







TPS568215

ZHCSFM7C - OCTOBER 2016 - REVISED AUGUST 2023

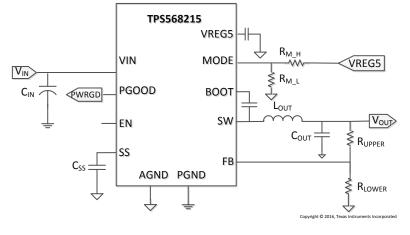
TPS568215 4.5V 至 17V 输入、8A 同步降压 SWIFT

1 特性

- 集成 $19m\Omega$ 和 $9.4m\Omega$ 金属氧化物半导体场效应晶 体管 (MOSFET)
- 400kHz、800kHz 和 1.2MHz 的可选 F_{SW}
- 具有断续重启功能的可调节电流限制设置
- 整个温度范围内的基准电压为 0.6V ±1%
- 支持可选 5V 外部偏置,可提升效率
- D-CAP3™ 控制模式,用于快速瞬态响应
- 可选强制持续导通模式 (FCCM),用于实现窄输出 电压纹波,或自动跳跃 Eco-mode™,用于实现高 轻负载效率
- 0.6V 至 5.5V 输出电压范围
- 支持所有陶瓷电容器
- 单调启动至预偏置输出
- 可调节软启动,默认软启动时间为 1ms
- 40°C 至 150°C 的工作结温范围
- 小型 3.5mm × 3.5mm HotRod™ QFN 封装
- 与 **8A TPS568231** 以及 12A TPS56C231 和 TPS56C215 引脚对引脚兼容
- 在 WEBENCH® 设计中心内受支持

2 应用

服务器和存储



- 机顶盒、高端 DTV
- 电信和网络、负载点 (POL)
- IPC、工厂自动化

3 说明

TPS568215 是 TI 最小的一款单片 8A 同步降压转换 器,具有自适应导通时间 D-CAP3™ 控制模式。该器 件集成了 R_{DS(on)} 较低的功率 MOSFET,简单易用并 且高效运行,所需外部组件最少,适用于空间受限的电 源系统。主要特性包括非常精确的基准电压、快速负载 瞬态响应、自动跳跃模式运行以实现轻负载效率、可调 节的电流限制和无需外部补偿。强制持续导通模式有助 于满足高性能 DSP 和 FPGA 的严格电压调节精度要 求。TPS568215 采用热增强型 18 引脚 HotRod QFN 封装,并且设计为在-40°C至150°C的结温范围内运 行。TPS568215 与 TPS56C215 引脚兼容,因此用户 可以在 6A 至 12A 范围内灵活选择采用同一封装的解 决方案。

封装信息

器件型号	封装 ⁽¹⁾	封装尺寸(标称值)
TPS568215	RNN (VQFN , 18)	3.5mm x 3.5mm

如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。

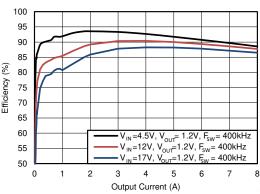




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4 Revision History		

注:以前版本的页码可能与当前版本的页码不同

Changes from Revision B (August 2023) to Revision C (August 2023)	Page
• 向特性列表中添加了引脚兼容数据表链接	
Changes from Revision A (October 2016) to Revision B (August 2023)	Page
更新了整个文档中的表格、图和交叉参考的编号格式 更新了特性列表以包含引脚兼容器件	
Changes from Revision * (October 2016) to Revision A (October 2016)	Page
• 将"产品预发布"更改为"量产数据发布"	
• Changed 图 7-1 image	14

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5 Pin Configuration and Functions

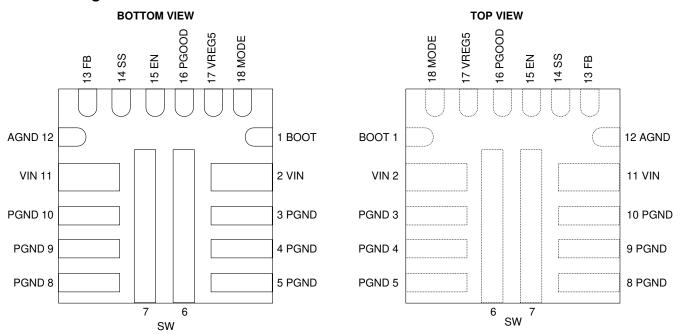


图 5-1. RNN Package 18-Pin VQFN

表 5-1. Pin Functions

Р	N		表 5-1.1 iii i diictions		
					DESCRIPTION
NO.	NAME				
1	воот	I	Supply input for the gate drive voltage of the high-side MOSFET. Connect a 0.1-µF bootstrap capacitor between BOOT and SW.		
2,11 VIN P Input voltage supply pin for the control circuitry. Connect the input decoupling capacitors between PGND.		Input voltage supply pin for the control circuitry. Connect the input decoupling capacitors between VIN and PGND.			
3, 4, 5, 8, 9, 10	PGND	G	Power GND terminal for the controller circuit and the internal circuitry.		
6, 7	SW	0	Switch node terminal. Connect the output inductor to this pin.		
12	AGND	G	Ground of internal analog circuitry. Connect AGND to PGND plane.		
13	FB	I	Converter feedback input. Connect to the resistor divider between output voltage and AGND.		
14	14 SS O		Soft-Start time selection pin. Connecting an external capacitor sets the soft-start time and if no external capacitor is connected, the soft-start time in 1ms.		
15	EN	I	Enable input control, leaving this pin floating enables the converter. It can also be used to adjust the input UVLO by connecting to the resistor divider between VIN and EN.		
16 PGOOD O		0	Open Drain Power Good Indicator, it is asserted low if output voltage is out of PGOOD threshold, Overvoltage or if the device is under thermal shutdown, EN shutdown or during soft start.		
17	VREG5	I/O	4.7-V internal LDO output which can also be driven externally with a 5V input. This pin supplies voltage to the internal circuitry and gate driver. Bypass this pin with a 4.7- μ F capacitor.		
18	MODE	I	Switching Frequency, Current Limit selection and Light load operation mode selection pin. Connect this pin to a resistor divider from VREG5 and AGND for different MODE options shown in table 4.		



6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)

, ,	,	MIN	MAX	UNIT
	VIN	- 0.3	20	
	SW	- 2	19	
	SW(10 ns transient)	- 3	20	
Innut Valtage	EN	- 0.3	6.5	
Input Voltage	BOOT - SW	- 0.3	6.5	V
	BOOT	- 0.3	25.5	
	SS, MODE, FB	- 0.3	6.5	
	VREG5	- 0.3	6	
Output Voltage	PGOOD	- 0.3	6.5	V
Output Current ⁽²⁾	Гоит		10	А
T _J	Operating junction temperature	- 40	150	°C
T _{stg}	Storage temperature	- 55	150	°C

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability

6.2 ESD Ratings

			VALUE	UNIT
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	
V _(ESD)	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±500	V

⁽¹⁾ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
	V _{IN}	4.5		17	
Input Voltage	SW	- 1.8		17	V
Input voltage	BOOT	- 0.1		23.5	v
	VREG5	- 0.1		5.2	
Output Current	I _{LOAD}	0		8	Α
Operating junction temperature	Т	-40		150	°C

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⁽²⁾ To be consistent with the TI reliability requirement of 100k Power-On-Hours at 105°C junction temperature, the output current must not exceed 10A continuously under 100% duty operation as to prevent electromigration failure in the solder. Higher junction temperature or longer power-on hours are achievable at lower than 10A continuous output current.

