Technical Article **Power Tips: Design Considerations of High-voltage Converters in a Cascode MOSFET**



Sheng-yang Yu1

As I mentioned in my last blog, a cascode MOSFET configuration provides a low-cost alternative for highvoltage applications such as smart meters and motor drives. To further understand how a cascode MOSFET configuration works in high-voltage converters, Figure 1 shows a MOSFET modeled by a switch in parallel with a diode and a capacitor,. In addition to the switch, diode and paralleled capacitor, you must also consider the gate-to-source capacitance, C_a , of the top-side MOSFET.

In this blog post, I will discuss two possible operational conditions when using a cascode MOSFET configuration: $V_{in} < V_{Zc}$ and $V_{in} \ge V_{Zc}$, where V_{Zc} is the clamping voltage of the Zener diode Z_C .

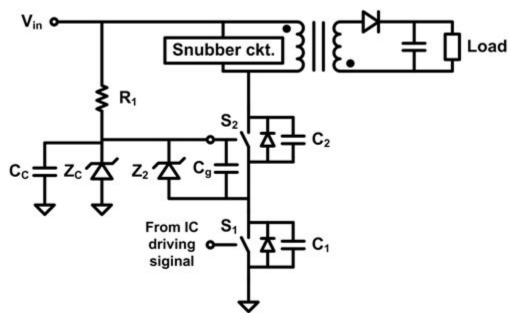


Figure 1. Flyback Converter in a Cascode MOSFET Configuration

$V_{in} < V_{Zc}$

When the converter first powers up, capacitor C_C will be charged to V_{in} through R_1 . Once the controller bias voltage is charged above the undervoltage lockout (UVLO) threshold, switch S_1 turns on. As shown in Figure 2, when S_1 turns on, the energy in C_C transfers to C_g and leads to voltage increases on C_g . In order to turn on S_2 , the clamping voltage of Z_2 needs to be set higher than the gate-to-source threshold voltage ($V_{gs(th)}$) of the top-side MOSFET. It is important to have enough energy in C_g to keep the top-side MOSFET turned on during the entire on state after the bottom-side MOSFET turns on. In other words, C_C can't be too small. Sometimes, the parasitic capacitance of Z_C might not be enough and will require an external capacitor in parallel with Z_C .



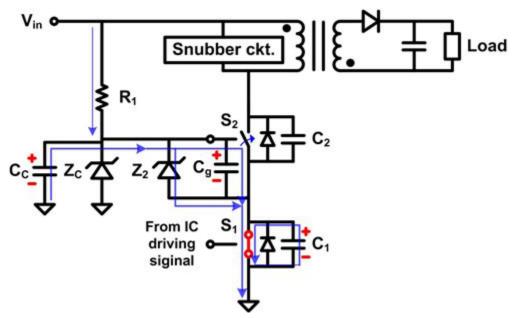


Figure 2. MOSFET Turned-on Transient

When the MOSFET on the bottom side turns off (Figure 3), the current from the transformer quickly charges C_1 . C_g discharges and energy goes back to C_C again. Once C_g discharges to a voltage level lower than $V_{gs(th)}$, S_2 turns off and C_2 charges up.

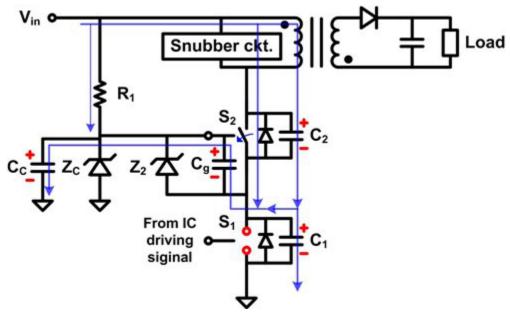


Figure 3. MOSFET Turned-off Transient (v_{in} < V_{Zc})

$V_{in} \ge V_{Zc}$

The current-flow directions during the low-side MOSFET turned-on transient when $V_{in} \ge V_{Zc}$ are exactly the same as when $V_{in} < V_{Zc}$. During low-side MOSFET turned-off transient, transformer current discharges C_g and then flows through C_C and Z_C , as shown in Figure 4. In this transient, Z_C acts as a snubber and clamps the low-side MOSFET voltage to $V_{Zc} + V_{F_z}$, where V_{F_z} is the Zener forward voltage drop of Z_2 .



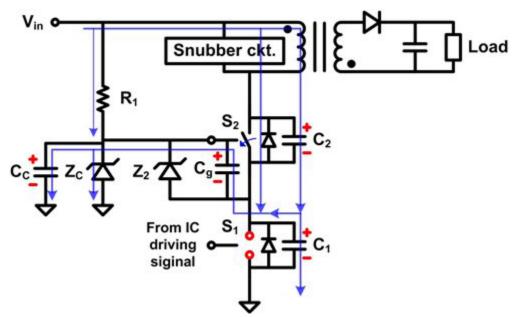


Figure 4. MOSFET Turned-off Transient ($v_{in} \ge V_{Zc}$)

The longer turn-off delay time S_2 has after S_1 has already turned off, the higher current flows through S_2 to Z_C , which might lead to a thermal issue for Z_C . Figure 5 below shows a turn-off transient example. As you can see, S_2 is starting to turn off after S_1 is fully turned off. In the transient, S_1 is already off and S_2 is turning on. A surge current flows through Z_C and this causes a thermal issue with Zener diode Z_C .

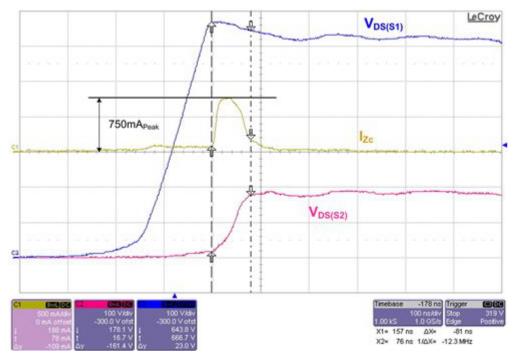


Figure 5. Waveforms During MOSFET Turned-off Transient with a Longer Turn-off Delay Time ($v_{in} \ge V_{Zc}$)

If the turn-off delay time between S_1 and S_2 can be minimized by using MOSFETs with better transient characteristics (like the example in Figure 6), the current going to Z_C can also be minimized, and reducing the temperature rise of Z_C .

3



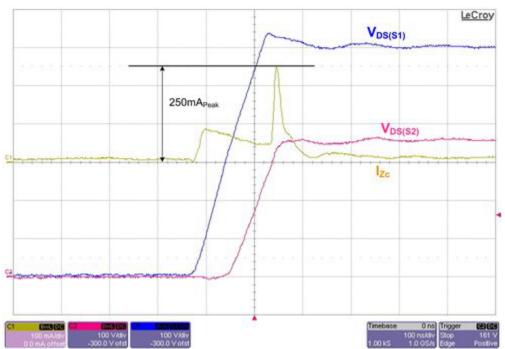


Figure 6. Waveforms During Low-side MOSFET Turned-off Transient with a Shorter Turn-off Delay Time $(v_{in} \ge V_{Zc})$

Many components go into designing high voltage converters with a cascode MOSFET configuration, but mastering the key operations with carefully circuit parameter selection allows for a low cost alternative for high-voltage applications.

Additional Resources

- Discover TI's Power Tips blog series on Power House.
- Check out the following TI Designs reference design, which use a cascode MOSFET configuration
 - 400V to 690V AC Input, 50W Flyback Isolated Power Supply Reference Design for Motor Drives

IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2023, Texas Instruments Incorporated