 96.081 |
| 12.005 | 32.11 | 24.012 | 15.42 | 96.053 |
| 12.005 | 34.2 | 24.011 | 16.44 | 96.144 |
| 12.005 | 36.28 | 24.009 | 17.42 | 96.027 |
| 12.004 | 38.37 | 24.008 | 18.42 | 96.013 |
| 12.004 | 40.48 | 24.007 | 19.42 | 95.945 |
| 12.004 | 42.59 | 24.006 | 20.44 | 95.977 |
| 12.004 | 44.7 | 24.005 | 21.44 | 95.916 |
| 12.004 | 46.8 | 24.003 | 22.44 | 95.877 |
| 12.004 | 48.93 | 24.002 | 23.44 | 95.786 |
| 12.003 | 51.07 | 24.001 | 24.44 | 95.692 |
| 12.003 | 53.2 | 24 | 25.44 | 95.615 |


| $\operatorname{Vin}(\mathrm{V})$ | $\operatorname{lin}(\mathrm{A})$ | $\operatorname{Vout}(\mathrm{V})$ | $\operatorname{lout}(\mathrm{A})$ | Efficiency(\%) |
| ---: | ---: | ---: | ---: | ---: |
| 16.009 | 0.22 | 24.03 | 0 | 0 |
| 16.011 | 2.37 | 24.029 | 1.42 | 89.92 |
| 16.009 | 3.9 | 24.027 | 2.42 | 93.129 |


| 16.009 | 5.42 | 24.027 | 3.42 | 94.703 |
| ---: | ---: | ---: | ---: | ---: |
| 16.008 | 6.95 | 24.026 | 4.42 | 95.451 |
| 16.008 | 8.49 | 24.025 | 5.42 | 95.812 |
| 16.008 | 10.06 | 24.024 | 6.42 | 95.773 |
| 16.008 | 11.61 | 24.023 | 7.42 | 95.91 |
| 16.008 | 13.13 | 24.022 | 8.42 | 96.232 |
| 16.007 | 14.65 | 24.021 | 9.42 | 96.493 |
| 16.007 | 16.19 | 24.02 | 10.42 | 96.579 |
| 16.008 | 17.72 | 24.019 | 11.42 | 96.699 |
| 16.007 | 19.25 | 24.018 | 12.42 | 96.809 |
| 16.007 | 20.78 | 24.017 | 13.42 | 96.898 |
| 16.007 | 22.32 | 24.016 | 14.42 | 96.931 |
| 16.007 | 23.87 | 24.015 | 15.42 | 96.918 |
| 16.007 | 25.41 | 24.014 | 16.44 | 97.063 |
| 16.006 | 26.94 | 24.013 | 17.42 | 97.009 |
| 16.006 | 28.49 | 24.012 | 18.42 | 96.994 |
| 16.006 | 30.04 | 24.011 | 19.44 | 97.079 |
| 16.005 | 31.59 | 24.01 | 20.44 | 97.066 |
| 16.006 | 33.14 | 24.009 | 21.44 | 97.043 |
| 16.006 | 34.68 | 24.008 | 22.42 | 96.968 |
| 16.006 | 36.23 | 24.007 | 23.44 | 97.039 |
| 16.005 | 37.8 | 24.006 | 24.44 | 96.978 |
| 16.005 | 39.36 | 24.005 | 25.44 | 96.941 |

## Waveforms

## Switch Nodes



Switch Nodes of all 4 phases at Vin = 9V and 21A Load


Switch Nodes of all 4 phases at Vin = 11V and Full (25A) Load


Switch Nodes of all 4 phases at Vin = 13V and Full (25A) Load


Switch Nodes of all 4 phases at Vin = 16V and Full (25A) Load

Load Transient Response


Load Transient Response at Vin $=9 \mathrm{~V}$ with 50\%-to-100\% (12.5A-to-25A) Load Step

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Load Transient Response at Vin = 11V with 50\%-to-100\% (12.5A-to-25A) Load Step

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Load Transient Response at Vin $=13 \mathrm{~V}$ with $50 \%$-to-100\% (12.5A-to-25A) Load Step


Load Transient Response at Vin = 16V with 50\%-to-100\% (12.5A-to-25A) Load Step

## Startup



Startup into No Load (Vin = 9V)

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Startup into No Load (Vin = 11V)

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Startup into No Load (Vin = 13V)

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Startup into No Load (Vin = 16V)

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Startup into 21A Load (Vin = 9V) Note: Load current limited by available supply current limit.

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Startup into Full (25A) Load (Vin = 11V)

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Startup into Full (25A) Load (Vin = 13V)


Startup into Full (25A) Load (Vin = 16V)

Output Voltage Ripple and Switch Node Voltage


Output Voltage Ripple and Switch Node Voltage (Phase 1) at Vin =9V and 21A Load (Vripple $\approx$ 330 mVp -p)


Output Voltage Ripple and Switch Node Voltage (Phase 1) at Vin = 11V and 25A Load (Vripple $\approx$ 300mVp-p)


Output Voltage Ripple and Switch Node Voltage (Phase 1) at Vin = 13V and 25A Load (Vripple $\approx$ 230mVp-p)


Output Voltage Ripple and Switch Node Voltage (Phase 1) at Vin = 16V and 25A Load (Vripple $\approx$ 245mVp-p)

## Control Loop Response



Control Loop Response at Vin =9V and OA Load; Phase Margin = $\mathbf{7 4}$ deg.; Gain Margin $=-45 \mathrm{~dB}$


Control Loop Response at Vin = 9V and 21A Load; Phase Margin = 59.6 deg.; Gain Margin = -9.8 dB

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## Control Loop Response at Vin = 16V and OA Load; Phase Margin = 65.4 deg.; Gain Margin =-36.3 dB



Control Loop Response at Vin = 16V and 25A Load; Phase Margin = 53.3 deg.; Gain Margin = -13.5 dB

Current Sharing

| Test Condition = 16Vin and 25A Load |  |
| :---: | :---: |
| Phase | Current (A) |
| Phase 1 (Master) | 12.27 |
| Phase 2 | 9.27 |
| Phase 3 | 8.7 |
| Phase 4 | 8.23 |

## Current Cutoff Data

| Input Voltage (V) | Enabled Phase | Cutoff Current (A) |
| :---: | :---: | :---: |
| 16 | Phase 1 Only (Master) | 23.542 |
| 22 | Phase 1 Only (Master) | 24.87 |
| 16 | Phase 1 (Master) and Phase 2 | 44.459 |
| 22 | Phase 1 (Master) and Phase 2 | 46.062 |
| 16 | Phase 1 (Master) and Phase 3 | 42.653 |
| 22 | Phase 1 (Master) and Phase 3 | 45.128 |
| 16 | Phase 1 (Master) and Phase 4 | 42.532 |
| 22 | Phase 1 (Master) and Phase 4 | 45.617 |
| N/A* | All four phases | N/A (Overcurrent hiccup should <br> take place, but is not tested*) |

*NOTE: The above cutoff current tests were performed at 16 Vin and 22 Vin and with only one or two phases enabled due to the current limitations of the input supply used/available. The term "cutoff current" implies that the controllers stopped switching at the noted input current values. During this time all FETs are OFF and the currents pass through the body diodes of all four synchronous FETs from the input to the output load. Hiccup mode should be enabled and working only with all four phases being enabled. This has not been tested, though, due to the current limitation of the input supply used.

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