⁽²⁾ JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.4 Thermal Information

	THERMAL METRIC(1)	RNN PACKAGE	UNIT
	I DERIMAL METRIC	18 PINS	UNII
R ₀ JA	Junction-to-ambient thermal resistance	42.3	°C/W
R _{θ JC(top)}	Junction-to-case (top) thermal resistance	23.9	°C/W
R ₀ JB	Junction-to-board thermal resistance	10.0	°C/W
ΨJT	Junction-to-top characterization parameter	0.5	°C/W
^ф ЈВ	Junction-to-board characterization parameter	10.0	°C/W
R _{θ JC(bot)}	Junction-to-case (bottom) thermal resistance	0.5	°C/W

⁽¹⁾ For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

6.5 Electrical Characteristics

 $T_{.1} = -40$ °C to 150°C, VIN=12V (unless otherwise noted)

	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY CU	JRRENT					
I _{IN}	V _{IN} supply current	T _J = 25°C, V _{EN} =5 V, non switching		600	700	μA
I _{VINSDN}	V _{IN} shutdown current	T _J = 25°C, V _{EN} =0 V		7		μA
LOGIC THR	RESHOLD					
V _{ENH}	EN H-level threshold voltage		1.175	1.225	1.3	V
V _{ENL}	EN L-level threshold voltage		1.025	1.104	1.15	V
V _{ENHYS}				0.121		V
I _{ENp1}	EN pull up ourropt	V _{EN} = 1.0 V	0.35	1.91	2.95	μΑ
I _{ENp2}	EN pull-up current	V _{EN} = 1.3 V	3	4.197	5.5	μΑ
FEEDBACK	(VOLTAGE					
		T _J = 25°C	598	600	602	mV
. ,	FB voltage	T _J = 0°C to 85°C	597.5	600	602.5	mV
V_{FB}		T _J = -40°C to 85°C	594	600	602.5	mV
		T _J = -40°C to 150°C	594	600	606	mV
LDO VOLTA	AGE					
VREG5	LDO Output voltage	T _J = -40°C to 150°C	4.58	4.7	4.83	V
ILIM5	LDO Output Current limit	T _J = -40°C to 150°C	100	150	200	mA
MOSFET						
R _{DS(on)H}	High side switch resistance	T _J = 25°C, V _{VREG5} = 4.7 V		19		mΩ
R _{DS(on)L}	Low side switch resistance	T _J = 25°C, V _{VREG5} = 4.7 V		9.4		mΩ
SOFT STAF	RT					
I _{ss}	Soft start charge current	T _J = -40°C to 150°C	4.9	6	7.1	μA
CURRENT	LIMIT					-
		ILIM-1 option, Valley Current	6	7.1	8.15	Α
I _{OCL}	Current Limit (Low side sourcing)	ILIM option, Valley Current	8	9.4	10.8	Α
	Current Limit (Low side negative)	Valley Current		3		Α
POWER GO	DOD	1				
		V _{FB} falling (fault)		84%		%V _{REF}
.,	DOOOD through all	V _{FB} rising (good)		93%		%V _{REF}
V _{PGOODTH}	PGOOD threshold	V _{FB} rising (fault)		116%		%V _{REF}

 $T_J = -40$ °C to 150°C, VIN=12V (unless otherwise noted)

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
OUTPUT UN	DERVOLTAGE PROTECTION		'			
V _{UVP}	Output UVP threshold	Hiccup detect		68% x V _{FB}		
THERMAL S	HUTDOWN					
-	The award also states and the sale	Shutdown temperature		160		°C
T _{SDN}	Thermal shutdown threshold	Hysteresis		15		°C
T	VREG5 thermal shutdown threshold	Shutdown temperature		171		°C
T _{SDN VREG5}		Hysteresis		18		°C
UVLO			'			
		VREG5 rising voltage	4.1	4.3	4.5	V
UVLO	UVLO threshold	VREG5 falling voltage	3.34	3.57	3.8	V
		VREG5 hysteresis		730		mV

6.6 Timing Requirements

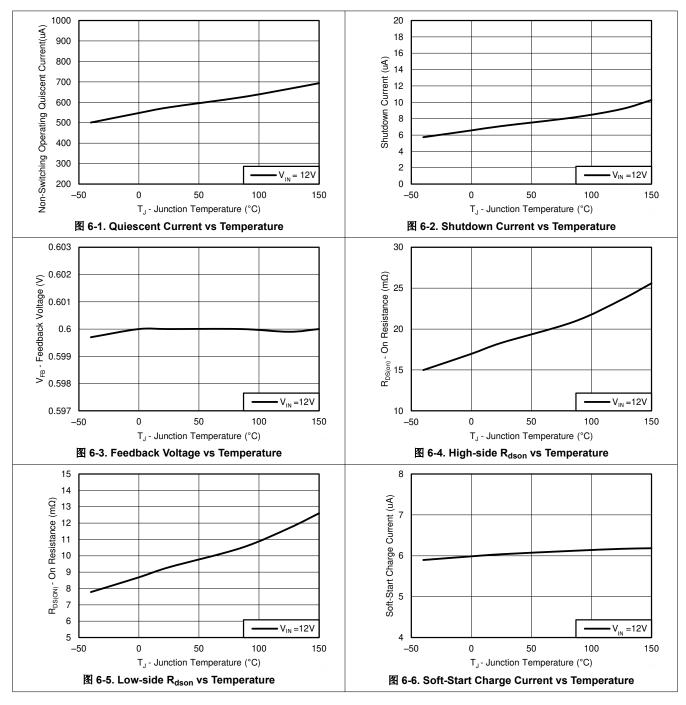
	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
ON-TIME	TIMER CONTROL				'	
t _{ON}	SW On Time	V _{IN} = 12 V, V _{OUT} =3.3 V, F _{SW} = 800 kHz	310	340	380	ns
t _{ON min}	SW Minimum on time	V _{IN} = 17 V, V _{OUT} =0.6 V, F _{SW} = 1200 kHz		54		ns
t _{OFF}	SW Minimum off time	25°C, V _{FB} =0.5 V			310	ns
SOFT ST	ART					
t _{SS}	Soft start time	Internal soft start time		1.045		ms
OUTPUT	UNDERVOLTAGE AND OVERVOLTAGE F	PROTECTION			'	
t _{UVPDEL}	Output Hiccup delay relative to SS time	UVP detect		1		cycle
t _{UVPEN}	Output Hiccup enable delay relative to SS time	UVP detect		7		cycle

