## Test Report: PMP22075

High Efficiency 12-V/5-A Active-Clamp Forward With Wide Input Range 9-V to 60-V Reference Design

## TEXAS INSTRUMENTS

## Description

This forward converter was designed for an isolated 60 W intermediate bus voltage rail 12 V . It features LM5026100 V active clamp current mode PWM controller. A self-driven secondary rectifier with UCC27511 4A/8A driver was used for high efficiency. It is good for isolated supplies where high efficiency and hiccup protection are needed.


## 1 Test Prerequisites

### 1.1 Voltage and Current Requirements

Table 1. Voltage and Current Requirements

| PARAMETER | SPECIFICATIONS |
| :--- | :---: |
| Input voltage, Vin | $9 \mathrm{~V} \sim 60 \mathrm{~V}$ |
| Output Voltage, Vo | $12 \mathrm{~V} / 5 \mathrm{~A}$ |

### 1.2 Required Equipment

- Power Supply, 0~60V, 0~10A
- Load: 12V/5A

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## 2 Startup and shutdown



Turn-on, 12Vin, 12V/5A


Turn-on, 48Vin, 12V/5A

## 3 Startup with Enable



Turn-on, 24Vin


Turn-off, 12Vin, 12V/5A


## 4 Input Ripple and Primary Switching Node



12 Vin, 12 Vout, 0A Load, 254 mV ( $2.1 \%$ ) ( $1 \times 68 \mathrm{uF}, 100 \mathrm{~V}$, 320 mohm +1x10uF, $80 \mathrm{~V}, 2.4 \mathrm{ohm}+3 x 2.2 \mathrm{uF}, 100 \mathrm{~V}, 1210$ )

$24 \mathrm{Vin}, 12 \mathrm{Vout}, 0 \mathrm{~A}$ Load, 301 mV (1.25\%) (1x68uF, 100V, 320mohm +1x10uF, $80 \mathrm{~V}, 2.4 \mathrm{ohm}+3 \times 2.2 \mathrm{uF}, 100 \mathrm{~V}, 1210$ )

$36 \mathrm{Vin}, 12 \mathrm{Vout}, 0 \mathrm{~A}$ Load, $310 \mathrm{mV}(0.86 \%)(1 \times 68 \mathrm{uF}, 100 \mathrm{~V}, 320 \mathrm{mohm}$ +1x10uF, 80V, $2.4 \mathrm{ohm}+3 \times 2.2 \mathrm{uF}, 100 \mathrm{~V}, 1210$ )


48Vin, 12Vout, 0A Load, 376mV (0.78\%) (1x68uF, 100V, 320mohm $+1 \times 10 \mathrm{uF}, 80 \mathrm{~V}, 2.4 \mathrm{ohm}+3 \mathrm{x} 2.2 \mathrm{uF}, 100 \mathrm{~V}, 1210$ )


12Vin, 12Vout, 5A Load, 1.2V (10\%) (1x68uF, 100V, 320mohm +1x10uF, 80V, 2.4ohm+ 3x 2.2uF,100V,1210)



24Vin, 12Vout, 5A Load, 1.25V (5.2\%) (1x68uF, 100V, 320mohm +1x10uF, 80V, 2.4ohm+3x 2.2uF,100V,1210)



36Vin, 12Vout, 5A Load, 1.305V (3.6\%)(1x68uF, 100V, 320mohm +1x10uF, 80V, 2.4ohm+3x 2.2uF,100V,1210)


48Vin, 12Vout, 5A Load, 1.274V (2.65\%) (1x68uF, 100V, 320mohm +1x10uF, 80V, 2.4ohm+3x 2.2uF,100V,1210)

## 5 Output Ripple


$12 \mathrm{Vin}, 12 \mathrm{Vout}, 0 \mathrm{~A}$ Load, 100 mV (+/-0.5\%) (1x100uF, 25 V , $260 \mathrm{mohm}+2 \times 22 \mathrm{uF}, 25 \mathrm{~V}, 1210)$

$24 \mathrm{Vin}, 12$ Vout, OA Load, 180 mV (+/-0.75\%) (1x100uF, 25V,
$260 \mathrm{mohm}+2 \times 22 \mathrm{uF}, 25 \mathrm{~V}, 1210)$


36Vin, 12 Vout, 0A Load, 240 mV (+/-1\%) (1x100uF, 25V, 260mohm+ 2x 22uF, 25V, 1210)


48Vin, 12Vout, 0A Load, 240 mV (+/-1\%) (1x100uF, 25V, $260 \mathrm{mohm}+2 \mathrm{x} 22 \mathrm{uF}, 25 \mathrm{~V}, 1210$ )
 $260 \mathrm{mohm}+2 \mathrm{x} 22 \mathrm{uF}, 25 \mathrm{~V}, 1210$ )

