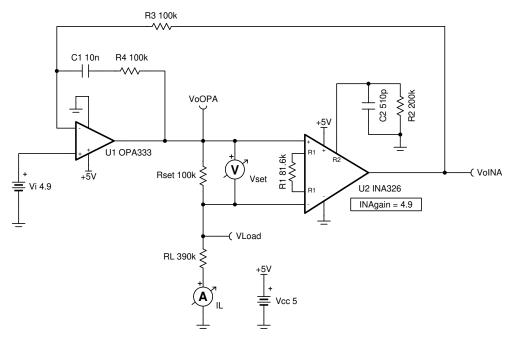


### **Design Goals**

Input		Output		Supply		Load Resistance (R <sub>L</sub> )	
V <sub>iMin</sub>	V <sub>iMax</sub>	I <sub>LMin</sub>	I <sub>LMax</sub>	V <sub>cc</sub>	V <sub>ee</sub>	R <sub>LMin</sub>	R <sub>LMax</sub>
0.49 V	4.9 V	1 µA	10 µA	5 V	0 V	0 Ω	390 kΩ

### **Design Description**

This circuit delivers a precise low-level current,  $I_L$ , to a load,  $R_L$ . The design operates on a single 5 V supply and uses one precision low-drift op amp and one instrumentation amplifier. Simple modifications can change the range and accuracy of the voltage-to-current (V-I) converter.



#### **Design Notes**

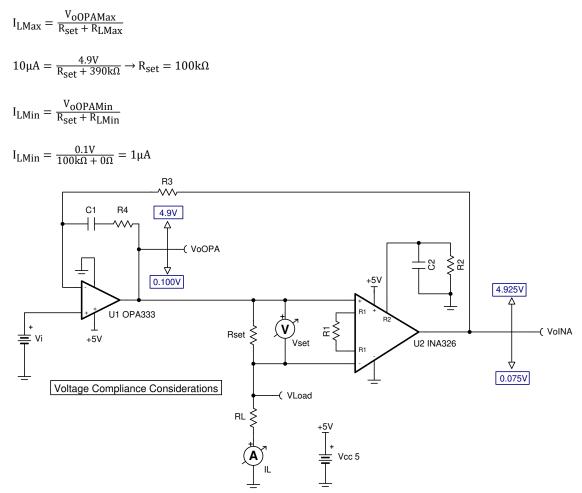
- Voltage compliance is dominated by op amp linear output swing (see data sheet A<sub>OL</sub> test conditions) and instrumentation amplifier linear output swing. See the *Common-Mode Input Range Calculator for Instrumentation Amplifiers* for more information.
- 2. Voltage compliance, along with  $R_{LMin}$ ,  $R_{LMax}$ , and  $R_{set}$  bound the I<sub>L</sub> range.
- 3. Check op amp and instrumentation amplifier input common-mode voltage range.
- 4. Stability analysis must be done to choose R<sub>4</sub> and C<sub>1</sub> for stable operation.
- 5. Loop stability analysis to select R<sub>4</sub> and C<sub>1</sub> will be different for each design. The compensation shown is only valid for the resistive load ranges used in this design. Other types of loads, op amps, or instrumentation amplifiers, or both will require different compensation. See the **Design References** section for more op amp stability resources.

1



## **Design Steps**

1. Select R<sub>set</sub> and check I<sub>LMin</sub> based on voltage compliance.



2. Compute instrumentation amplifier gain, G.

 $V_{setMin} = I_{LMin} \times R_{set} = 1 \mu A \times 100 k \Omega = 0.1 V$ 

 $V_{setMax} = I_{LMax} \times R_{set} = 10 \mu A \times 100 k\Omega = 1V$ 

$$G = \frac{V_{iMax} - V_{iMin}}{V_{setMax} - V_{setMin}}$$
$$G = \frac{4.9V - 0.49V}{1V - 0.1V} = 4.9$$

3. Choose R<sub>1</sub> for INA326 instrumentation amplifier gain, G. Use data sheet recommended R<sub>2</sub> = 200 k $\Omega$  and C<sub>2</sub> = 510 pF.

$$G = 2 \times \left(\frac{R_2}{R_1}\right)$$
$$R_1 = \frac{2 \times R_2}{G}$$
$$R_1 = \left(\frac{2 \times 200 k\Omega}{4.9}\right) = 81.6327 k\Omega \approx 81.6 k\Omega$$

4. The final transfer function of the circuit follows:

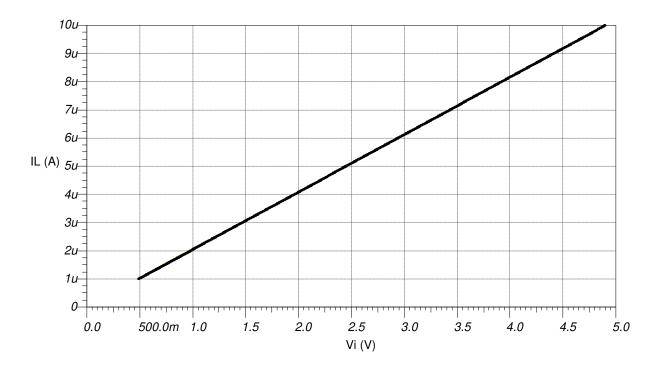
$$\begin{split} I_L &= \frac{V_i}{G \times R_{set}} \\ I_L &= \frac{V_i}{4.9 \times 100 \text{k}\Omega} = \frac{V_i}{490 \text{k}\Omega} \\ V_i &= 0.49 \text{V} \rightarrow I_L = 1 \mu \text{A} \\ V_i &= 4.9 \text{V} \rightarrow I_L = 10 \mu \text{A} \end{split}$$



# **Design Simulations**

## **DC Simulation Results**

Vi	RL	١L	V <sub>oOPA</sub>	V <sub>oOPA</sub> Compliance	V <sub>oINA</sub>	V <sub>oINA</sub> Compliance
0.49 V	0 Ω	0.999627 µA	99.982723 mV	100 mV to 4.9 V	490.013346 mV	75 mV to 4.925 V
0.49 V	390 kΩ	0.999627 µA	489.837228 mV	100 mV to 4.9 V	490.013233 mV	75 mV to 4.925 V
4.9 V	0 Ω	9.996034 µA	999.623352 mV	100 mV to 4.9 V	4.900016 V	75 mV to 4.925 V
4.9 V	390 kΩ	9.996031 µA	4.898075 V	100 mV to 4.9 V	4.900015 V	75 mV to 4.925 V



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# **Design References**

See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.

See the TINA-TI<sup>™</sup> circuit simulation file, SBOMAT8.

See TIPD107.

See Solving Op Amp Stability Issues - E2E FAQ.

See TI Precision Labs - Op Amps.

### **Design Featured Op Amp**

OPA333			
V <sub>ss</sub>	1.8 V to 5.5 V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>out</sub>	Rail-to-rail		
V <sub>os</sub>	2 μV		
Ι <sub>q</sub>	17 µA/Ch		
l <sub>b</sub>	70 pA		
UGBW	350 kHz		
SR	0.16 V/µs		
#Channels	1 and 2		
OPA333			

#### **Design Featured Instrumentation Amplifier**

INA326			
V <sub>ss</sub>	2.7 V to 5.5 V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>out</sub>	Rail-to-rail		
V <sub>os</sub>	20 µV		
۱ <sub>q</sub>	2.4 mA		
ا <sub>b</sub>	0.2 nA		
UGBW	1 kHz (set by 1 kHz filter)		
SR	0.012 V/µs (set by 1 kHz filter)		
#Channels	1		
INA326			

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