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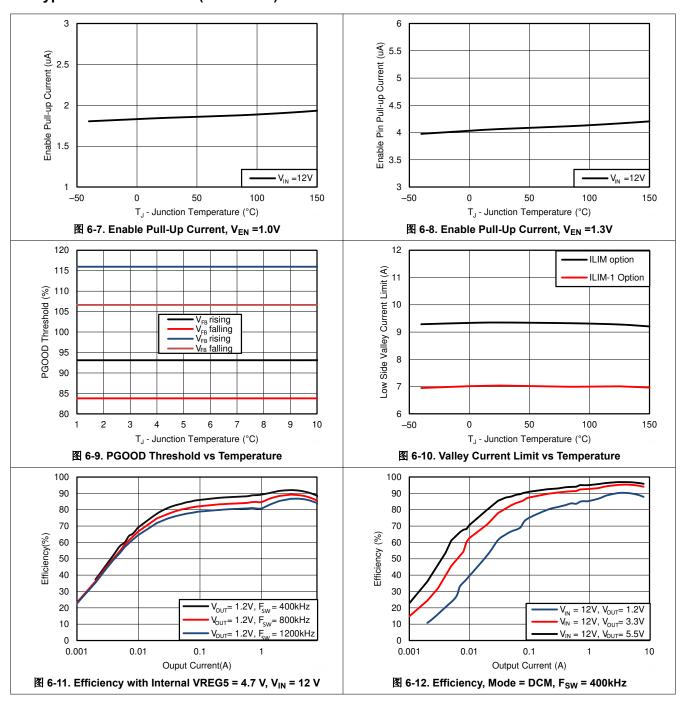


6.7 Typical Characteristics



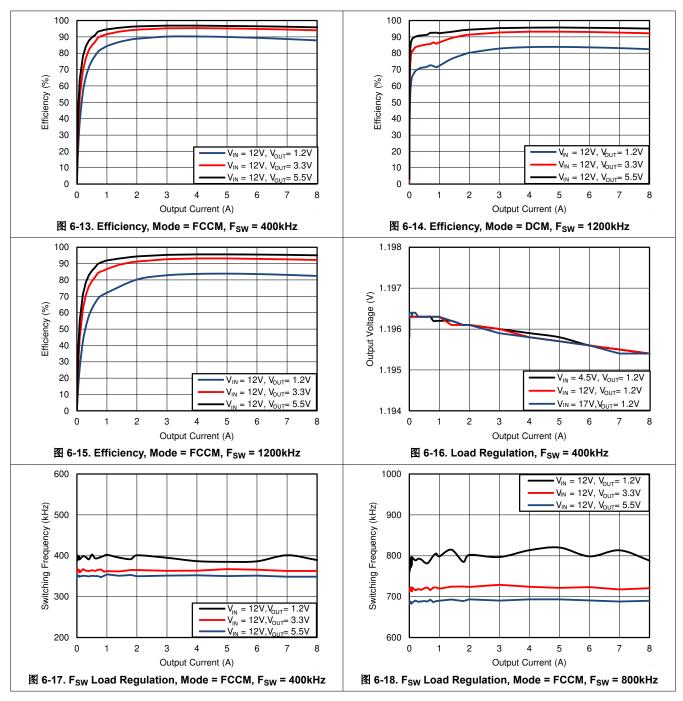


6.7 Typical Characteristics (continued)



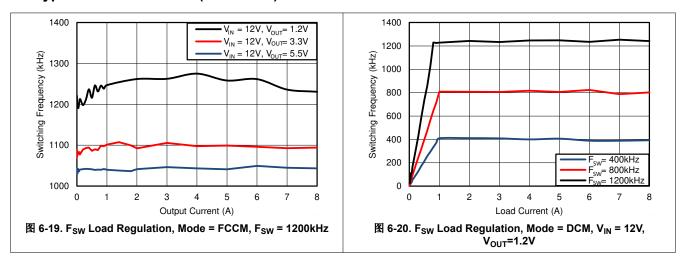


6.7 Typical Characteristics (continued)





6.7 Typical Characteristics (continued)



7 Detailed Description

7.1 Overview

The TPS568215 is a high-density, synchronous, step-down buck converter which can operate from 4.5-V to 17-V input voltage (V_{IN}). The device has 19-m Ω and 9-m Ω integrated MOSFETs that enable high efficiency up to 8 A. The device employs D-CAP3 $^{\text{TM}}$ control mode that provides fast transient response with no external compensation components and an accurate feedback voltage. The control topology provides seamless transition between FCCM operating mode at higher load condition and DCM/Eco-mode $^{\text{TM}}$ operation at lighter load condition. DCM/Eco-mode $^{\text{TM}}$ allows the TPS568215 to maintain high efficiency at light load. The TPS568215 is able to adapt to both low equivalent series resistance (ESR) output capacitors such as POSCAP or SP-CAP, and ultra-low ESR ceramic capacitors.

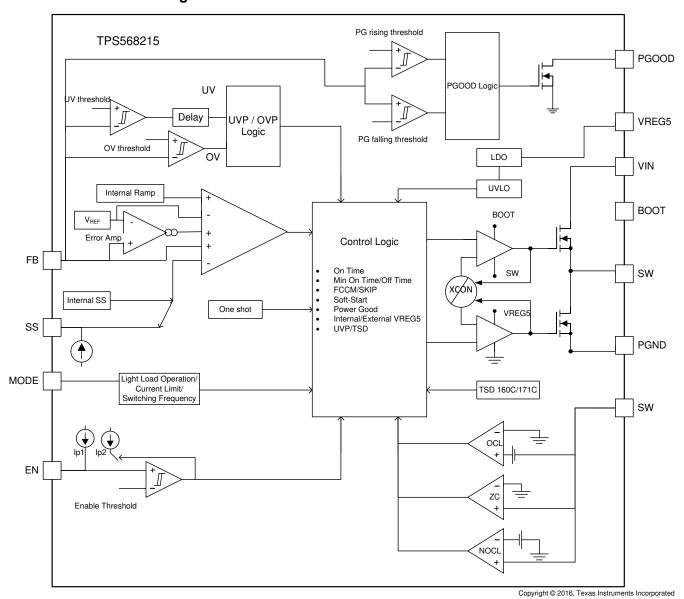
The TPS568215 has three selectable switching frequencies (F_{SW}) 400 kHz, 800 kHz, and 1200 kHz which gives the flexibility to optimize the design for higher efficiency or smaller size. There are two selectable current limits. All these options are configured by choosing the right voltage on the MODE pin.

The TPS568215 has a 4.7-V internal LDO that creates bias for all internal circuitry. There is a feature to overdrive this internal LDO with an external voltage on the VREG5 pin which improves the converter efficiency. The undervoltage lockout (UVLO) circuit monitors the VREG5 pin voltage to protect the internal circuitry from low input voltages. The device has an internal pullup current source on the EN pin which can enable the device even with the pin floating.

Soft-start time can be selected by connecting a capacitor to the SS pin. The device is protected from output short, undervoltage, and overtemperature conditions.



7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 PWM Operation and D-CAP3™ Control Mode

The TPS568215 operates using the adaptive on-time PWM control with a proprietary D-CAP3 control mode which enables low external component count with a fast load transient response while maintaining a good output voltage accuracy. At the beginning of each switching cycle the high side MOSFET is turned on for an on-time set by an internal one shot timer. This on-time is set based on the converter's input voltage, output voltage and the pseudo-fixed frequency hence this type of control topology is called an adaptive on-time control. The one shot timer resets and turns on again after the feedback voltage (V_{FB}) falls below the internal reference voltage (V_{REF}). An internal ramp is generated which is fed to the FB pin to simulate the output voltage ripple. This enables the use of very low-ESR output capacitors such as multi-layered ceramic caps (MLCC). No external current sense network or loop compensation is required for DCAP3TM control topology.

