

Analysis of Start-Up Performance for UCC28700

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Power Management/Field Application

ABSTRACT

The UCC28700 device is a primary controlled fly-back power supply controller, which provides both constant voltage and constant current regulation. The device has high resolution for voltage and current regulation, and it has very low no-load power consumption and good start-up performance. As a result, the UCC28700 device is highly suited for low-power adapter and auxiliary power supply application. Compared with other competitors, the UCC28700 device has better performance and needs a smaller V_{DD} capacitor. A customer may experience a situation in which the UCC28700 device cannot start a constant current full load, but can start at resistance full load. The real reason is that the value of the V_{DD} capacitor is not sufficient and primary peak current is designed too small. This paper analyzes the design of primary peak current and V_{DD} capacitor. An experiment result validates the theoretical analysis.

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1. Introduction

The UCC28700 device is a constant voltage, constant current fly-back controller with primary side regulation without the use of an optical coupler. Figure 1 shows the UCC28700 application circuit.



Figure 1. UCC28700 Application Circuit

In Figure 1:

- R_{STR} is high-voltage start-up resistance.
- C_{DD} is energy storage capacitor on the V_{DD} pin.
- R_{S1} is high-side feedback resistance.
- R_{S2} is low-side feedback resistance.
- R_{CBC} is programming cable compensation resistance.
- R_{cs} is primary peak current programming resistance.
- R_{LC} is MOSFET turn-off delay compensation programming resistance.

Primary peak current is a critical factor for the UCC28700 starting up at constant current full load. The following section provides a detailed analysis.

2. Analysis

Figure 2 shows the UCC28700 secondary side circuit, $I_s = I_c + I_L$. If the load of the UCC28700 device is resistance at the beginning of startup, V_o ramps up from zero and I_L is low enough so that high I_s is not required. However, if the load of the device is constant current and the load current is large, high I_s is required to make I_c positive and to reduce the time that output voltage ramps up from 0 to V_{occ}. V_{occ} is the target lowest converter output voltage, which makes auxiliary turn voltage equal to UVLO turn-off voltage on the V_{DD} pin.



Figure 2. UCC28700 Secondary Side Circuit

To C_{DD} , C_{O} , and the transformer, the following equations are achieved. In Equation 4, a 1-mA current margin is provided.

NOTE: N_P is primary turns of transformer, N_S is secondary turns, and N_A is auxiliary turns.

$$I_C = I_S - I_L \tag{1}$$

$$V_{OCC} = V_{DD(off)} \frac{N_s}{N_A}$$
(2)

$$t_a = C_o \frac{V_{OCC}}{I_C}$$
(3)

$$\Delta V_{DD} = \frac{(I_{run} + 1mA)}{C_{DD}} t_a \tag{4}$$

$$V_{DD} = V_{DD(on)} - \Delta V_{DD}$$
⁽⁵⁾

Where:

- V_{DD(off)} is UVLO turn-off voltage.
- V_{DD(on)} is UVLO turn-on voltage.
- I_{run} is supply current on the V_{DD} pin when UCC28700 works.
- V_{DD} is the voltage of C_{DD}.
- ΔV_{DD} is the decreased voltage on C_{DD}.
- t_a is the time that output voltage ramps up from 0 to V_{occ}.

According to the preceding equations, if the value of I_S is low, I_C will be small, so t_a becomes a long time when output voltage ramps up to V_{OCC}; however, during this period, V_{DD} may decrease below V_{DD(off)} and the UCC28700 device may enter UVLO state and stop switching. Then the current through R_{STR} charges C_{DD}; when V_{DD} is higher than V_{DD(on)}, the device restarts. Although faulty startup continues, the UCC28700 device cannot enter normal state.

In Equation 4, if C_{DD} is large enough, ΔV_{DD} will be small for certain t_a . So, both a large value C_{DD} and a high primary peak current can make the UCC28700 device start well. However, large value C_{DD} means higher price and larger size, and high primary peak current increases power loss and increases transformer size. Consequently, choosing C_{DD} and primary peak current is a trade-off.



In normal operation, auxiliary winding voltage dominates V_{DD} . If V_O reaches its maximum value, V_{DD} will also match its maximum value. The relation is shown in Equation 6.

$$V_{DD\max} = V_{O\max} \frac{N_A}{N_S}$$
(6)

From Equation 2, 3, and 6, if N_A increases, t_a is reduced, that's good for UCC28700 starting up. So a large value should be chosen for N_A , and it also must provide voltage margin for V_{DD} .

3. Design

All device values, except C_{DD} and R_{CS} , are the same as the UCC28700EVM-068 5-W USB adapter ^[1] schematic. Figure 3 is shown in the UCC28700 data sheet ^[2]. I_S is deduced as Equation 7, where η_{XFMR} is estimated transformer efficiency.

Transformer efficiency is influenced by the core and winding losses, leakage inductance ratio, and bias power ratio to rated output power. For a 5-V, 1-A charger example, bias power of 1.5% is a good estimate ^[1]. An overall transformer efficiency of 0.9 is an approximate estimate to include 3.5% leakage inductance, 5% core and winding loss, and 1.5% bias power ^[1].

Maximum primary peak current I_{PP} is achieved at the beginning of startup, and the UCC28700 device enters constant current regulation with maintaining constant secondary diode conduction duty cycle, 0.425.

The transformer is WE 750312723 on EVM, $N_P/N_S = 15.33$, $N_P/N_A = 3.83$, and saturation current is 440 mA.