$24 \mathrm{Vin}, 12$ Vout, 5 A Load, 180 mV (+/-0.75\%) (1x100uF, 25V, $260 \mathrm{mohm}+2 \mathrm{x} 22 \mathrm{uF}, 25 \mathrm{~V}, 1210)$

$36 \mathrm{Vin}, 12 \mathrm{Vout}, 5 \mathrm{~A}$ Load, $240 \mathrm{mV}(+/-1 \%)(1 \times 100 \mathrm{uF}, 25 \mathrm{~V}$, $260 \mathrm{mohm}+$


48Vin, 12Vout, 5A Load, 240 mV (+/-1\%) (1x100uF, 25V, $260 \mathrm{mohm}+2 \mathrm{x} 22 \mathrm{uF}, 25 \mathrm{~V}, 1210$ )

## 6 Secondary Switching Node



## 7 Transient



## 8 Over-current protection



12 Vin , Over-load applied, OCP=6.3A.

## 9 Short-circuit protection


$48 \mathrm{Vin}, 12 \mathrm{Vout}$, Short circuit applied, $\mathrm{SCP}=9.2 \mathrm{~A}$.


10 Short-circuit thermal


48 Vin , 0 Vout, 9.2 A short circuit average current, $\mathrm{T}_{\text {FET(SEC) }}=97.2 \mathrm{C}$

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## 11 Efficiency



Test conditions: 12Vout, 160 kHz .

| Vin | Vout | lin | lout | eff | ploss |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 9.011 | 10.579 | 0.193 | 0.016 | $9.8 \%$ | 1.57 |
| 9.009 | 10.460 | 0.746 | 0.497 | $77.3 \%$ | 1.52 |
| 9.007 | 10.365 | 1.317 | 0.993 | $86.8 \%$ | 1.57 |
| 9.005 | 10.280 | 1.892 | 1.488 | $89.8 \%$ | 1.74 |
| 9.003 | 10.193 | 2.469 | 1.985 | $91.0 \%$ | 2.00 |
| 9.001 | 10.109 | 3.047 | 2.481 | $91.5 \%$ | 2.35 |
| 8.999 | 10.037 | 3.630 | 2.979 | $91.5 \%$ | 2.76 |
| 8.997 | 9.952 | 4.209 | 3.475 | $91.3 \%$ | 3.29 |
| 8.996 | 9.853 | 4.780 | 3.973 | $91.0 \%$ | 3.86 |
| 8.994 | 9.762 | 5.353 | 4.471 | $90.7 \%$ | 4.50 |
| 8.992 | 9.680 | 5.925 | 4.968 | $90.2 \%$ | 5.20 |
|  |  |  |  |  |  |
| 12.001 | 11.842 | 0.160 | 0.016 | $9.9 \%$ | 1.73 |
| 11.999 | 11.844 | 0.637 | 0.497 | $77.1 \%$ | 1.75 |
| 11.998 | 11.846 | 1.132 | 0.993 | $86.7 \%$ | 1.81 |
| 11.996 | 11.846 | 1.634 | 1.489 | $89.9 \%$ | 1.97 |
| 11.994 | 11.846 | 2.148 | 1.986 | $91.3 \%$ | 2.24 |
| 11.992 | 11.847 | 2.667 | 2.482 | $91.9 \%$ | 2.58 |
| 11.991 | 11.847 | 3.194 | 2.979 | $92.2 \%$ | 3.00 |
| 11.989 | 11.847 | 3.725 | 3.475 | $92.2 \%$ | 3.49 |