The TPS568215 includes an error amplifier that makes the output voltage very accurate. This error amplifier is absent in other flavors of D-CAP3 control mode. For any control topology that is compensated internally, there is a range of the output filter it can support. The output filter used with the TPS568215 is a low pass L-C circuit. This L-C filter has double pole that is described in

$$f_{P} = \frac{1}{2 \times \pi \times \sqrt{L_{OUT} \times C_{OUT}}}$$
(1)

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the TPS568215. The low frequency L-C double pole has a 180 degree in phase. At the output filter frequency, the gain rolls off at a -40dB per decade rate and the phase drops rapidly. The internal ripple generation network introduces a high-frequency zero that reduces the gain roll off from -40dB to -20dB per decade and increases the phase to 90 degree one decade above the zero frequency. The internal ripple injection high frequency zero is changed according to the switching frequency selected as shown in table below. The inductor and capacitor selected for the output filter must be such that the double pole is located close enough to the high-frequency zero so that the phase boost provided by this high-frequency zero provides adequate phase margin for the stability requirement. The crossover frequency of the overall system must usually be targeted to be less than one-fifth of the switching frequency (F_{SW}).

表 7-1. Ripple Injection Zero

Switching Frequency (kHz)	Zero Location (kHz)
400	7.1
800	14.3
1200	21.4

 $ilde{ ilde{\pi}}$ 7-2 lists the inductor values and part numbers that are used to plot the efficiency curves in the $ilde{\pi}$ 6.7 section.

表 7-2. Inductor Values

V _{OUT} (V)	F _{SW} (kHz)	L _{OUT} (uH)	Würth Part Number ⁽¹⁾
	400	1.2	744325120
1.2	800	0.68	744311068
	1200	0.47	744314047
	400	2.4	744325240
3.3	800	1.5	744314150
	1200	1.1	744314110

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V _{OUT} (V)	F _{SW} (kHz)	L _{OUT} (uH)	Würth Part Number ⁽¹⁾
	400	3.3	744325330
5.5	800	2.4	744325240
	1200	1.2	744325120

(1) See Third-Party Products disclaimer

7.3.2 Eco-mode™ Control

The TPS568215 is designed with Eco-mode™ control to increase efficiency at light loads. This option can be chosen using the MODE pin as shown in table 3. As the output current decreases from heavy load condition, the inductor current is also reduced. If the output current is reduced enough, the valley of the inductor current reaches the zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The low-side MOSFET is turned off when a zero inductor current is detected. As the load current further decreases the converter runs into discontinuous conduction mode. The on-time is kept approximately the same as it is in continuous conduction mode. The off-time increases as it takes more time to discharge the output with a smaller load current. The light load current where the transition to Eco-mode™ operation happens (I_{OUT(LL)}) can be calculated from \hbar ₹式 2.

$$I_{OUT(LL)} = \frac{1}{2 \times L_{OUT} \times F_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}}$$
(2)

After identifying the application requirements, design the output inductance so that the inductor peak-to-peak ripple current is approximately between 20% and 30% of the $I_{CC(max)}$ (peak current in the application). it is also important to size the inductor properly so that the valley current doesn't hit the negative low side current limit.

7.3.3 4.7 V LDO and External Bias

The VREG5 pin is the output of the internal 4.7-V linear regulator that creates the bias for all the internal circuitry and MOSFET gate drivers. The VREG5 pin needs to be bypassed with a 4.7-µF capacitor. An external voltage that is above the LDO's internal output voltage can override the internal LDO, switching it to the external rail after a higher voltage is detected. This enhances the efficiency of the converter because the quiescent current now runs off this external rail instead of the input power supply. The UVLO circuit monitors the VREG5 pin voltage and disables the output when VREG5 falls below the UVLO threshold. When using an external bias on the VREG5 rail, any power-up and power-down sequencing can be applied but it is important to understand that if there is a discharge path on the VREG5 rail that can pull a current higher than the internal LDO's current limit (ILIM5) from the VREG5, then the VREG5 LDO turns off thereby shutting down the output of TPS568215. If such condition does not exist and if the external VREG5 rail is turned off, the VREG5 voltage switches over to the internal LDO voltage which is 4.7 V typically in a few nanoseconds. Figure 26 below shows this transition of the VREG5 voltage from an external bias of 5.5 V to the internal LDO output of 4.7 V when the external bias to VREG5 is disabled while the output of TPS568215 remains unchanged.

7.3.4 MODE Selection

TPS568215 has a MODE pin that can offer 12 different states of operation as a combination of Current Limit, Switching Frequency and Light Load operation. The device can operate at two different current limits ILIM-1 and ILIM to support an output continuous current of 6 A, 8 A respectively. The TPS568215 is designed to compare the valley current of the inductor against the current limit thresholds so understand that the output current is half the ripple current above the valley current. TPS568215 can operate at three different frequencies of 400 kHz, 800 kHz and 1200 kHz and also can choose between Eco-mode $^{\text{TM}}$ and FCCM mode. The device reads the voltage on the MODE pin during start-up and latches onto one of the MODE options listed below in table 3. The voltage on the MODE pin can be set by connecting this pin to the center tap of a resistor divider connected between VREG5 and AGND. A guideline for the top resistor (R_{M_H}) and the bottom resistor (R_{M_L}) as 5% resistors is shown in Table 3. It is important that the voltage for the MODE pin is derived from the VREG5 rail

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only must internally this voltage is referenced to detect the MODE option. The MODE pin setting can be reset only by a VIN power cycling.

表 7-3. Mode Pin Resistor Settings										
$R_{M_L}(k\Omega)$	R _{M_H} (kΩ)	Light Load Operation	Current Limit	Frequency (kHz)						
5.1	300	FCCM	ILIM-1	400						
10	200	FCCM	ILIM	400						
20	160	FCCM	ILIM-1	800						
20	120	FCCM	ILIM	800						
51	200	FCCM	ILIM-1	1200						
51	180	FCCM	ILIM	1200						
51	150	DCM	ILIM-1	400						
51	120	DCM	ILIM	400						
51	91	DCM	ILIM-1	800						
51	82	DCM	ILIM	800						
51	62	DCM	ILIM-1	1200						
51	51	DCM	ILIM	1200						

🗵 7-1 below shows the typical start-up sequence of the device after the enable signal crosses the EN turn-on threshold. After the voltage on VREG5 crosses the rising UVLO threshold it takes about 500 us to read the first mode setting and approximately 100 us from there to finish the last mode setting. The output voltage starts ramping after the mode reading is done.