Figure 3. Transformer Current

$$I_{S} = \frac{I_{PP}N_{P}t_{DM}}{2N_{S}T_{SW}}\eta_{XFMR}$$

(7)



At the beginning of startup, average charging current of output capacitor is positive, the charge current equals (I_S - I_L) as Equation 1 shows. Before V_O ramps up to V_{OCC} , the auxiliary turn voltage is lower than V_{DD} , and C_{DD} cannot be charged by auxiliary turns. However, C_{DD} is discharged by I_{run} and gate drive current during this period; if V_{DD} is lower than $V_{DD(off)}$, the UCC28700 device shuts down. To ensure the device starts up well, V_{DD} must be larger than $V_{DD(off)}$ during t_a . In Equations 8 and 9, a critical condition is applied; t_{start} is the time that V_O ramps up from 0 to V_{OCC} . Equation 2 shows the relation of V_{OCC} and $V_{DD(off)}$. An estimated 1 mA of gate-drive current exists in Equation 8 and 1 V of margin is added to V_{DD} . V_{CST} is chip select threshold voltage. At the beginning of startup, voltage on the UCC28700 VS pin is low, so V_{CST} stays at its maximum value.

$$C_{DD} = \frac{t_{start}(I_{run} + 1mA)}{(V_{DD(on)} - V_{DD(off)}) - 1V}$$
(8)

$$t_{start} = \frac{C_O V_{OCC}}{I_S - I_L} \tag{9}$$

$$R_{CS} = \frac{V_{CST}}{I_{PP}} \tag{10}$$

In the UCC28700 device, $V_{DD(on)} = 21 \text{ V}$, $V_{DD(off)} = 8.1 \text{ V}$, so according to Equation 2, $V_{OCC} = 2.02 \text{ V}$. $I_{run} = 2.1 \text{ mA}$ in data sheet, C_{DD} is chosen as 4.7 µF, $t_{start} = 18.04 \text{ ms}$ is deduced by Equation 8. UCC28700 EVM is 5-V, 1-A adapter, so full load current I_L is 1 A. Output capacitors are two paralleled 560-µF capacitors, so $C_O = 1120 \text{ µF}$. t_{start} , I_L , and C_O are substituted into Equations 7 and 9, I_{PP} is obtained as 383.85 mA. From Equation 10, $R_{CS} = 1.95 \Omega$. To add margin on V_{DD} , 1.8 Ω is selected for R_{CS} .

As shown in Table 1, the UCC28700 device has better constant current (CC) regulation performance; a higher max operation frequency, which can minimize the solution size; standby power is less than 30 mW, which is for 5-star rating; and higher max V_{DD}, which can reduce V_{DD} capacitor value. Of the three products highlighted in Table 1, the UCC28700 device is the best choice when designing 5-V adapters. The UCC28700 device can choose higher N_A/N_S because it has higher max V_{DD} according to Equation 2, and smaller t_{start} is achieved (see Equation 9). In Equation 8, t_{start} is proportional to C_{DD}, so smaller C_{DD} is required during design.

Product Number	UCC28700	OB2520M	iW1680
CV (constant voltage)	5%	5%	null
CC (constant current)	5%	6%	null
Max Operation Frequency	130 kHz	100 kHz	72 kHz
Standby Power	<30 mW	<200 mW	<30 mW
Max V _{DD}	38 V	28 V	25 V

 Table 1.
 Parameters Comparison Table

4. Experiment

To validate the preceding analysis, a UCC28700EVM-068 5-W USB adapter is used. All device values are kept the same except C_{DD} and R_{CS} , C_{DD} = 4.7 µF, R_{CS} = 1.8 Ω . The load is constant current as 1 A.

Figure 4 is a UCC28700 start-up waveform. CH1 is a MOSFET gate-drive signal and CH3 is output voltage. The device starts up smoothly, with no overshoot and audible noise. The figure shows the UCC28700 device has a very good start-up performance. In Figure 4, t_{start} approximates 18 ms, which meets the calculated result.



Figure 5, Figure 6, and Figure 7 represent a compared experiment. CH1 is V_{DD} voltage and CH3 is output voltage.



- In Figure 5, C_{DD} = 4.7 μF, R_{C S}= 2.05 Ω: because primary peak current is not large enough, V_{DD} decreases below V_{DD(off)}, thus the UCC28700 device cannot start.
- In Figure 6, C_{DD} = 4.7 μF, R_{CS} = 1.8 Ω: primary peak current is increased, so a good start-up performance is observed.
- In Figure 7, $C_{DD} = 1 \mu F$, $R_{CS} = 1.8 \Omega$: the UCC28700 device cannot start because C_{DD} is not large enough to provide sufficient energy.

The results of the experiment reveal that both high primary peak current and large volume C_{DD} can make the UCC28700 device start successfully at constant current full load. These findings verify the preceding analysis.





5. Conclusion

Comparison results indicate the UCC28700 device has better performance in CV and CC regulation, solution size, standby power, and V_{DD} capacitor value. In the course of this study, primary peak current and V_{DD} capacitor were analyzed and calculated. Proper parameters were chosen according to equations, and the analysis was verified by experiment results.

6. References

[1] UCC28700EVM-068 5-W USB Adapter. Texas Instruments User's Guide, SLUU968, July 2012

[2] *Constant-Voltage, Constant-Current Controller With Primary-Side Regulation*. Texas Instruments UCC2870x data sheet, SLUSB41, July 2012

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