| 11.987 | 11.847 | 4.264 | 3.974 | $92.1 \%$ | 4.04 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 11.985 | 11.847 | 4.814 | 4.472 | $91.8 \%$ | 4.71 |
| 11.984 | 11.847 | 5.367 | 4.968 | $91.5 \%$ | 5.45 |
|  |  |  |  |  |  |
| 24.003 | 11.852 | 0.136 | 0.016 | $5.9 \%$ | 3.08 |
| 24.003 | 11.852 | 0.375 | 0.498 | $65.6 \%$ | 3.10 |
| 24.002 | 11.851 | 0.621 | 0.994 | $79.0 \%$ | 3.12 |
| 24.001 | 11.850 | 0.867 | 1.489 | $84.8 \%$ | 3.16 |
| 24.000 | 11.850 | 1.119 | 1.986 | $87.7 \%$ | 3.31 |
| 23.999 | 11.849 | 1.374 | 2.482 | $89.2 \%$ | 3.56 |
| 23.998 | 11.849 | 1.634 | 2.980 | $90.0 \%$ | 3.91 |
| 23.997 | 11.848 | 1.895 | 3.476 | $90.6 \%$ | 4.29 |
| 23.996 | 11.848 | 2.160 | 3.974 | $90.8 \%$ | 4.76 |
| 23.996 | 11.847 | 2.428 | 4.472 | $90.9 \%$ | 5.29 |
| 23.995 | 11.846 | 2.699 | 4.968 | $90.9 \%$ | 5.90 |
|  |  |  |  |  |  |
| 36.028 | 11.851 | 0.068 | 0.015 | $7.4 \%$ | 2.28 |
| 36.028 | 11.851 | 0.232 | 0.497 | $70.5 \%$ | 2.46 |
| 36.027 | 11.851 | 0.403 | 0.993 | $81.1 \%$ | 2.75 |
| 36.027 | 11.851 | 0.576 | 1.489 | $85.1 \%$ | 3.10 |
| 36.026 | 11.851 | 0.751 | 1.986 | $87.0 \%$ | 3.50 |
| 36.026 | 11.851 | 0.924 | 2.482 | $88.3 \%$ | 3.89 |
| 36.025 | 11.851 | 1.100 | 2.980 | $89.1 \%$ | 4.31 |
| 36.024 | 11.850 | 1.276 | 3.476 | $89.6 \%$ | 4.78 |
| 36.024 | 11.849 | 1.455 | 3.974 | $89.9 \%$ | 5.31 |
| 36.023 | 11.848 | 1.634 | 4.472 | $90.0 \%$ | 5.89 |
| 36.023 | 11.848 | 1.816 | 4.969 | $90.0 \%$ | 6.53 |
|  |  |  |  |  |  |
| 48.027 | 11.852 | 0.060 | 0.016 | $6.6 \%$ | 2.69 |
| 48.026 | 11.852 | 0.181 | 0.498 | $68.0 \%$ | 2.78 |
| 48.026 | 11.852 | 0.309 | 0.994 | $79.3 \%$ | 3.07 |
| 48.025 | 11.851 | 0.443 | 1.489 | $82.9 \%$ | 3.65 |
| 48.025 | 11.850 | 0.582 | 1.987 | $84.3 \%$ | 4.39 |
| 48.024 | 11.850 | 0.714 | 2.483 | $85.8 \%$ | 4.86 |
| 48.024 | 11.849 | 0.847 | 2.980 | $86.8 \%$ | 5.35 |
| 48.023 | 11.849 | 0.980 | 3.477 | $87.5 \%$ | 5.89 |
| 48.023 | 11.847 | 1.115 | 3.974 | $87.9 \%$ | 6.46 |
| 48.023 | 11.847 | 1.251 | 4.472 | $88.2 \%$ | 7.08 |
| 48.022 | 11.846 | 1.386 | 4.969 | $88.4 \%$ | 7.72 |
|  |  |  |  |  |  |
| 60.030 | 11.850 | 0.056 | 0.015 | $5.5 \%$ | 3.15 |
| 60.029 | 11.851 | 0.152 | 0.498 | $64.5 \%$ | 3.25 |
| 60.029 | 11.850 | 0.255 | 0.994 | $77.0 \%$ | 3.52 |
| 60.029 | 11.850 | 0.364 | 1.489 | $80.7 \%$ | 4.22 |
| 60.029 | 11.849 | 0.480 | 1.987 | $81.8 \%$ | 5.25 |
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| 60.028 | 11.848 | 0.588 | 2.483 | $83.3 \%$ | 5.89 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 60.028 | 11.848 | 0.696 | 2.980 | $84.6 \%$ | 6.45 |
| 60.027 | 11.847 | 0.804 | 3.477 | $85.3 \%$ | 7.07 |
| 60.027 | 11.847 | 0.914 | 3.974 | $85.9 \%$ | 7.75 |
| 60.026 | 11.845 | 1.022 | 4.473 | $86.4 \%$ | 8.37 |
| 60.026 | 11.844 | 1.132 | 4.969 | $86.6 \%$ | 9.08 |

## 12 Thermal


$48 \mathrm{Vin}, 12 \mathrm{~V} 5 \mathrm{~A}, \mathrm{~T}_{\mathrm{FET}(\mathrm{SEC})}=60.8 \mathrm{C}$ Front view

Test conditions: $48 \mathrm{Vin}, 12 \mathrm{~V} / 5$ Aout, 160 kHz , Room Temperature, 200LFM. $\mathrm{T}_{\text {FET(SEC })}=60.8 \mathrm{C}, \mathrm{T}_{\mathrm{XFMR}}=40 \mathrm{C}$, $\mathrm{T}_{\text {FET(PRI) }}=39 \mathrm{C}$.

## 13 Bode Plot


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