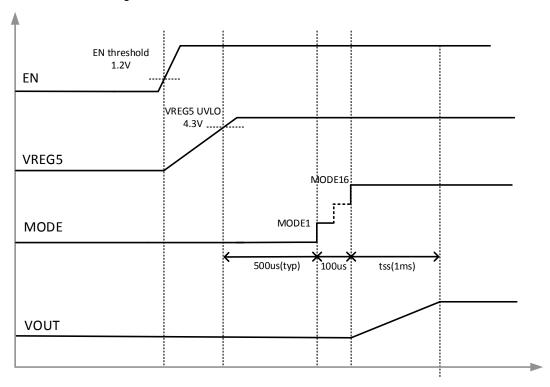


图 7-1. Power-Up Sequence

7.3.5 Soft Start and Pre-biased Soft Start

The TPS568215 has an adjustable soft-start time that can be set by connecting a capacitor on SS pin. When the EN pin becomes high, the soft-start charge current (I_{SS}) begins charging the external capacitor (C_{SS}) connected between SS and AGND. The devices tracks the lower of the internal soft-start voltage or the external soft-start voltage as the reference. The equation for the soft-start time (T_{SS}) is shown in 方程式 3:

$$T_{SS(S)} = \frac{C_{SS} \times V_{REF}}{I_{SS}}$$
(3)

where

V_{RFF} is 0.6 V and I_{SS} is 6 μA

If the output capacitor is pre-biased at startup, the device initiates switching and starts ramping up only after the internal reference voltage becomes greater than the feedback voltage V_{FB} . This scheme ensures that the converters ramp up smoothly into regulation point.

7.3.6 Enable and Adjustable UVLO

The EN pin controls the turn-on and turn-off of the device. When EN pin voltage is above the turn-on threshold which is around 1.2 V, the device starts switching and when the EN pin voltage falls below the turn-off threshold which is around 1.1V it stops switching. If the user application requires a different turn-on (V_{START}) and turn-off thresholds (V_{STOP}) respectively, the EN pin can be configured as shown in $\[mathbb{R}\]$ 7-2 by connecting a resistor divider between VIN and EN. The EN pin has a pull-up current I_{p1} that sets the default state of the pin when it is floating. This current increases to I_{p2} when the EN pin voltage crosses the turn-on threshold. The UVLO thresholds can be set by using $\[mathbb{T}\]$ 4 and $\[mathbb{T}\]$ 7-2 by connecting a resistor divider between VIN and EN. The EN pin has a pull-up current I_{p1} that sets the default state of the pin when it is floating.

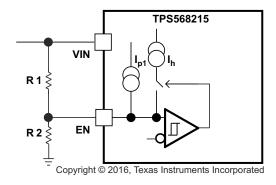


图 7-2. Adjustable VIN Under Voltage Lock Out

$$R1 = \frac{V_{START} \left(\frac{V_{ENFALLING}}{V_{ENRISING}} \right) - V_{STOP}}{I_{p1} \left(1 - \frac{V_{ENFALLING}}{V_{ENRISING}} \right) + I_{h}}$$
(4)

$$R2 = \frac{R1 \times V_{ENFALLING}}{V_{STOP} - V_{ENFALLING} + R1 I_{p2}}$$
(5)

where

- $I_{p2} = 4.197 \mu A$
- I_{p1} = 1.91 μA
- $I_h = 2.287 \mu A$
- V_{ENRISING} = 1.225 V
- V_{ENFALLING} = 1.104 V

7.3.7 Power Good

The Power-Good (PGOOD) pin is an open drain output. After the FB pin voltage is between 93% and 107% of the internal reference voltage (V_{REF}) the PGOOD is de-asserted and floats after a 200 $\,\mu$ s de-glitch time. TI recommends a pullup resistor of 10 k $\,\Omega$ to pull it up to VREG5. The PGOOD pin is pulled low when the FB pin voltage is lower than V_{UVP} or greater than V_{OVP} threshold; or, in an event of thermal shutdown or during the soft-start period.

7.3.8 Overcurrent Protection and Undervoltage Protection

The output overcurrent limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. During the on time of the high-side FET switch, the switch current increases at a linear rate determined by input voltage , output voltage, the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current I_{OUT} . If the measured drain to source voltage of the low-side FET is above the voltage proportional to current limit, the low side FET stays on until the current level becomes lower than the OCL level which reduces the output current available. When the current is limited the output voltage tends to drop because the load demand is higher than what the converter can support. When the output voltage falls below 68% of the target voltage, the UVP comparator detects it and shuts down the device after a wait time of 1ms, the device restarts after a hiccup time of 7ms. In this type of valley detect control the load current is higher than the OCL threshold by one half of the peak to peak inductor ripple current. When the overcurrent condition is removed, the output voltage returns to the regulated value. If an OCL condition happens during start-up then the device enters hiccup-mode immediately without a wait time of 1 ms.

7.3.9 Out-of-Bounds Operation

The device has an out-of-bounds (OOB) overvoltage protection that protects the output load at a much lower overvoltage threshold of 8% above the target voltage. OOB protection does not trigger an overvoltage fault, OOB protection operates as an early no-fault overvoltage protection mechanism. During the OOB operation, the controller operates in forced PWM mode only by turning on the low-side FET. Turning on the low-side FET beyond the zero inductor current quickly discharges the output capacitor thus causing the output voltage to fall quickly toward the setpoint. During the operation, the cycle-by cycle negative current limit is also activated to ensure the safe operation of the internal FETs.

7.3.10 UVLO Protection

Under voltage lock out protection (UVLO) monitors the internal VREG5 regulator voltage. When the VREG5 voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

7.3.11 Thermal Shutdown

The device monitors the internal die temperature. If this temperature exceeds the thermal shutdown threshold value (T_{SDN} typically 160°C) the device shuts off. This is a non-latch protection. During start up, if the device temperature is higher than 160°C the device does not start switching and does not load the MODE settings. If the device temp goes higher than T_{SDN} threshold after startup, it stops switching with SS reset to ground and an internal discharge switch turns on to quickly discharge the output voltage. The device re-starts switching when the temperature goes below the thermal shutdown threshold but the MODE settings are not re-loaded again. There is a second higher thermal protection on the device T_{SDN} VREG5 which protects it from over temperature conditions not caused by the switching of the device itself. This threshold is at typically 170°C. Even under nonswitching condition of the device after exceeding T_{SDN} threshold, if it still continues to heat up the VREG5 output shuts off after temperature goes beyond T_{SDN} VREG5, thereby shutting down the device completely.

7.3.12 Output Voltage Discharge

The device has a 500ohm discharge switch that discharges the output V_{OUT} through SW node during any event of fault like output overvoltage, output undervoltage , TSD , if VREG5 voltage below the UVLO and when the EN pin voltage (V_{EN}) is below the turn-on threshold.



7.4 Device Functional Modes

7.4.1 Light Load Operation

When the MODE pin is selected to operate in FCCM mode, the converter operates in continuous conduction mode (FCCM) during light-load conditions. During FCCM, the switching frequency (F_{SW}) is maintained at an almost constant level over the entire load range which is suitable for applications requiring tight control of the switching frequency and output voltage ripple at the cost of lower efficiency under light load. If the MODE pin is selected to operate in DCM/Eco-mode TM , the device enters pulse skip mode after the valley of the inductor ripple current crosses zero. The Eco-mode TM maintains higher efficiency at light load with a lower switching frequency.

7.4.2 Standby Operation

The TPS568215 can be placed in standby mode by pulling the EN pin low. The device operates with a shutdown current of 7uA when in standby condition.

Product Folder Links: TPS568215

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8 Application and Implementation

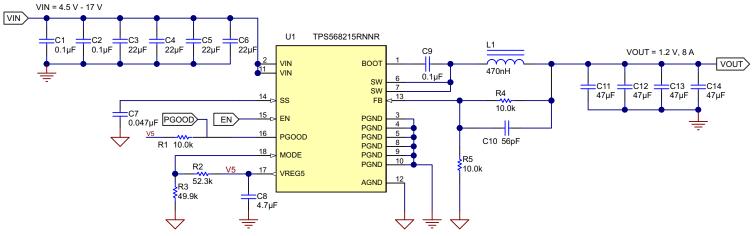
备注

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8.1 Application Information

The schematic of 88-1 shows a typical application for TPS568215. This design converts an input voltage range of 4.5 V to 17 V down to 1.2 V with a maximum output current of 8 A.

8.2 Typical Application



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图 8-1. Application Schematic

8.2.1 Design Requirements

表 8-1. Design Parameters

	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
V _{OUT}	Output voltage			1.2		V
I _{OUT}	Output current			8		Α
ΔV _{OUT}	Transient response	4-A load step		±30		mV
V _{IN}	Input voltage		4.5	12	17	V
V _{OUT(ripple)}	Output voltage ripple			<10		mV _(P-P)
	Start input voltage	Input voltage rising		Internal UVLO		V
	Stop input voltage	Input voltage falling		Internal UVLO		V
f _{SW}	Switching frequency			1.2		MHz
Operating Mode				DCM		
T _A	Ambient temperature			25		°C

8.2.2 Detailed Design Procedure

8.2.2.1 External Component Selection

8.2.2.1.1 Output Voltage Set Point

To change the output voltage of the application, it is necessary to change the value of the upper feedback resistor. By changing this resistor the user can change the output voltage above 0.6 V. See 方程式 6

$$V_{OUT} = 0.6 \times \left(1 + \frac{R_{UPPER}}{R_{LOWER}}\right)$$
 (6)

8.2.2.1.2 Switching Frequency and Mode Selection

Switching Frequency, current limit and switching mode (DCM or FCCM) are set by a voltage divider from VREG5 to GND connected to the MODE pin. See $\frac{1}{8}$ 7-3 for possible MODE pin configurations. Switching frequency selection is a tradeoff between higher efficiency and smaller system solution size. Lower switching frequency yields higher overall efficiency but relatively bigger external components. Higher switching frequencies cause additional switching losses which impact efficiency and thermal performance. For this design 1.2 MHz is chosen as the switching frequency, the switching mode is DCM and the output current is 8 A.

8.2.2.1.3 Inductor Selection

The inductor ripple current is filtered by the output capacitor. A higher inductor ripple current means the output capacitor must have a ripple current rating higher than the inductor ripple current. See 表 8-2 for recommended inductor values.

The RMS and peak currents through the inductor can be calculated using 方程式 7 and 方程式 8. It is important that the inductor is rated to handle these currents.

$$I_{L(rms)} = \sqrt{\left(I_{OUT}^2 + \frac{1}{12} \times \left(\frac{V_{OUT} \times \left(V_{IN(max)} - V_{OUT}\right)}{V_{IN(max)} \times L_{OUT} \times F_{SW}}\right)^2}\right)}$$
(7)

$$I_{L(peak)} = I_{OUT} + \frac{I_{OUT(ripple)}}{2}$$
 (8)

During transient/short circuit conditions the inductor current can increase up to the current limit of the device so it is safe to choose an inductor with a saturation current higher than the peak current under current limit condition.

8.2.2.1.4 Output Capacitor Selection

After selecting the inductor the output capacitor needs to be optimized. In D-CAP3 control mode, the regulator reacts within one cycle to the change in the duty cycle so the good transient performance can be achieved without needing large amounts of output capacitance. The recommended output capacitance range is given in $\frac{1}{8}$ 8-2

Ceramic capacitors have very low ESR, otherwise the maximum ESR of the capacitor must be less than $V_{OUT(ripple)}/I_{OUT(ripple)}$

表 8-2. Recommended Component Values

R _{LOWER} (kΩ)	R _{UPPER} (kΩ)	F _{SW} (kHz)	L _{OUT} (µH)	C _{OUT(min)} (μF)	C _{OUT(max)} (μF)	C _{FF} (pF)
		400	0.68	300	500	-
10	0	800	0.47	100	500	-
		1200	0.33	88	500	-
		400	1.2	100	500	-
	10	800	0.68	88	500	-
		1200	0.47	88	500	-
		10 0	10 0 800 1200 400 10 800	10 0 400 0.68 800 0.47 1200 0.33 400 1.2 10 800 0.68	10 0 800 0.47 1200 0.33 88 400 1.2 10 800 800 0.68 88	10 0 800 0.47 1200 0.33 400 1.2 10 500 400 1.2 10 800 0 88 500 10 800 0.68 88 500

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表 8-2. Recommended Component Values (continued)

_											
	V _{OUT} (V)	R_{LOWER} (k Ω)	R _{UPPER} (kΩ)	F _{SW} (kHz)	L _{OUT} (µH)	C _{OUT(min)} (μF)	C _{OUT(max)} (µF)	C _{FF} (pF)			
				400	2.4	88	500	100 - 220			
	3.3		45.3	800	1.5	88	500	100 - 220			
				1200	1.1	88	500	100 - 220			
				400	3.3	88	500	100 - 220			
	5.5		82.5	800	2.4	88	500	100 - 220			
				1200	1.2	88	700	100 - 220			

8.2.2.1.5 Input Capacitor Selection

The minimum input capacitance required is given in 方程式 9.

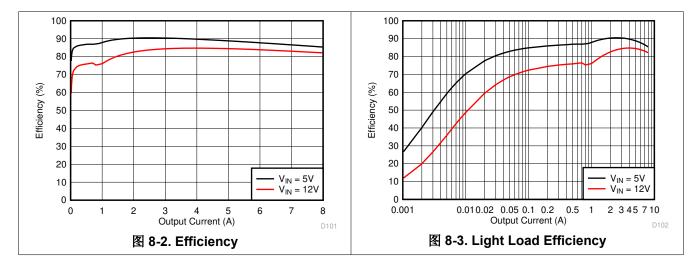
$$C_{IN(min)} = \frac{I_{OUT} \times V_{OUT}}{V_{INripple} \times V_{IN} \times F_{SW}}$$
(9)

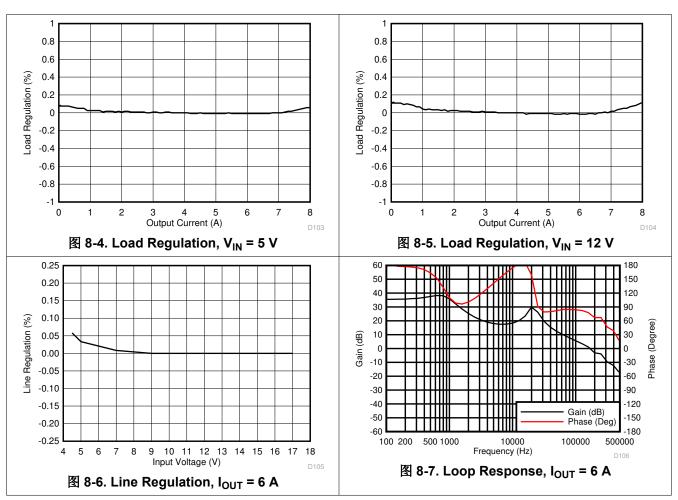
$$I_{CIN(ms)} = I_{OUT} \times \sqrt{\frac{V_{OUT}}{V_{IN(min)}}} \times \frac{(V_{IN(min)} - V_{OUT})}{V_{IN(min)}}$$
(10)

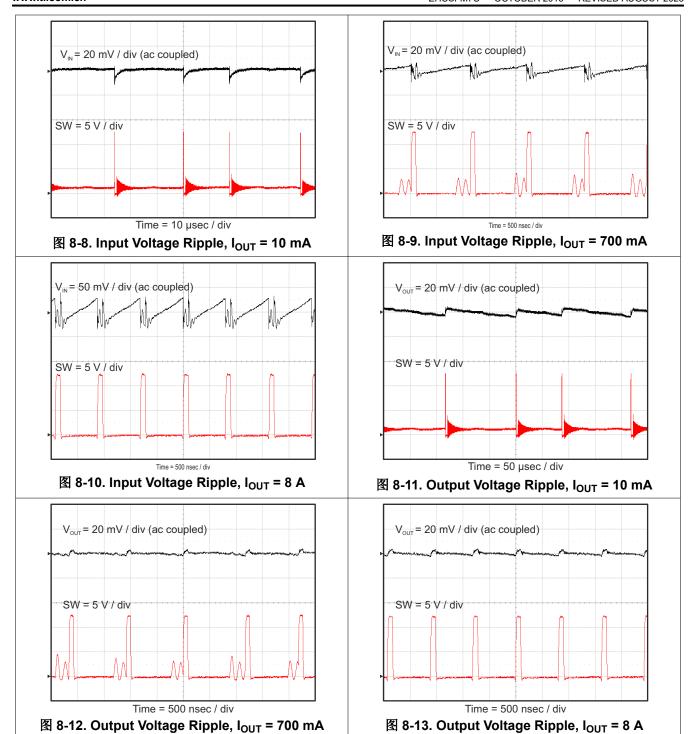


8.2.3 Application Curves

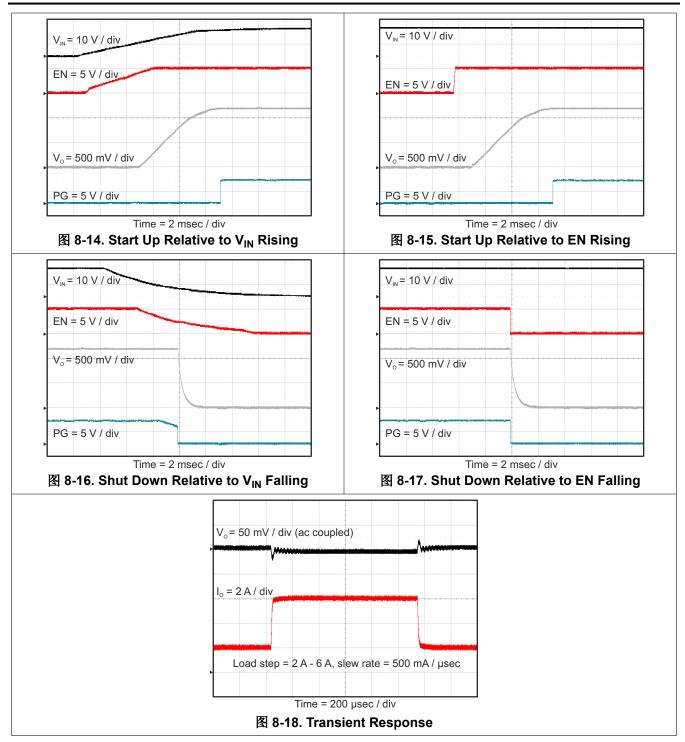
图 8-2 through 图 8-18 apply to the circuit of 图 8-1. V_{IN} = 12 V. T_a = 25 °C unless otherwise specified.











8.3 Power Supply Recommendations

The TPS568215 is intended to be powered by a well regulated dc voltage. The input voltage range is 4.5 to 17 V. TPS568215 is a buck converter. The input supply voltage must be greater than the desired output voltage for proper operation. Input supply current must be appropriate for the desired output current. If the input voltage supply is located far from the TPS568215 circuit, TI recommends some additional input bulk capacitance. Typical values are $100~\mu\text{F}$ to $470~\mu\text{F}$.

Product Folder Links: TPS568215

8.4 Layout

8.4.1 Layout Guidelines

- Recommend a four-layer or six-layer PCB for good thermal performance and with maximum ground plane. 3" × 3", four-layer PCB with 2-oz. copper used as example.
- Recommend having equal caps on each side of the IC. Place them right across VIN as close as possible.
- Inner layer 1 is ground with the PGND to AGND net tie.
- Inner layer 2 has VIN copper pour that has vias to the top layer VIN. Place multiple vias under the device near VIN and GND and near input capacitors to reduce parasitic inductance and improve thermal performance
- · Bottom later is GND with the BOOT trace routing.
- Reference feedback to the quite AGND and routed away from the switch node.
- Make VIN trace wide to reduce the trace impedance.

8.4.2 Layout Example

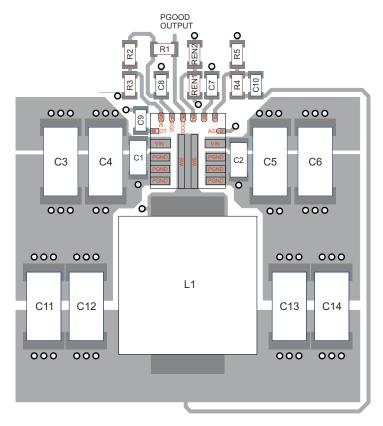


图 8-19. Top Side Layout



8-20 shows the recommended layout for the first internal layer. It is comprised of a large PGND plane and a smaller ANGD island. AGND and PGND are connected at a single point to reduce circulating currents.

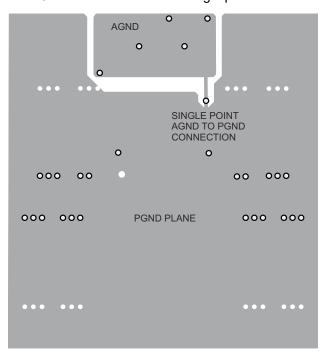


图 8-20. Mid Layer 1 Layout

8-21 shows the recommended layout for the second internal layer. It is comprised of a large PGND plane, a smaller copper fill area to connect the two top side V_{IN} copper areas and a second V_{OUT} copper fill area.

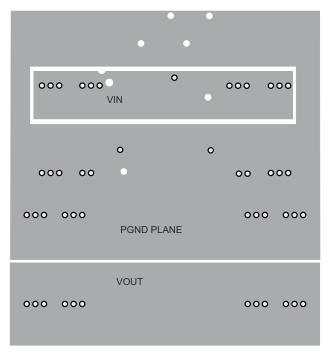


图 8-21. Mid Layer 2 Layout

8-22 shows the recommended layout for the bottom layer. It is comprised of a large PGND plane and a trace to connect the BOOT capacitor to the SW node.

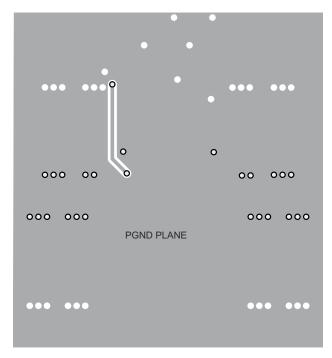


图 8-22. Bottom Layer Layout

9 Device and Documentation Support

9.1 Device Support

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9.1.2 Development Support

TPS568215EVM-762 8-A, SWIFT™ Regulator Evaluation Module User's Guide

9.2 接收文档更新通知

要接收文档更新通知,请导航至 ti.com 上的器件产品文件夹。点击*订阅更新* 进行注册,即可每周接收产品信息更改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

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9.6 术语表

TI术语表本术语表列出并解释了术语、首字母缩略词和定义。

10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

Product Folder Links: TPS568215

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PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead finish/ Ball material	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
TPS568215RNNR	ACTIVE	VQFN-HR	RNN	18	3000	RoHS & Green	Call TI NIPDAU	Level-2-260C-1 YEAR	-40 to 125	568215	Samples
TPS568215RNNT	ACTIVE	VQFN-HR	RNN	18	250	RoHS & Green	Call TI NIPDAU	Level-2-260C-1 YEAR	-40 to 125	568215	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

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- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead finish/Ball material Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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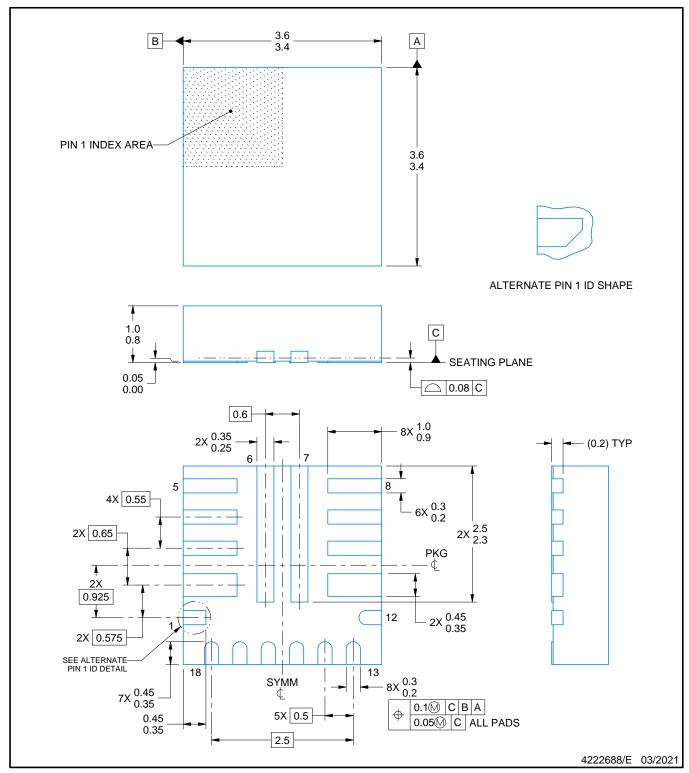


PACKAGE OPTION ADDENDUM

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PLASTIC QUAD FLATPACK - NO LEAD

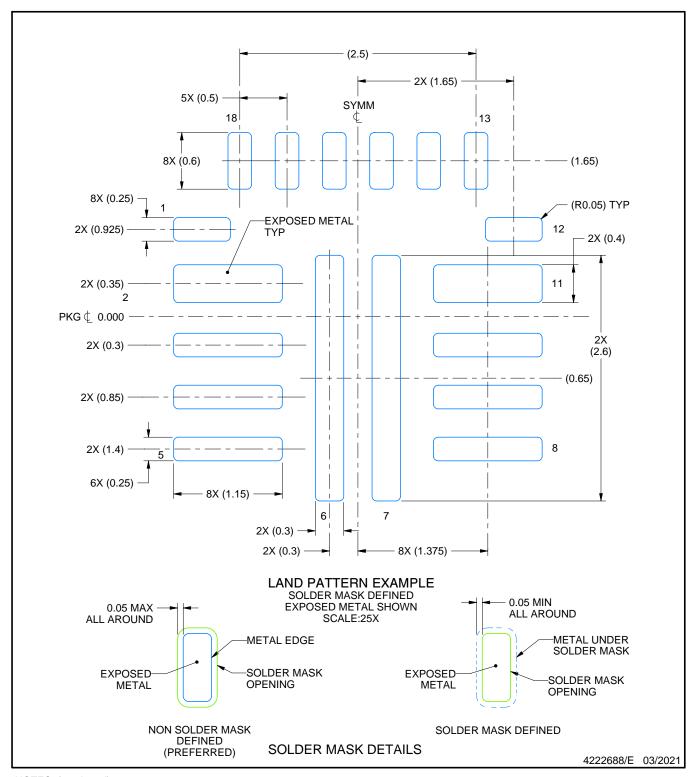


NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
 2. This drawing is subject to change without notice.



PLASTIC QUAD FLATPACK - NO LEAD

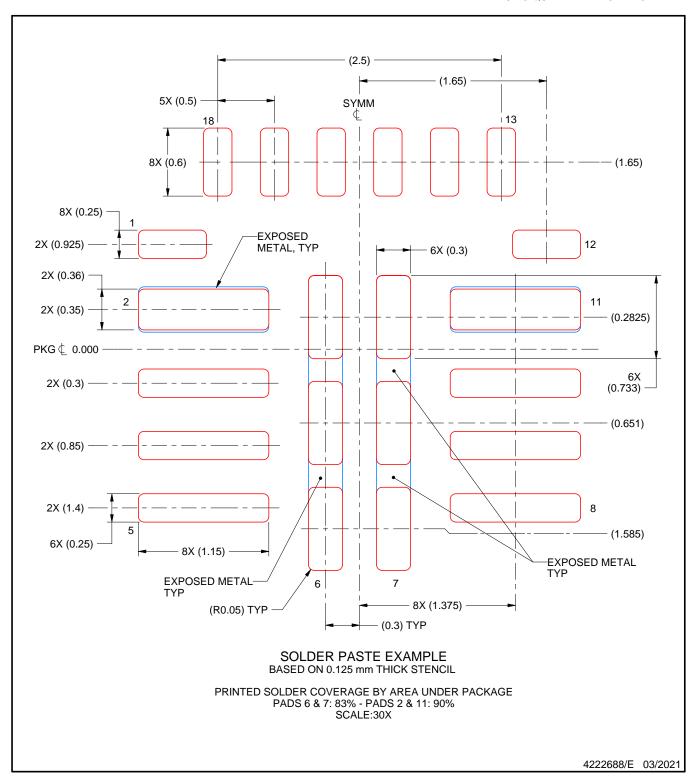


NOTES: (continued)

- 3. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
- 4. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



PLASTIC QUAD FLATPACK - NO LEAD



NOTES: (continued)

5. For alternate stencil design recommendations, see IPC-7525 or board assembly site preference.



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